1	Page 1		Page 3
1	Wednesday, 16 January 2019	1	Q. Then you tried to plot that in your graph versus the
2	PROF YEUNG TAK CHUNG, ALBERT (on former affirmation	) 2	actual physical test results. That was the purpose of
3	(10.07 am)	3	your chart; remember?
4	CHAIRMAN: Sorry, just before we start, could I mention one	4	A. Correct.
5	thing. I have a longstanding hearing this evening in	5	Q. We can look at that now. Could I have shown on the
6	the Market Misconduct Tribunal, starting at 5.30. It's	6	screen Prof Yeung's chart. We actually sent we took
7	not merely a directions hearing, it's a substantive	7	that out of Prof Yeung's series of slides yesterday and
8	hearing, and I'll obviously have to be there. I've got	8	we emailed that to the Commission. I don't know whether
9	the papers with me, so it's only a question of	9	or not the Commission has managed to include that in the
10	presenting myself there by 5.30. I wouldn't want to	10	e-bundles yet.
11	keep a room full of people waiting.	11	CHAIRMAN: I think we all have them. This is the one we're
12	So, all being well, I would this evening ask if we	12	talking about? (Indicating).
13	could rise at quarter to five. All right? Thank you	13	MR SHIEH: Yes, but for the benefit of those sitting
14	very much.	14	outside
15	MR BOULDING: Sir, I was going to ask for leave to ask one	15	CHAIRMAN: Yes, of course, who are sitting outside.
16	or two further questions arising out of our reading of	16	MR PENNICOTT: What's the question?
17	last night's transcript, but I understand that Mr Shieh	17	MR SHIEH: The question has not been asked yet because I'm
18	might also have an application to reopen his	18	trying to locate the actual graph Prof Yeung presented
19	cross-examination. So assuming that leave is granted,	19	yesterday. It's halfway through.
20	logically he probably ought to go first.	20	WITNESS: I think it's slide number 12.
21	MR SHIEH: Yes. Mr Chairman, I've had a word with Mr Chow	21	MR SHIEH: That's it, yes.
22	who indicated that he would be asking questions after	22	Prof Yeung, look at the description that you put
23	me, and also with Mr So, representing China Technology,	23	at the bottom of page 108, you say, line 24:
24	that I have one topic I wish to explore with Prof Yeung,	24	"Then now you can look at the open circle. The open
25	arising out of one of the slides that he produced. The	25	circles are the experimental results from the five
	Page 2		Page 4
1	slides were produced sometime during the day yesterday	1	ones"
2	and we only had time to do some detailed checking and	2	And then over the page at page 28:
3	production of graphs overnight. Therefore, for that	3	" that we saw so far. So you can see now I try
4	reason, I seek leave to ask some further questions of	4	to adopt the same symbol you have seen in those reports,
5	Prof Yeung on one topic.		
6	The Teang on one topic.	5	so 'S' stands for slipout 'C' stands for the failure
I Ŭ	COMMISSIONER HANSFORD: That's fine.	5 6	so 'S' stands for slipout 'C' stands for the failure in the coupler, and then the 'B' stands for the fracture
7			*
	COMMISSIONER HANSFORD: That's fine. CHAIRMAN: Yes. You may proceed, and Mr Boulding also, thank you.	6	in the coupler, and then the 'B' stands for the fracture
7	COMMISSIONER HANSFORD: That's fine. CHAIRMAN: Yes. You may proceed, and Mr Boulding also,	6 7	in the coupler, and then the 'B' stands for the fracture in the bar.
7 8	COMMISSIONER HANSFORD: That's fine. CHAIRMAN: Yes. You may proceed, and Mr Boulding also, thank you.	6 7 8	in the coupler, and then the 'B' stands for the fracture in the bar. When you look at this circle, look at the first one
7 8 9	<ul><li>COMMISSIONER HANSFORD: That's fine.</li><li>CHAIRMAN: Yes. You may proceed, and Mr Boulding also, thank you.</li><li>MR BOULDING: I appreciate that.</li></ul>	6 7 8 9	in the coupler, and then the 'B' stands for the fracture in the bar. When you look at this circle, look at the first one with 'S', it looks like it's very close to the
7 8 9 10	<ul><li>COMMISSIONER HANSFORD: That's fine.</li><li>CHAIRMAN: Yes. You may proceed, and Mr Boulding also, thank you.</li><li>MR BOULDING: I appreciate that.</li><li>Further cross-examination by MR SHIEH</li></ul>	6 7 8 9 10	in the coupler, and then the 'B' stands for the fracture in the bar. When you look at this circle, look at the first one with 'S', it looks like it's very close to the theoretical calculation, but in fact now is, if you
7 8 9 10 11	<ul> <li>COMMISSIONER HANSFORD: That's fine.</li> <li>CHAIRMAN: Yes. You may proceed, and Mr Boulding also, thank you.</li> <li>MR BOULDING: I appreciate that.</li> <li>Further cross-examination by MR SHIEH</li> <li>MR SHIEH: Prof Yeung, good morning.</li> <li>A. Good morning.</li> <li>Q. Can I ask you to look at the transcript of yesterday's</li> </ul>	6 7 8 9 10 11	<ul> <li>in the coupler, and then the 'B' stands for the fracture in the bar.</li> <li>When you look at this circle, look at the first one with 'S', it looks like it's very close to the theoretical calculation, but in fact now is, if you think about more detail, the solid circle"</li> <li>Pausing here, Prof Yeung, the solid circle is what we call the calculated the theoretical circle?</li> </ul>
7 8 9 10 11 12 13 14	<ul> <li>COMMISSIONER HANSFORD: That's fine.</li> <li>CHAIRMAN: Yes. You may proceed, and Mr Boulding also, thank you.</li> <li>MR BOULDING: I appreciate that. Further cross-examination by MR SHIEH</li> <li>MR SHIEH: Prof Yeung, good morning.</li> <li>A. Good morning.</li> <li>Q. Can I ask you to look at the transcript of yesterday's hearing at page 109.</li> </ul>	6 7 8 9 10 11 12	in the coupler, and then the 'B' stands for the fracture in the bar. When you look at this circle, look at the first one with 'S', it looks like it's very close to the theoretical calculation, but in fact now is, if you think about more detail, the solid circle" Pausing here, Prof Yeung, the solid circle is what
7 8 9 10 11 12 13 14 15	<ul> <li>COMMISSIONER HANSFORD: That's fine.</li> <li>CHAIRMAN: Yes. You may proceed, and Mr Boulding also, thank you.</li> <li>MR BOULDING: I appreciate that. Further cross-examination by MR SHIEH</li> <li>MR SHIEH: Prof Yeung, good morning.</li> <li>A. Good morning.</li> <li>Q. Can I ask you to look at the transcript of yesterday's hearing at page 109. In fact, it starts at page 108, the previous page.</li> </ul>	6 7 8 9 10 11 12 13 14 15	<ul> <li>in the coupler, and then the 'B' stands for the fracture in the bar.</li> <li>When you look at this circle, look at the first one with 'S', it looks like it's very close to the theoretical calculation, but in fact now is, if you think about more detail, the solid circle"</li> <li>Pausing here, Prof Yeung, the solid circle is what we call the calculated the theoretical circle?</li> <li>A. The calculated value.</li> <li>Q. The calculated value, yes.</li> </ul>
7 8 9 10 11 12 13 14	<ul> <li>COMMISSIONER HANSFORD: That's fine.</li> <li>CHAIRMAN: Yes. You may proceed, and Mr Boulding also, thank you.</li> <li>MR BOULDING: I appreciate that.</li> <li>Further cross-examination by MR SHIEH</li> <li>MR SHIEH: Prof Yeung, good morning.</li> <li>A. Good morning.</li> <li>Q. Can I ask you to look at the transcript of yesterday's hearing at page 109.</li> <li>In fact, it starts at page 108, the previous page.</li> <li>This is where you introduce that chart remember, in</li> </ul>	6 7 8 9 10 11 12 13 14 15 16	<ul> <li>in the coupler, and then the 'B' stands for the fracture in the bar.</li> <li>When you look at this circle, look at the first one with 'S', it looks like it's very close to the theoretical calculation, but in fact now is, if you think about more detail, the solid circle"</li> <li>Pausing here, Prof Yeung, the solid circle is what we call the calculated the theoretical circle?</li> <li>A. The calculated value.</li> <li>Q. The calculated value, yes.</li> <li>" the solid circle is based on a tensile strength</li> </ul>
7 8 9 10 11 12 13 14 15 16 17	<ul> <li>COMMISSIONER HANSFORD: That's fine.</li> <li>CHAIRMAN: Yes. You may proceed, and Mr Boulding also, thank you.</li> <li>MR BOULDING: I appreciate that.</li> <li>Further cross-examination by MR SHIEH</li> <li>MR SHIEH: Prof Yeung, good morning.</li> <li>A. Good morning.</li> <li>Q. Can I ask you to look at the transcript of yesterday's hearing at page 109.</li> <li>In fact, it starts at page 108, the previous page.</li> <li>This is where you introduce that chart remember, in your slides, you produced a chart where you tried to</li> </ul>	6 7 8 9 10 11 12 13 14 15 16 17	<ul> <li>in the coupler, and then the 'B' stands for the fracture in the bar.</li> <li>When you look at this circle, look at the first one with 'S', it looks like it's very close to the theoretical calculation, but in fact now is, if you think about more detail, the solid circle"</li> <li>Pausing here, Prof Yeung, the solid circle is what we call the calculated the theoretical circle?</li> <li>A. The calculated value.</li> <li>Q. The calculated value, yes.</li> <li>" the solid circle is based on a tensile strength of 529 and this bar may actually be, as what we've been</li> </ul>
7 8 9 10 11 12 13 14 15 16 17 18	<ul> <li>COMMISSIONER HANSFORD: That's fine.</li> <li>CHAIRMAN: Yes. You may proceed, and Mr Boulding also, thank you.</li> <li>MR BOULDING: I appreciate that. <ul> <li>Further cross-examination by MR SHIEH</li> </ul> </li> <li>MR SHIEH: Prof Yeung, good morning.</li> <li>A. Good morning.</li> <li>Q. Can I ask you to look at the transcript of yesterday's hearing at page 109. <ul> <li>In fact, it starts at page 108, the previous page.</li> <li>This is where you introduce that chart remember, in your slides, you produced a chart where you tried to plot, first of all, the tensile strength as per BOSA's</li> </ul> </li> </ul>	6 7 8 9 10 11 12 13 14 15 16 17 18	<ul> <li>in the coupler, and then the 'B' stands for the fracture in the bar.</li> <li>When you look at this circle, look at the first one with 'S', it looks like it's very close to the theoretical calculation, but in fact now is, if you think about more detail, the solid circle"</li> <li>Pausing here, Prof Yeung, the solid circle is what we call the calculated the theoretical circle?</li> <li>A. The calculated value.</li> <li>Q. The calculated value, yes.</li> <li>" the solid circle is based on a tensile strength of 529 and this bar may actually be, as what we've been discussing so far, 500 with a tensile strength of 625.</li> </ul>
7 8 9 10 11 12 13 14 15 16 17	<ul> <li>COMMISSIONER HANSFORD: That's fine.</li> <li>CHAIRMAN: Yes. You may proceed, and Mr Boulding also, thank you.</li> <li>MR BOULDING: I appreciate that.</li> <li>Further cross-examination by MR SHIEH</li> <li>MR SHIEH: Prof Yeung, good morning.</li> <li>A. Good morning.</li> <li>Q. Can I ask you to look at the transcript of yesterday's hearing at page 109.</li> <li>In fact, it starts at page 108, the previous page.</li> <li>This is where you introduce that chart remember, in your slides, you produced a chart where you tried to plot, first of all, the tensile strength as per BOSA's table; right?</li> </ul>	6 7 8 9 10 11 12 13 14 15 16 17 18 19	<ul> <li>in the coupler, and then the 'B' stands for the fracture in the bar.</li> <li>When you look at this circle, look at the first one with 'S', it looks like it's very close to the theoretical calculation, but in fact now is, if you think about more detail, the solid circle"</li> <li>Pausing here, Prof Yeung, the solid circle is what we call the calculated the theoretical circle?</li> <li>A. The calculated value.</li> <li>Q. The calculated value, yes.</li> <li>" the solid circle is based on a tensile strength of 529 and this bar may actually be, as what we've been discussing so far, 500 with a tensile strength of 625. And if you use those numbers to recalculate, BOSA's</li> </ul>
7 8 9 10 11 12 13 14 15 16 17 18	<ul> <li>COMMISSIONER HANSFORD: That's fine.</li> <li>CHAIRMAN: Yes. You may proceed, and Mr Boulding also, thank you.</li> <li>MR BOULDING: I appreciate that. <ul> <li>Further cross-examination by MR SHIEH</li> </ul> </li> <li>MR SHIEH: Prof Yeung, good morning.</li> <li>A. Good morning.</li> <li>Q. Can I ask you to look at the transcript of yesterday's hearing at page 109. <ul> <li>In fact, it starts at page 108, the previous page.</li> <li>This is where you introduce that chart remember, in your slides, you produced a chart where you tried to plot, first of all, the tensile strength as per BOSA's</li> </ul> </li> </ul>	6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	<ul> <li>in the coupler, and then the 'B' stands for the fracture in the bar.</li> <li>When you look at this circle, look at the first one with 'S', it looks like it's very close to the theoretical calculation, but in fact now is, if you think about more detail, the solid circle"</li> <li>Pausing here, Prof Yeung, the solid circle is what we call the calculated the theoretical circle?</li> <li>A. The calculated value.</li> <li>Q. The calculated value, yes.</li> <li>" the solid circle is based on a tensile strength of 529 and this bar may actually be, as what we've been discussing so far, 500 with a tensile strength of 625.</li> </ul>
7 8 9 10 11 12 13 14 15 16 17 18 19	<ul> <li>COMMISSIONER HANSFORD: That's fine.</li> <li>CHAIRMAN: Yes. You may proceed, and Mr Boulding also, thank you.</li> <li>MR BOULDING: I appreciate that. <ul> <li>Further cross-examination by MR SHIEH</li> </ul> </li> <li>MR SHIEH: Prof Yeung, good morning.</li> <li>A. Good morning.</li> <li>Q. Can I ask you to look at the transcript of yesterday's hearing at page 109. <ul> <li>In fact, it starts at page 108, the previous page.</li> <li>This is where you introduce that chart remember, in your slides, you produced a chart where you tried to plot, first of all, the tensile strength as per BOSA's table; right?</li> </ul> </li> <li>A. Correct.</li> <li>Q. One thread, two threads, three threads, all the way down</li> </ul>	6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	<ul> <li>in the coupler, and then the 'B' stands for the fracture in the bar.</li> <li>When you look at this circle, look at the first one with 'S', it looks like it's very close to the theoretical calculation, but in fact now is, if you think about more detail, the solid circle"</li> <li>Pausing here, Prof Yeung, the solid circle is what we call the calculated the theoretical circle?</li> <li>A. The calculated value.</li> <li>Q. The calculated value, yes.</li> <li>" the solid circle is based on a tensile strength of 529 and this bar may actually be, as what we've been discussing so far, 500 with a tensile strength of 625. And if you use those numbers to recalculate, BOSA's</li> </ul>
7 8 9 10 11 12 13 14 15 16 17 18 19 20	<ul> <li>COMMISSIONER HANSFORD: That's fine.</li> <li>CHAIRMAN: Yes. You may proceed, and Mr Boulding also, thank you.</li> <li>MR BOULDING: I appreciate that.</li> <li>Further cross-examination by MR SHIEH</li> <li>MR SHIEH: Prof Yeung, good morning.</li> <li>A. Good morning.</li> <li>Q. Can I ask you to look at the transcript of yesterday's hearing at page 109.</li> <li>In fact, it starts at page 108, the previous page.</li> <li>This is where you introduce that chart remember, in your slides, you produced a chart where you tried to plot, first of all, the tensile strength as per BOSA's table; right?</li> <li>A. Correct.</li> </ul>	6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	<ul> <li>in the coupler, and then the 'B' stands for the fracture in the bar.</li> <li>When you look at this circle, look at the first one with 'S', it looks like it's very close to the theoretical calculation, but in fact now is, if you think about more detail, the solid circle"</li> <li>Pausing here, Prof Yeung, the solid circle is what we call the calculated the theoretical circle?</li> <li>A. The calculated value.</li> <li>Q. The calculated value, yes.</li> <li>" the solid circle is based on a tensile strength of 529 and this bar may actually be, as what we've been discussing so far, 500 with a tensile strength of 625. And if you use those numbers to recalculate, BOSA's calculate, those red dots"</li> </ul>
7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	<ul> <li>COMMISSIONER HANSFORD: That's fine.</li> <li>CHAIRMAN: Yes. You may proceed, and Mr Boulding also, thank you.</li> <li>MR BOULDING: I appreciate that. <ul> <li>Further cross-examination by MR SHIEH</li> </ul> </li> <li>MR SHIEH: Prof Yeung, good morning.</li> <li>A. Good morning.</li> <li>Q. Can I ask you to look at the transcript of yesterday's hearing at page 109. <ul> <li>In fact, it starts at page 108, the previous page.</li> <li>This is where you introduce that chart remember, in your slides, you produced a chart where you tried to plot, first of all, the tensile strength as per BOSA's table; right?</li> </ul> </li> <li>A. Correct.</li> <li>Q. One thread, two threads, three threads, all the way down</li> </ul>	6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	<ul> <li>in the coupler, and then the 'B' stands for the fracture in the bar.</li> <li>When you look at this circle, look at the first one with 'S', it looks like it's very close to the theoretical calculation, but in fact now is, if you think about more detail, the solid circle"</li> <li>Pausing here, Prof Yeung, the solid circle is what we call the calculated the theoretical circle?</li> <li>A. The calculated value.</li> <li>Q. The calculated value, yes.</li> <li>" the solid circle is based on a tensile strength of 529 and this bar may actually be, as what we've been discussing so far, 500 with a tensile strength of 625. And if you use those numbers to recalculate, BOSA's calculate, those red dots"</li> </ul>
7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>COMMISSIONER HANSFORD: That's fine.</li> <li>CHAIRMAN: Yes. You may proceed, and Mr Boulding also, thank you.</li> <li>MR BOULDING: I appreciate that. <ul> <li>Further cross-examination by MR SHIEH</li> </ul> </li> <li>MR SHIEH: Prof Yeung, good morning.</li> <li>A. Good morning.</li> <li>Q. Can I ask you to look at the transcript of yesterday's hearing at page 109. <ul> <li>In fact, it starts at page 108, the previous page.</li> <li>This is where you introduce that chart remember, in your slides, you produced a chart where you tried to plot, first of all, the tensile strength as per BOSA's table; right?</li> </ul> </li> <li>A. Correct.</li> <li>Q. One thread, two threads, three threads, all the way down to ten threads; yes?</li> </ul>	6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>in the coupler, and then the 'B' stands for the fracture in the bar.</li> <li>When you look at this circle, look at the first one with 'S', it looks like it's very close to the theoretical calculation, but in fact now is, if you think about more detail, the solid circle"</li> <li>Pausing here, Prof Yeung, the solid circle is what we call the calculated the theoretical circle?</li> <li>A. The calculated value.</li> <li>Q. The calculated value, yes. <ul> <li>" the solid circle is based on a tensile strength of 529 and this bar may actually be, as what we've been discussing so far, 500 with a tensile strength of 625.</li> <li>And if you use those numbers to recalculate, BOSA's calculate, those red dots"</li> <li>That means the solid dots; right?</li> </ul> </li> </ul>

	Page 5		Page 7
1	Q. The solid circle.	1	threads that appeared on the photographs?
2	" those red dots should be a whole lot higher	2	A. I trust the experimental record, rather than what they
3	because you get a higher shear strength, so for each	3	say to be 30 per cent, because I think they may make the
4	thread get engaged, they can take more stresses."	4	thread first because the bar was specially made for
5	Yes?	5	that experiment, and you can look at it, there are only
6	I'm not sure if there's anything wrong there. No.	6	four on it, because they did it on purpose to test the
7	If I may ask you to look at your graph, looking at	7	bar with less number of threads than the standard number
8	the open circles, the first open circle appears above	8	threads. Then they may do the calculation and say it's
9	"Number of threads engaged", 4?	9	approximately 30 per cent and I would consider the
10	A. Correct.	10	accurate way to do is you look at actually what they
11	Q. Now, that, according to the result, is actually	11	have done in the experiment and put it on the graph.
12	30 per cent engagement.	12	Q. Now, I would ask you to tell me where the photographs
13	A. Correct.	13	are, because everyone can look at the photographs. They
14	Q. And because the BOSA calculation is based on number of	14	are in the bundles; right?
15	threads engaged, we have to convert percentage	15	A. They are in the bundle.
16	engagement into threads engaged?	16	Q. I'm going to ask you where the photographs are.
17	A. Actually, when I do the analysis, I did look at the	17	A. I think they are attached to the letter of 7 January
18	picture in BOSA's letter. When they take a picture of	18	from BOSA to BD.
19	the 30 what they mark 30 per cent in the picture, and	19	Q. Yes. As I say, I'm going to look at that set of
20	I look at the picture, I actually count the threads in	20	photographs with you later.
21	the picture. That's how I get four.	21	A. Okay.
22	Q. The BOSA table, actually if we look at the BOSA	22	Q. But I'm just trying to test with you some propositions
23	table the BOSA table we can find in Prof McQuillan's	23	based on pure arithmetical value and see whether you
24	report, appendix V.	24	accept. You may not agree with the underlying
25	So that's ten threads, based on ten threads?	25	assumption but let's leave that to one side.
	Page 6		Page 8
1	Page 6 A. BOSA calculate up to ten threads.	1	Page 8 A. No, I think that's not an assumption. When you went to
1 2	-	1 2	-
	A. BOSA calculate up to ten threads.		A. No, I think that's not an assumption. When you went to
2	<ul><li>A. BOSA calculate up to ten threads.</li><li>Q. Up to ten threads, yes. Whether it's ten threads or</li></ul>	2	A. No, I think that's not an assumption. When you went to compare experimental data with theoretical or calculated
2 3	<ul><li>A. BOSA calculate up to ten threads.</li><li>Q. Up to ten threads, yes. Whether it's ten threads or 11 threads, a 30 per cent engagement of ten threads</li></ul>	2 3	A. No, I think that's not an assumption. When you went to compare experimental data with theoretical or calculated data, you need to actually plot what has been done in the experiment. You cannot mix up the two sets of data in such a way for a fair comparison.
2 3 4	<ul><li>A. BOSA calculate up to ten threads.</li><li>Q. Up to ten threads, yes. Whether it's ten threads or 11 threads, a 30 per cent engagement of ten threads would be three threads, do you accept that,</li></ul>	2 3 4	A. No, I think that's not an assumption. When you went to compare experimental data with theoretical or calculated data, you need to actually plot what has been done in the experiment. You cannot mix up the two sets of data
2 3 4 5	<ul><li>A. BOSA calculate up to ten threads.</li><li>Q. Up to ten threads, yes. Whether it's ten threads or 11 threads, a 30 per cent engagement of ten threads would be three threads, do you accept that, arithmetically?</li></ul>	2 3 4 5	A. No, I think that's not an assumption. When you went to compare experimental data with theoretical or calculated data, you need to actually plot what has been done in the experiment. You cannot mix up the two sets of data in such a way for a fair comparison.
2 3 4 5 6	<ul> <li>A. BOSA calculate up to ten threads.</li> <li>Q. Up to ten threads, yes. Whether it's ten threads or 11 threads, a 30 per cent engagement of ten threads would be three threads, do you accept that, arithmetically?</li> <li>A. 10 times 0.33.</li> </ul>	2 3 4 5 6	<ul><li>A. No, I think that's not an assumption. When you went to compare experimental data with theoretical or calculated data, you need to actually plot what has been done in the experiment. You cannot mix up the two sets of data in such a way for a fair comparison.</li><li>Q. Can I proceed to the next open circle, at I think</li></ul>
2 3 4 5 6 7	<ul> <li>A. BOSA calculate up to ten threads.</li> <li>Q. Up to ten threads, yes. Whether it's ten threads or 11 threads, a 30 per cent engagement of ten threads would be three threads, do you accept that, arithmetically?</li> <li>A. 10 times 0.33.</li> <li>Q. Yes, and 10 times even if you apply 11 threads,</li> </ul>	2 3 4 5 6 7	<ul> <li>A. No, I think that's not an assumption. When you went to compare experimental data with theoretical or calculated data, you need to actually plot what has been done in the experiment. You cannot mix up the two sets of data in such a way for a fair comparison.</li> <li>Q. Can I proceed to the next open circle, at I think it's 40 per cent engagement in the actual test</li> </ul>
2 3 4 5 6 7 8	<ul> <li>A. BOSA calculate up to ten threads.</li> <li>Q. Up to ten threads, yes. Whether it's ten threads or 11 threads, a 30 per cent engagement of ten threads would be three threads, do you accept that, arithmetically?</li> <li>A. 10 times 0.33.</li> <li>Q. Yes, and 10 times even if you apply 11 threads, it would be 3.3 threads?</li> <li>A. Correct.</li> <li>Q. So, on that basis, would you accept that if we convert</li> </ul>	2 3 4 5 6 7 8	<ul> <li>A. No, I think that's not an assumption. When you went to compare experimental data with theoretical or calculated data, you need to actually plot what has been done in the experiment. You cannot mix up the two sets of data in such a way for a fair comparison.</li> <li>Q. Can I proceed to the next open circle, at I think it's 40 per cent engagement in the actual test remember? 50, sorry.</li> <li>A. They denote it as 50.</li> <li>Q. 50. If you apply 50 per cent to ten threads, that would</li> </ul>
2 3 4 5 6 7 8 9 10 11	<ul> <li>A. BOSA calculate up to ten threads.</li> <li>Q. Up to ten threads, yes. Whether it's ten threads or 11 threads, a 30 per cent engagement of ten threads would be three threads, do you accept that, arithmetically?</li> <li>A. 10 times 0.33.</li> <li>Q. Yes, and 10 times even if you apply 11 threads, it would be 3.3 threads?</li> <li>A. Correct.</li> <li>Q. So, on that basis, would you accept that if we convert the percentage engagement into number of threads in this</li> </ul>	2 3 4 5 6 7 8 9 10 11	<ul> <li>A. No, I think that's not an assumption. When you went to compare experimental data with theoretical or calculated data, you need to actually plot what has been done in the experiment. You cannot mix up the two sets of data in such a way for a fair comparison.</li> <li>Q. Can I proceed to the next open circle, at I think it's 40 per cent engagement in the actual test remember? 50, sorry.</li> <li>A. They denote it as 50.</li> <li>Q. 50. If you apply 50 per cent to ten threads, that would give you five threads, numerically?</li> </ul>
2 3 4 5 6 7 8 9 10 11 12	<ul> <li>A. BOSA calculate up to ten threads.</li> <li>Q. Up to ten threads, yes. Whether it's ten threads or 11 threads, a 30 per cent engagement of ten threads would be three threads, do you accept that, arithmetically?</li> <li>A. 10 times 0.33.</li> <li>Q. Yes, and 10 times even if you apply 11 threads, it would be 3.3 threads?</li> <li>A. Correct.</li> <li>Q. So, on that basis, would you accept that if we convert the percentage engagement into number of threads in this way, the open circle above the number 4 should be moved</li> </ul>	2 3 4 5 6 7 8 9 10 11	<ul> <li>A. No, I think that's not an assumption. When you went to compare experimental data with theoretical or calculated data, you need to actually plot what has been done in the experiment. You cannot mix up the two sets of data in such a way for a fair comparison.</li> <li>Q. Can I proceed to the next open circle, at I think it's 40 per cent engagement in the actual test remember? 50, sorry.</li> <li>A. They denote it as 50.</li> <li>Q. 50. If you apply 50 per cent to ten threads, that would give you five threads, numerically?</li> <li>A. Correct.</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13	<ul> <li>A. BOSA calculate up to ten threads.</li> <li>Q. Up to ten threads, yes. Whether it's ten threads or 11 threads, a 30 per cent engagement of ten threads would be three threads, do you accept that, arithmetically?</li> <li>A. 10 times 0.33.</li> <li>Q. Yes, and 10 times even if you apply 11 threads, it would be 3.3 threads?</li> <li>A. Correct.</li> <li>Q. So, on that basis, would you accept that if we convert the percentage engagement into number of threads in this way, the open circle above the number 4 should be moved sideways a bit to the left, to be above 3 or 3.3?</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13	<ul> <li>A. No, I think that's not an assumption. When you went to compare experimental data with theoretical or calculated data, you need to actually plot what has been done in the experiment. You cannot mix up the two sets of data in such a way for a fair comparison.</li> <li>Q. Can I proceed to the next open circle, at I think it's 40 per cent engagement in the actual test remember? 50, sorry.</li> <li>A. They denote it as 50.</li> <li>Q. 50. If you apply 50 per cent to ten threads, that would give you five threads, numerically?</li> <li>A. Correct.</li> <li>Q. Even if you proceed on the basis that it has 11 threads,</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14	<ul> <li>A. BOSA calculate up to ten threads.</li> <li>Q. Up to ten threads, yes. Whether it's ten threads or 11 threads, a 30 per cent engagement of ten threads would be three threads, do you accept that, arithmetically?</li> <li>A. 10 times 0.33.</li> <li>Q. Yes, and 10 times even if you apply 11 threads, it would be 3.3 threads?</li> <li>A. Correct.</li> <li>Q. So, on that basis, would you accept that if we convert the percentage engagement into number of threads in this way, the open circle above the number 4 should be moved sideways a bit to the left, to be above 3 or 3.3?</li> <li>A. In terms of research, when you try to plot the</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14	<ul> <li>A. No, I think that's not an assumption. When you went to compare experimental data with theoretical or calculated data, you need to actually plot what has been done in the experiment. You cannot mix up the two sets of data in such a way for a fair comparison.</li> <li>Q. Can I proceed to the next open circle, at I think it's 40 per cent engagement in the actual test remember? 50, sorry.</li> <li>A. They denote it as 50.</li> <li>Q. 50. If you apply 50 per cent to ten threads, that would give you five threads, numerically?</li> <li>A. Correct.</li> <li>Q. Even if you proceed on the basis that it has 11 threads, 50 per cent of 11 threads would be 5.5 threads,</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15	<ul> <li>A. BOSA calculate up to ten threads.</li> <li>Q. Up to ten threads, yes. Whether it's ten threads or 11 threads, a 30 per cent engagement of ten threads would be three threads, do you accept that, arithmetically?</li> <li>A. 10 times 0.33.</li> <li>Q. Yes, and 10 times even if you apply 11 threads, it would be 3.3 threads?</li> <li>A. Correct.</li> <li>Q. So, on that basis, would you accept that if we convert the percentage engagement into number of threads in this way, the open circle above the number 4 should be moved sideways a bit to the left, to be above 3 or 3.3?</li> <li>A. In terms of research, when you try to plot the experimental data to compare the calculated data, the</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15	<ul> <li>A. No, I think that's not an assumption. When you went to compare experimental data with theoretical or calculated data, you need to actually plot what has been done in the experiment. You cannot mix up the two sets of data in such a way for a fair comparison.</li> <li>Q. Can I proceed to the next open circle, at I think it's 40 per cent engagement in the actual test remember? 50, sorry.</li> <li>A. They denote it as 50.</li> <li>Q. 50. If you apply 50 per cent to ten threads, that would give you five threads, numerically?</li> <li>A. Correct.</li> <li>Q. Even if you proceed on the basis that it has 11 threads, 50 per cent of 11 threads would be 5.5 threads, arithmetically?</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	<ul> <li>A. BOSA calculate up to ten threads.</li> <li>Q. Up to ten threads, yes. Whether it's ten threads or 11 threads, a 30 per cent engagement of ten threads would be three threads, do you accept that, arithmetically?</li> <li>A. 10 times 0.33.</li> <li>Q. Yes, and 10 times even if you apply 11 threads, it would be 3.3 threads?</li> <li>A. Correct.</li> <li>Q. So, on that basis, would you accept that if we convert the percentage engagement into number of threads in this way, the open circle above the number 4 should be moved sideways a bit to the left, to be above 3 or 3.3?</li> <li>A. In terms of research, when you try to plot the experimental data to compare the calculated data, the way you plot it is you should plot what you have</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	<ul> <li>A. No, I think that's not an assumption. When you went to compare experimental data with theoretical or calculated data, you need to actually plot what has been done in the experiment. You cannot mix up the two sets of data in such a way for a fair comparison.</li> <li>Q. Can I proceed to the next open circle, at I think it's 40 per cent engagement in the actual test remember? 50, sorry.</li> <li>A. They denote it as 50.</li> <li>Q. 50. If you apply 50 per cent to ten threads, that would give you five threads, numerically?</li> <li>A. Correct.</li> <li>Q. Even if you proceed on the basis that it has 11 threads, 50 per cent of 11 threads would be 5.5 threads, arithmetically?</li> <li>A. Correct.</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	<ul> <li>A. BOSA calculate up to ten threads.</li> <li>Q. Up to ten threads, yes. Whether it's ten threads or 11 threads, a 30 per cent engagement of ten threads would be three threads, do you accept that, arithmetically?</li> <li>A. 10 times 0.33.</li> <li>Q. Yes, and 10 times even if you apply 11 threads, it would be 3.3 threads?</li> <li>A. Correct.</li> <li>Q. So, on that basis, would you accept that if we convert the percentage engagement into number of threads in this way, the open circle above the number 4 should be moved sideways a bit to the left, to be above 3 or 3.3?</li> <li>A. In terms of research, when you try to plot the experimental data to compare the calculated data, the way you plot it is you should plot what you have actually done in the experiment. That's why I told you</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	<ul> <li>A. No, I think that's not an assumption. When you went to compare experimental data with theoretical or calculated data, you need to actually plot what has been done in the experiment. You cannot mix up the two sets of data in such a way for a fair comparison.</li> <li>Q. Can I proceed to the next open circle, at I think it's 40 per cent engagement in the actual test remember? 50, sorry.</li> <li>A. They denote it as 50.</li> <li>Q. 50. If you apply 50 per cent to ten threads, that would give you five threads, numerically?</li> <li>A. Correct.</li> <li>Q. Even if you proceed on the basis that it has 11 threads, 50 per cent of 11 threads would be 5.5 threads, arithmetically?</li> <li>A. Correct.</li> <li>Q. So proceeding on that basis, rather than looking at the</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	<ul> <li>A. BOSA calculate up to ten threads.</li> <li>Q. Up to ten threads, yes. Whether it's ten threads or 11 threads, a 30 per cent engagement of ten threads would be three threads, do you accept that, arithmetically?</li> <li>A. 10 times 0.33.</li> <li>Q. Yes, and 10 times even if you apply 11 threads, it would be 3.3 threads?</li> <li>A. Correct.</li> <li>Q. So, on that basis, would you accept that if we convert the percentage engagement into number of threads in this way, the open circle above the number 4 should be moved sideways a bit to the left, to be above 3 or 3.3?</li> <li>A. In terms of research, when you try to plot the experimental data to compare the calculated data, the way you plot it is you should plot what you have actually done in the experiment. That's why I told you earlier is I looked at the picture that they</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	<ul> <li>A. No, I think that's not an assumption. When you went to compare experimental data with theoretical or calculated data, you need to actually plot what has been done in the experiment. You cannot mix up the two sets of data in such a way for a fair comparison.</li> <li>Q. Can I proceed to the next open circle, at I think it's 40 per cent engagement in the actual test remember? 50, sorry.</li> <li>A. They denote it as 50.</li> <li>Q. 50. If you apply 50 per cent to ten threads, that would give you five threads, numerically?</li> <li>A. Correct.</li> <li>Q. Even if you proceed on the basis that it has 11 threads, 50 per cent of 11 threads would be 5.5 threads, arithmetically?</li> <li>A. Correct.</li> <li>Q. So proceeding on that basis, rather than looking at the photographs, the open circle above the number 6 would</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	<ul> <li>A. BOSA calculate up to ten threads.</li> <li>Q. Up to ten threads, yes. Whether it's ten threads or 11 threads, a 30 per cent engagement of ten threads would be three threads, do you accept that, arithmetically?</li> <li>A. 10 times 0.33.</li> <li>Q. Yes, and 10 times even if you apply 11 threads, it would be 3.3 threads?</li> <li>A. Correct.</li> <li>Q. So, on that basis, would you accept that if we convert the percentage engagement into number of threads in this way, the open circle above the number 4 should be moved sideways a bit to the left, to be above 3 or 3.3?</li> <li>A. In terms of research, when you try to plot the experimental data to compare the calculated data, the way you plot it is you should plot what you have actually done in the experiment. That's why I told you earlier is I looked at the picture that they prepared, that they denote as 30 per cent threads.</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	<ul> <li>A. No, I think that's not an assumption. When you went to compare experimental data with theoretical or calculated data, you need to actually plot what has been done in the experiment. You cannot mix up the two sets of data in such a way for a fair comparison.</li> <li>Q. Can I proceed to the next open circle, at I think it's 40 per cent engagement in the actual test remember? 50, sorry.</li> <li>A. They denote it as 50.</li> <li>Q. 50. If you apply 50 per cent to ten threads, that would give you five threads, numerically?</li> <li>A. Correct.</li> <li>Q. Even if you proceed on the basis that it has 11 threads, 50 per cent of 11 threads would be 5.5 threads, arithmetically?</li> <li>A. Correct.</li> <li>Q. So proceeding on that basis, rather than looking at the photographs, the open circle above the number 6 would have to be moved sideways towards the left, on that</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	<ul> <li>A. BOSA calculate up to ten threads.</li> <li>Q. Up to ten threads, yes. Whether it's ten threads or 11 threads, a 30 per cent engagement of ten threads would be three threads, do you accept that, arithmetically?</li> <li>A. 10 times 0.33.</li> <li>Q. Yes, and 10 times even if you apply 11 threads, it would be 3.3 threads?</li> <li>A. Correct.</li> <li>Q. So, on that basis, would you accept that if we convert the percentage engagement into number of threads in this way, the open circle above the number 4 should be moved sideways a bit to the left, to be above 3 or 3.3?</li> <li>A. In terms of research, when you try to plot the experimental data to compare the calculated data, the way you plot it is you should plot what you have actually done in the experiment. That's why I told you earlier is I looked at the picture that they prepared, that they denote as 30 per cent threads. I looked at that bar and I count it, there are four</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	<ul> <li>A. No, I think that's not an assumption. When you went to compare experimental data with theoretical or calculated data, you need to actually plot what has been done in the experiment. You cannot mix up the two sets of data in such a way for a fair comparison.</li> <li>Q. Can I proceed to the next open circle, at I think it's 40 per cent engagement in the actual test remember? 50, sorry.</li> <li>A. They denote it as 50.</li> <li>Q. 50. If you apply 50 per cent to ten threads, that would give you five threads, numerically?</li> <li>A. Correct.</li> <li>Q. Even if you proceed on the basis that it has 11 threads, 50 per cent of 11 threads would be 5.5 threads, arithmetically?</li> <li>A. Correct.</li> <li>Q. So proceeding on that basis, rather than looking at the photographs, the open circle above the number 6 would have to be moved sideways towards the left, on that basis?</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	<ul> <li>A. BOSA calculate up to ten threads.</li> <li>Q. Up to ten threads, yes. Whether it's ten threads or 11 threads, a 30 per cent engagement of ten threads would be three threads, do you accept that, arithmetically?</li> <li>A. 10 times 0.33.</li> <li>Q. Yes, and 10 times even if you apply 11 threads, it would be 3.3 threads?</li> <li>A. Correct.</li> <li>Q. So, on that basis, would you accept that if we convert the percentage engagement into number of threads in this way, the open circle above the number 4 should be moved sideways a bit to the left, to be above 3 or 3.3?</li> <li>A. In terms of research, when you try to plot the experimental data to compare the calculated data, the way you plot it is you should plot what you have actually done in the experiment. That's why I told you earlier is I looked at the picture that they prepared, that they denote as 30 per cent.</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	<ul> <li>A. No, I think that's not an assumption. When you went to compare experimental data with theoretical or calculated data, you need to actually plot what has been done in the experiment. You cannot mix up the two sets of data in such a way for a fair comparison.</li> <li>Q. Can I proceed to the next open circle, at I think it's 40 per cent engagement in the actual test remember? 50, sorry.</li> <li>A. They denote it as 50.</li> <li>Q. 50. If you apply 50 per cent to ten threads, that would give you five threads, numerically?</li> <li>A. Correct.</li> <li>Q. Even if you proceed on the basis that it has 11 threads, 50 per cent of 11 threads would be 5.5 threads, arithmetically?</li> <li>A. Correct.</li> <li>Q. So proceeding on that basis, rather than looking at the photographs, the open circle above the number 6 would have to be moved sideways towards the left, on that basis?</li> <li>A. Again, as what I said, you try to mix up the theoretical</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>A. BOSA calculate up to ten threads.</li> <li>Q. Up to ten threads, yes. Whether it's ten threads or 11 threads, a 30 per cent engagement of ten threads would be three threads, do you accept that, arithmetically?</li> <li>A. 10 times 0.33.</li> <li>Q. Yes, and 10 times even if you apply 11 threads, it would be 3.3 threads?</li> <li>A. Correct.</li> <li>Q. So, on that basis, would you accept that if we convert the percentage engagement into number of threads in this way, the open circle above the number 4 should be moved sideways a bit to the left, to be above 3 or 3.3?</li> <li>A. In terms of research, when you try to plot the experimental data to compare the calculated data, the way you plot it is you should plot what you have actually done in the experiment. That's why I told you earlier is I looked at the picture that they prepared, that they denote as 30 per cent threads. I looked at that bar and I count it, there are four threads on it. They call it 30 per cent.</li> <li>Q. So, basically, what you are telling us is you did not do</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>A. No, I think that's not an assumption. When you went to compare experimental data with theoretical or calculated data, you need to actually plot what has been done in the experiment. You cannot mix up the two sets of data in such a way for a fair comparison.</li> <li>Q. Can I proceed to the next open circle, at I think it's 40 per cent engagement in the actual test remember? 50, sorry.</li> <li>A. They denote it as 50.</li> <li>Q. 50. If you apply 50 per cent to ten threads, that would give you five threads, numerically?</li> <li>A. Correct.</li> <li>Q. Even if you proceed on the basis that it has 11 threads, 50 per cent of 11 threads would be 5.5 threads, arithmetically?</li> <li>A. Correct.</li> <li>Q. So proceeding on that basis, rather than looking at the photographs, the open circle above the number 6 would have to be moved sideways towards the left, on that basis?</li> <li>A. Again, as what I said, you try to mix up the theoretical and the experimental results, and that's not the correct</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	<ul> <li>A. BOSA calculate up to ten threads.</li> <li>Q. Up to ten threads, yes. Whether it's ten threads or 11 threads, a 30 per cent engagement of ten threads would be three threads, do you accept that, arithmetically?</li> <li>A. 10 times 0.33.</li> <li>Q. Yes, and 10 times even if you apply 11 threads, it would be 3.3 threads?</li> <li>A. Correct.</li> <li>Q. So, on that basis, would you accept that if we convert the percentage engagement into number of threads in this way, the open circle above the number 4 should be moved sideways a bit to the left, to be above 3 or 3.3?</li> <li>A. In terms of research, when you try to plot the experimental data to compare the calculated data, the way you plot it is you should plot what you have actually done in the experiment. That's why I told you earlier is I looked at the picture that they prepared, that they denote as 30 per cent threads. I looked at that bar and I count it, there are four threads on it. They call it 30 per cent.</li> <li>Q. So, basically, what you are telling us is you did not do the conversion by an arithmetical process of multiplying</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	<ul> <li>A. No, I think that's not an assumption. When you went to compare experimental data with theoretical or calculated data, you need to actually plot what has been done in the experiment. You cannot mix up the two sets of data in such a way for a fair comparison.</li> <li>Q. Can I proceed to the next open circle, at I think it's 40 per cent engagement in the actual test remember? 50, sorry.</li> <li>A. They denote it as 50.</li> <li>Q. 50. If you apply 50 per cent to ten threads, that would give you five threads, numerically?</li> <li>A. Correct.</li> <li>Q. Even if you proceed on the basis that it has 11 threads, 50 per cent of 11 threads would be 5.5 threads, arithmetically?</li> <li>A. Correct.</li> <li>Q. So proceeding on that basis, rather than looking at the photographs, the open circle above the number 6 would have to be moved sideways towards the left, on that basis?</li> <li>A. Again, as what I said, you try to mix up the theoretical and the experimental results, and that's not the correct way to research on a certain phenomena, when you perform</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>A. BOSA calculate up to ten threads.</li> <li>Q. Up to ten threads, yes. Whether it's ten threads or 11 threads, a 30 per cent engagement of ten threads would be three threads, do you accept that, arithmetically?</li> <li>A. 10 times 0.33.</li> <li>Q. Yes, and 10 times even if you apply 11 threads, it would be 3.3 threads?</li> <li>A. Correct.</li> <li>Q. So, on that basis, would you accept that if we convert the percentage engagement into number of threads in this way, the open circle above the number 4 should be moved sideways a bit to the left, to be above 3 or 3.3?</li> <li>A. In terms of research, when you try to plot the experimental data to compare the calculated data, the way you plot it is you should plot what you have actually done in the experiment. That's why I told you earlier is I looked at the picture that they prepared, that they denote as 30 per cent threads. I looked at that bar and I count it, there are four threads on it. They call it 30 per cent.</li> <li>Q. So, basically, what you are telling us is you did not do</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>A. No, I think that's not an assumption. When you went to compare experimental data with theoretical or calculated data, you need to actually plot what has been done in the experiment. You cannot mix up the two sets of data in such a way for a fair comparison.</li> <li>Q. Can I proceed to the next open circle, at I think it's 40 per cent engagement in the actual test remember? 50, sorry.</li> <li>A. They denote it as 50.</li> <li>Q. 50. If you apply 50 per cent to ten threads, that would give you five threads, numerically?</li> <li>A. Correct.</li> <li>Q. Even if you proceed on the basis that it has 11 threads, 50 per cent of 11 threads would be 5.5 threads, arithmetically?</li> <li>A. Correct.</li> <li>Q. So proceeding on that basis, rather than looking at the photographs, the open circle above the number 6 would have to be moved sideways towards the left, on that basis?</li> <li>A. Again, as what I said, you try to mix up the theoretical and the experimental results, and that's not the correct</li> </ul>

1	Page 9		Page 11
1 1	Q. I did say "on that basis".	1	A. Yes.
2	A. So you are mixing up the basis.	2	Q. But, if you replot the graphs, then you can see that the
3	Q. I know. You can assume that I am as wrong as I possibly	3	position of the circles would have changed, and the odd
4	can, but on the wrong basis then the circle above the	4	or strange feature that you described in the transcript
5	number 6 would have to be moved sideways, to the left?	5	no longer featured; would you accept that?
6	A. Correct.	6	A. No, I don't.
7	Q. By saying "correct", I know you don't mean to accept the	7	Q. Right. Why was that?
8	underlying premise that I put to you the question, but	8	A. Steel now I think Mr So would want to make a fair
9	as I say I'm just putting to you the arithmetical	9	comparison. The tensile strength of the experimental
10	consequences.	10	data are based on 500 grade steel. The solid circle
11	A. Or your logic of plotting the data.	11	right now shown on the graph, on both graphs, are based
12	Q. Then we come to the next dot, open dot, which is at	12	on 460 steel.
13	60 per cent engagement. 60 per cent engagement, on the	13	Q. When you said "experimental data"
14	basis of a ten-thread bar, would be six threads?	14	A. No, the calculated data.
15	A. Correct.	15	Q. Calculated data is based on 460?
16	Q. Even if it's 11 threads, it would be 6.6 threads?	16	A. 460, right, and the experimental data are based on 500.
17	A. Yes.	17	Q. So there would be a gap between them, which is what you
18	Q. Then, on that basis, again, that circle, that open	18	expect to see?
19	circle, somewhere between 6 and 8, marked "B", which you	19	A. Between the two sets of theoretical data, there should
20	intended to denote the 60 per cent breakage, would have	20	be a gap.
21	to be moved again sideways to the left?	21	Q. Which is there.
22	A. Very slightly.	22	A. No, no. This one we are comparing experimental data to
23	Q. Slightly to the left.	23	calculated data.
24	Now, could I show to you what Mr Southward has done,	24	Q. Yes, I know, and there should be a gap between
25	the next slide which we submitted to the Commission this	25	experimental, actual pulling out, and calculated,
	Page 10		Page 12
1	morning.	1	theoretical; correct?
-			
2	If you look at the screen, Professor	2	A. That's right.
2 3	A. Yes.	2 3	<ul><li>A. That's right.</li><li>Q. So you would expect to see a gap between solid circle</li></ul>
	<ul><li>A. Yes.</li><li>Q this is what Mr Southward has done overnight, by</li></ul>		A. That's right.
3	<ul><li>A. Yes.</li><li>Q this is what Mr Southward has done overnight, by replotting your graph, by applying the percentage to</li></ul>	3	<ul><li>A. That's right.</li><li>Q. So you would expect to see a gap between solid circle and hollow circle for each value of engagement; correct?</li><li>A. Correct.</li></ul>
3 4 5 6	<ul><li>A. Yes.</li><li>Q this is what Mr Southward has done overnight, by replotting your graph, by applying the percentage to a thread length of ten threads; right?</li></ul>	3 4 5 6	<ul><li>A. That's right.</li><li>Q. So you would expect to see a gap between solid circle and hollow circle for each value of engagement; correct?</li><li>A. Correct.</li><li>Q. But that is what you see, for each value of number of</li></ul>
3 4 5	<ul><li>A. Yes.</li><li>Q this is what Mr Southward has done overnight, by replotting your graph, by applying the percentage to a thread length of ten threads; right?</li><li>A. Okay.</li></ul>	3 4 5 6 7	<ul><li>A. That's right.</li><li>Q. So you would expect to see a gap between solid circle and hollow circle for each value of engagement; correct?</li><li>A. Correct.</li><li>Q. But that is what you see, for each value of number of threads engagement, you see one value for theoretical,</li></ul>
3 4 5 6 7 8	<ul><li>A. Yes.</li><li>Q this is what Mr Southward has done overnight, by replotting your graph, by applying the percentage to a thread length of ten threads; right?</li><li>A. Okay.</li><li>Q. Then the result would be, as I have just explored with</li></ul>	3 4 5 6 7 8	<ul> <li>A. That's right.</li> <li>Q. So you would expect to see a gap between solid circle and hollow circle for each value of engagement; correct?</li> <li>A. Correct.</li> <li>Q. But that is what you see, for each value of number of threads engagement, you see one value for theoretical, calculated value, and one value for actual pulling-out</li> </ul>
3 4 5 6 7 8 9	<ul> <li>A. Yes.</li> <li>Q this is what Mr Southward has done overnight, by replotting your graph, by applying the percentage to a thread length of ten threads; right?</li> <li>A. Okay.</li> <li>Q. Then the result would be, as I have just explored with you, a moving sideways to the left of the circles</li> </ul>	3 4 5 6 7 8 9	<ul><li>A. That's right.</li><li>Q. So you would expect to see a gap between solid circle and hollow circle for each value of engagement; correct?</li><li>A. Correct.</li><li>Q. But that is what you see, for each value of number of threads engagement, you see one value for theoretical, calculated value, and one value for actual pulling-out test results?</li></ul>
3 4 5 6 7 8 9 10	<ul> <li>A. Yes.</li> <li>Q this is what Mr Southward has done overnight, by replotting your graph, by applying the percentage to a thread length of ten threads; right?</li> <li>A. Okay.</li> <li>Q. Then the result would be, as I have just explored with you, a moving sideways to the left of the circles depicting 30 per cent engagement, 50 per cent engagement</li> </ul>	3 4 5 6 7 8 9 10	<ul> <li>A. That's right.</li> <li>Q. So you would expect to see a gap between solid circle and hollow circle for each value of engagement; correct?</li> <li>A. Correct.</li> <li>Q. But that is what you see, for each value of number of threads engagement, you see one value for theoretical, calculated value, and one value for actual pulling-out test results?</li> <li>A. When you mention you see a gap between theoretical data</li> </ul>
3 4 5 6 7 8 9 10 11	<ul> <li>A. Yes.</li> <li>Q this is what Mr Southward has done overnight, by replotting your graph, by applying the percentage to a thread length of ten threads; right?</li> <li>A. Okay.</li> <li>Q. Then the result would be, as I have just explored with you, a moving sideways to the left of the circles depicting 30 per cent engagement, 50 per cent engagement and 60 per cent engagement. You understand the logic?</li> </ul>	3 4 5 6 7 8 9 10 11	<ul> <li>A. That's right.</li> <li>Q. So you would expect to see a gap between solid circle and hollow circle for each value of engagement; correct?</li> <li>A. Correct.</li> <li>Q. But that is what you see, for each value of number of threads engagement, you see one value for theoretical, calculated value, and one value for actual pulling-out test results?</li> <li>A. When you mention you see a gap between theoretical data and experimental data, the gap can go either way. Like,</li> </ul>
3 4 5 6 7 8 9 10 11 12	<ul> <li>A. Yes.</li> <li>Q this is what Mr Southward has done overnight, by replotting your graph, by applying the percentage to a thread length of ten threads; right?</li> <li>A. Okay.</li> <li>Q. Then the result would be, as I have just explored with you, a moving sideways to the left of the circles depicting 30 per cent engagement, 50 per cent engagement and 60 per cent engagement. You understand the logic? You may not agree with the logic but you understand this</li> </ul>	3 4 5 6 7 8 9 10 11 12	<ul> <li>A. That's right.</li> <li>Q. So you would expect to see a gap between solid circle and hollow circle for each value of engagement; correct?</li> <li>A. Correct.</li> <li>Q. But that is what you see, for each value of number of threads engagement, you see one value for theoretical, calculated value, and one value for actual pulling-out test results?</li> <li>A. When you mention you see a gap between theoretical data and experimental data, the gap can go either way. Like, for example, I can create a model myself and then I run</li> </ul>
3 4 5 6 7 8 9 10 11 12 13	<ul> <li>A. Yes.</li> <li>Q this is what Mr Southward has done overnight, by replotting your graph, by applying the percentage to a thread length of ten threads; right?</li> <li>A. Okay.</li> <li>Q. Then the result would be, as I have just explored with you, a moving sideways to the left of the circles depicting 30 per cent engagement, 50 per cent engagement and 60 per cent engagement. You understand the logic?</li> <li>You may not agree with the logic but you understand this logic?</li> </ul>	3 4 5 6 7 8 9 10 11 12 13	<ul> <li>A. That's right.</li> <li>Q. So you would expect to see a gap between solid circle and hollow circle for each value of engagement; correct?</li> <li>A. Correct.</li> <li>Q. But that is what you see, for each value of number of threads engagement, you see one value for theoretical, calculated value, and one value for actual pulling-out test results?</li> <li>A. When you mention you see a gap between theoretical data and experimental data, the gap can go either way. Like, for example, I can create a model myself and then I run experiment. If the experiment match my model</li> </ul>
3 4 5 6 7 8 9 10 11 12 13 14	<ul> <li>A. Yes.</li> <li>Q this is what Mr Southward has done overnight, by replotting your graph, by applying the percentage to a thread length of ten threads; right?</li> <li>A. Okay.</li> <li>Q. Then the result would be, as I have just explored with you, a moving sideways to the left of the circles depicting 30 per cent engagement, 50 per cent engagement and 60 per cent engagement. You understand the logic?</li> <li>A. I understand.</li> </ul>	3 4 5 6 7 8 9 10 11 12 13 14	<ul> <li>A. That's right.</li> <li>Q. So you would expect to see a gap between solid circle and hollow circle for each value of engagement; correct?</li> <li>A. Correct.</li> <li>Q. But that is what you see, for each value of number of threads engagement, you see one value for theoretical, calculated value, and one value for actual pulling-out test results?</li> <li>A. When you mention you see a gap between theoretical data and experimental data, the gap can go either way. Like, for example, I can create a model myself and then I run experiment. If the experiment match my model 100 per cent, that's probably a good indicator my model</li> </ul>
3 4 5 6 7 8 9 10 11 12 13 14 15	<ul> <li>A. Yes.</li> <li>Q this is what Mr Southward has done overnight, by replotting your graph, by applying the percentage to a thread length of ten threads; right?</li> <li>A. Okay.</li> <li>Q. Then the result would be, as I have just explored with you, a moving sideways to the left of the circles depicting 30 per cent engagement, 50 per cent engagement and 60 per cent engagement. You understand the logic?</li> <li>A. I understand.</li> <li>Q. Then you can see that there is a pattern whereby for the</li> </ul>	3 4 5 6 7 8 9 10 11 12 13 14 15	<ul> <li>A. That's right.</li> <li>Q. So you would expect to see a gap between solid circle and hollow circle for each value of engagement; correct?</li> <li>A. Correct.</li> <li>Q. But that is what you see, for each value of number of threads engagement, you see one value for theoretical, calculated value, and one value for actual pulling-out test results?</li> <li>A. When you mention you see a gap between theoretical data and experimental data, the gap can go either way. Like, for example, I can create a model myself and then I run experiment. If the experiment match my model 100 per cent, that's probably a good indicator my model is correct. On the other hand now is, the experimental</li> </ul>
3 4 5 6 7 8 9 10 11 12 13 14 15 16	<ul> <li>A. Yes.</li> <li>Q this is what Mr Southward has done overnight, by replotting your graph, by applying the percentage to a thread length of ten threads; right?</li> <li>A. Okay.</li> <li>Q. Then the result would be, as I have just explored with you, a moving sideways to the left of the circles depicting 30 per cent engagement, 50 per cent engagement and 60 per cent engagement. You understand the logic? You may not agree with the logic but you understand this logic?</li> <li>A. I understand.</li> <li>Q. Then you can see that there is a pattern whereby for the theoretical line and the line represented by the actual</li> </ul>	3 4 5 6 7 8 9 10 11 12 13 14 15 16	<ul> <li>A. That's right.</li> <li>Q. So you would expect to see a gap between solid circle and hollow circle for each value of engagement; correct?</li> <li>A. Correct.</li> <li>Q. But that is what you see, for each value of number of threads engagement, you see one value for theoretical, calculated value, and one value for actual pulling-out test results?</li> <li>A. When you mention you see a gap between theoretical data and experimental data, the gap can go either way. Like, for example, I can create a model myself and then I run experiment. If the experiment match my model 100 per cent, that's probably a good indicator my model is correct. On the other hand now is, the experimental data, in the usual way in research, may not match</li> </ul>
3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	<ul> <li>A. Yes.</li> <li>Q this is what Mr Southward has done overnight, by replotting your graph, by applying the percentage to a thread length of ten threads; right?</li> <li>A. Okay.</li> <li>Q. Then the result would be, as I have just explored with you, a moving sideways to the left of the circles depicting 30 per cent engagement, 50 per cent engagement and 60 per cent engagement. You understand the logic? You may not agree with the logic but you understand this logic?</li> <li>A. I understand.</li> <li>Q. Then you can see that there is a pattern whereby for the theoretical line and the line represented by the actual result, the two lines are similar in shape?</li> </ul>	3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	<ul> <li>A. That's right.</li> <li>Q. So you would expect to see a gap between solid circle and hollow circle for each value of engagement; correct?</li> <li>A. Correct.</li> <li>Q. But that is what you see, for each value of number of threads engagement, you see one value for theoretical, calculated value, and one value for actual pulling-out test results?</li> <li>A. When you mention you see a gap between theoretical data and experimental data, the gap can go either way. Like, for example, I can create a model myself and then I run experiment. If the experiment match my model 100 per cent, that's probably a good indicator my model is correct. On the other hand now is, the experimental data, in the usual way in research, may not match 100 per cent to your theoretical data. Then the other</li> </ul>
3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	<ul> <li>A. Yes.</li> <li>Q this is what Mr Southward has done overnight, by replotting your graph, by applying the percentage to a thread length of ten threads; right?</li> <li>A. Okay.</li> <li>Q. Then the result would be, as I have just explored with you, a moving sideways to the left of the circles depicting 30 per cent engagement, 50 per cent engagement and 60 per cent engagement. You understand the logic? You may not agree with the logic but you understand this logic?</li> <li>A. I understand.</li> <li>Q. Then you can see that there is a pattern whereby for the theoretical line and the line represented by the actual result, the two lines are similar in shape?</li> <li>A. What do you mean by "two lines"? We see only one line</li> </ul>	3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	<ul> <li>A. That's right.</li> <li>Q. So you would expect to see a gap between solid circle and hollow circle for each value of engagement; correct?</li> <li>A. Correct.</li> <li>Q. But that is what you see, for each value of number of threads engagement, you see one value for theoretical, calculated value, and one value for actual pulling-out test results?</li> <li>A. When you mention you see a gap between theoretical data and experimental data, the gap can go either way. Like, for example, I can create a model myself and then I run experiment. If the experiment match my model 100 per cent, that's probably a good indicator my model is correct. On the other hand now is, the experimental data, in the usual way in research, may not match 100 per cent to your theoretical data. Then the other side we need to look at now is does my experimental data</li> </ul>
3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	<ul> <li>A. Yes.</li> <li>Q this is what Mr Southward has done overnight, by replotting your graph, by applying the percentage to a thread length of ten threads; right?</li> <li>A. Okay.</li> <li>Q. Then the result would be, as I have just explored with you, a moving sideways to the left of the circles depicting 30 per cent engagement, 50 per cent engagement and 60 per cent engagement. You understand the logic? You may not agree with the logic but you understand this logic?</li> <li>A. I understand.</li> <li>Q. Then you can see that there is a pattern whereby for the theoretical line and the line represented by the actual result, the two lines are similar in shape?</li> <li>A. What do you mean by "two lines"? We see only one line on the graph.</li> </ul>	3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	<ul> <li>A. That's right.</li> <li>Q. So you would expect to see a gap between solid circle and hollow circle for each value of engagement; correct?</li> <li>A. Correct.</li> <li>Q. But that is what you see, for each value of number of threads engagement, you see one value for theoretical, calculated value, and one value for actual pulling-out test results?</li> <li>A. When you mention you see a gap between theoretical data and experimental data, the gap can go either way. Like, for example, I can create a model myself and then I run experiment. If the experiment match my model 100 per cent, that's probably a good indicator my model is correct. On the other hand now is, the experimental data, in the usual way in research, may not match 100 per cent to your theoretical data. Then the other side we need to look at now is does my experimental data overestimate the theoretical data or underestimate?</li> </ul>
3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	<ul> <li>A. Yes.</li> <li>Q this is what Mr Southward has done overnight, by replotting your graph, by applying the percentage to a thread length of ten threads; right?</li> <li>A. Okay.</li> <li>Q. Then the result would be, as I have just explored with you, a moving sideways to the left of the circles depicting 30 per cent engagement, 50 per cent engagement and 60 per cent engagement. You understand the logic? You may not agree with the logic but you understand this logic?</li> <li>A. I understand.</li> <li>Q. Then you can see that there is a pattern whereby for the theoretical line and the line represented by the actual result, the two lines are similar in shape?</li> <li>A. What do you mean by "two lines"? We see only one line on the graph.</li> <li>Q. If you try to look at because you are making a point</li> </ul>	3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	<ul> <li>A. That's right.</li> <li>Q. So you would expect to see a gap between solid circle and hollow circle for each value of engagement; correct?</li> <li>A. Correct.</li> <li>Q. But that is what you see, for each value of number of threads engagement, you see one value for theoretical, calculated value, and one value for actual pulling-out test results?</li> <li>A. When you mention you see a gap between theoretical data and experimental data, the gap can go either way. Like, for example, I can create a model myself and then I run experiment. If the experiment match my model 100 per cent, that's probably a good indicator my model is correct. On the other hand now is, the experimental data, in the usual way in research, may not match 100 per cent to your theoretical data. Then the other side we need to look at now is does my experimental data overestimate the theoretical data or underestimate? The point I want to make yesterday is the</li> </ul>
3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	<ul> <li>A. Yes.</li> <li>Q this is what Mr Southward has done overnight, by replotting your graph, by applying the percentage to a thread length of ten threads; right?</li> <li>A. Okay.</li> <li>Q. Then the result would be, as I have just explored with you, a moving sideways to the left of the circles depicting 30 per cent engagement, 50 per cent engagement and 60 per cent engagement. You understand the logic? You may not agree with the logic but you understand this logic?</li> <li>A. I understand.</li> <li>Q. Then you can see that there is a pattern whereby for the theoretical line and the line represented by the actual result, the two lines are similar in shape?</li> <li>A. What do you mean by "two lines"? We see only one line on the graph.</li> <li>Q. If you try to look at because you are making a point about the comparative value between the actual result</li> </ul>	3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	<ul> <li>A. That's right.</li> <li>Q. So you would expect to see a gap between solid circle and hollow circle for each value of engagement; correct?</li> <li>A. Correct.</li> <li>Q. But that is what you see, for each value of number of threads engagement, you see one value for theoretical, calculated value, and one value for actual pulling-out test results?</li> <li>A. When you mention you see a gap between theoretical data and experimental data, the gap can go either way. Like, for example, I can create a model myself and then I run experiment. If the experiment match my model 100 per cent, that's probably a good indicator my model is correct. On the other hand now is, the experimental data, in the usual way in research, may not match 100 per cent to your theoretical data. Then the other side we need to look at now is does my experimental data overestimate the theoretical data or underestimate? The point I want to make yesterday is the theoretical data presented by BOSA actually</li> </ul>
3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>A. Yes.</li> <li>Q this is what Mr Southward has done overnight, by replotting your graph, by applying the percentage to a thread length of ten threads; right?</li> <li>A. Okay.</li> <li>Q. Then the result would be, as I have just explored with you, a moving sideways to the left of the circles depicting 30 per cent engagement, 50 per cent engagement and 60 per cent engagement. You understand the logic? You may not agree with the logic but you understand this logic?</li> <li>A. I understand.</li> <li>Q. Then you can see that there is a pattern whereby for the theoretical line and the line represented by the actual result, the two lines are similar in shape?</li> <li>A. What do you mean by "two lines"? We see only one line on the graph.</li> <li>Q. If you try to look at because you are making a point about the comparative value between the actual result and the theoretical result, and you observe that there</li> </ul>	3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>A. That's right.</li> <li>Q. So you would expect to see a gap between solid circle and hollow circle for each value of engagement; correct?</li> <li>A. Correct.</li> <li>Q. But that is what you see, for each value of number of threads engagement, you see one value for theoretical, calculated value, and one value for actual pulling-out test results?</li> <li>A. When you mention you see a gap between theoretical data and experimental data, the gap can go either way. Like, for example, I can create a model myself and then I run experiment. If the experiment match my model 100 per cent, that's probably a good indicator my model is correct. On the other hand now is, the experimental data, in the usual way in research, may not match 100 per cent to your theoretical data. Then the other side we need to look at now is does my experimental data overestimate the theoretical data or underestimate? The point I want to make yesterday is the theoretical data.</li> </ul>
3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	<ul> <li>A. Yes.</li> <li>Q this is what Mr Southward has done overnight, by replotting your graph, by applying the percentage to a thread length of ten threads; right?</li> <li>A. Okay.</li> <li>Q. Then the result would be, as I have just explored with you, a moving sideways to the left of the circles depicting 30 per cent engagement, 50 per cent engagement and 60 per cent engagement. You understand the logic? You may not agree with the logic but you understand this logic?</li> <li>A. I understand.</li> <li>Q. Then you can see that there is a pattern whereby for the theoretical line and the line represented by the actual result, the two lines are similar in shape?</li> <li>A. What do you mean by "two lines"? We see only one line on the graph.</li> <li>Q. If you try to look at because you are making a point about the comparative value between the actual result and the theoretical result, and you observe that there was something not quite right</li> </ul>	3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	<ul> <li>A. That's right.</li> <li>Q. So you would expect to see a gap between solid circle and hollow circle for each value of engagement; correct?</li> <li>A. Correct.</li> <li>Q. But that is what you see, for each value of number of threads engagement, you see one value for theoretical, calculated value, and one value for actual pulling-out test results?</li> <li>A. When you mention you see a gap between theoretical data and experimental data, the gap can go either way. Like, for example, I can create a model myself and then I run experiment. If the experiment match my model 100 per cent, that's probably a good indicator my model is correct. On the other hand now is, the experimental data, in the usual way in research, may not match 100 per cent to your theoretical data. Then the other side we need to look at now is does my experimental data overestimate the theoretical data or underestimate? The point I want to make yesterday is the theoretical data presented by BOSA actually overestimates the experimental data. In this graph now, what you try to present is the</li> </ul>
3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>A. Yes.</li> <li>Q this is what Mr Southward has done overnight, by replotting your graph, by applying the percentage to a thread length of ten threads; right?</li> <li>A. Okay.</li> <li>Q. Then the result would be, as I have just explored with you, a moving sideways to the left of the circles depicting 30 per cent engagement, 50 per cent engagement and 60 per cent engagement. You understand the logic? You may not agree with the logic but you understand this logic?</li> <li>A. I understand.</li> <li>Q. Then you can see that there is a pattern whereby for the theoretical line and the line represented by the actual result, the two lines are similar in shape?</li> <li>A. What do you mean by "two lines"? We see only one line on the graph.</li> <li>Q. If you try to look at because you are making a point about the comparative value between the actual result and the theoretical result, and you observe that there</li> </ul>	3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>A. That's right.</li> <li>Q. So you would expect to see a gap between solid circle and hollow circle for each value of engagement; correct?</li> <li>A. Correct.</li> <li>Q. But that is what you see, for each value of number of threads engagement, you see one value for theoretical, calculated value, and one value for actual pulling-out test results?</li> <li>A. When you mention you see a gap between theoretical data and experimental data, the gap can go either way. Like, for example, I can create a model myself and then I run experiment. If the experiment match my model 100 per cent, that's probably a good indicator my model is correct. On the other hand now is, the experimental data, in the usual way in research, may not match 100 per cent to your theoretical data. Then the other side we need to look at now is does my experimental data overestimate the theoretical data or underestimate? The point I want to make yesterday is the theoretical data.</li> </ul>

1	Page 13		Page 15
	line.	1	in response to the BD's enquiry of BOSA?
2	Q. The open circles represent the result of actual pulling	2	A. Right. That's what I can recall.
3	out based on the actual steel bars used; correct?	3	COMMISSIONER HANSFORD: Mr Shieh, could we have in the break
4	A. Correct.	4	this morning we don't need it now a hard copy of
5	Q. And if the actual steel bars are of a higher grade,	5	this graph, please?
6	let's say 500, you would expect them to require a higher	6	MR SHIEH: Mr Southward's graph?
7	strength to be able to break them?	7	COMMISSIONER HANSFORD: Yes.
8	A. Even theoretically.	8	MR SHIEH: We can. Certainly. The Commission will deal
9	Q. But theoretically they used 460?	9	with it.
10	A. That's correct.	10	Let's look at BOSA's letter, bundle H26. A letter
11	Q. But if in fact 500 is used you would expect the tensile	11	from BOSA.
12	strength to be higher?	12	MR PENNICOTT: 221_11. Is that it on the screen?
13	A. I would expect that the solid line will be moved above,	13	MR SHIEH: Yes.
14	because the thread gets stronger; right?	14	You are talking about page 45643? Is that the
15	COMMISSIONER HANSFORD: May I interject?	15	photograph that you were referring to?
16	MR SHIEH: Yes.	16	A. I also saw a different set, but I think they are taking
17	COMMISSIONER HANSFORD: Prof Yeung, are you saying that if	17	the same sample taking the same specimens.
18	one were to plot also on this graph the theoretical line	18	Q. Because if you are talking about the letter the
19	for 500	19	photograph attached to BOSA's letter, that is the BOSA
20	A. Yes.	20	letter attaching photographs.
21	COMMISSIONER HANSFORD: that would also provide a useful	21	COMMISSIONER HANSFORD: I'm not sure I'm very comfortable
22	additional piece of information?	22	with counting threads off photographs.
23	A. You are perfectly correct.	23	MR SHIEH: I just wish to make sure that we know what the
24	COMMISSIONER HANSFORD: And maybe that can be done before we		professor is talking about.
25	hear from one of the other experts.	25	COMMISSIONER HANSFORD: Yes, I understand.
	Page 14		Page 16
1	A. I think that's a good idea.	1	MR SHIEH: As I say, I'm not going to engage in this tedious
2	MR SHIEH: We can do all kinds of replotting and all that,	2	exercise of asking for each bar to be magnified and then
3	but as a matter of shape, if you plot if you look at	3	we do a counting by committee. I just wish to make sure
4	the distance if you look at the shape of the three	4	that we all know where it is and we can all observe the
5	hollow lines	5	threads ourselves.
6	A. Yes.	6	So this is the photograph that we can locate. Do
7	Q if you try to plot the three hollow lines, they are	7	you have in mind some other photograph that you acted
8	almost parallel to the solid line, maybe 30 per cent	8	on?
9	8	9	A. I recall I saw one is with a photograph of each of
1		10	the specimens. But I think they are taking the picture
10	Q. And the difference between 460 and 500 is 8 per cent?	11	of the same specimens.
11	A. 460 and 500 is	12	Q. Except this one they put all five together, you are
11 12			
11 12 13		13	saying?
11 12 13 14	A. Yes. I think you are talking more it's about	14	A. Yes.
11 12 13 14 15	<ul><li>A. Yes. I think you are talking more it's about</li><li>9 per cent, I guess.</li></ul>	14 15	<ul><li>A. Yes.</li><li>Q. Anyway, we know that these are the bars that you looked</li></ul>
11 12 13 14 15 16	<ul><li>A. Yes. I think you are talking more it's about</li><li>9 per cent, I guess.</li><li>Q. Anyway, can I ask you to refer us to the photograph that</li></ul>	14 15 16	<ul><li>A. Yes.</li><li>Q. Anyway, we know that these are the bars that you looked at?</li></ul>
11 12 13 14 15 16 17	<ul><li>A. Yes. I think you are talking more it's about</li><li>9 per cent, I guess.</li><li>Q. Anyway, can I ask you to refer us to the photograph that you say you looked at. I'm not going to spend any more</li></ul>	14 15 16 17	<ul><li>A. Yes.</li><li>Q. Anyway, we know that these are the bars that you looked at?</li><li>A. Correct.</li></ul>
11 12 13 14 15 16 17 18	<ul><li>A. Yes. I think you are talking more it's about 9 per cent, I guess.</li><li>Q. Anyway, can I ask you to refer us to the photograph that you say you looked at. I'm not going to spend any more time discussing what we can see from photographs,</li></ul>	14 15 16 17 18	<ul><li>A. Yes.</li><li>Q. Anyway, we know that these are the bars that you looked at?</li><li>A. Correct.</li><li>Q. Photographs of the bars that you looked at. You are</li></ul>
11 12 13 14 15 16 17 18 19	<ul><li>A. Yes. I think you are talking more it's about 9 per cent, I guess.</li><li>Q. Anyway, can I ask you to refer us to the photograph that you say you looked at. I'm not going to spend any more time discussing what we can see from photographs, because we can all see what's in the photograph. I just</li></ul>	14 15 16 17 18 19	<ul><li>A. Yes.</li><li>Q. Anyway, we know that these are the bars that you looked at?</li><li>A. Correct.</li><li>Q. Photographs of the bars that you looked at. You are saying that there may well somewhere be individual</li></ul>
11 12 13 14 15 16 17 18 19 20	<ul> <li>A. Yes. I think you are talking more it's about 9 per cent, I guess.</li> <li>Q. Anyway, can I ask you to refer us to the photograph that you say you looked at. I'm not going to spend any more time discussing what we can see from photographs, because we can all see what's in the photograph. I just wish the professor to let us know, when he said instead</li> </ul>	14 15 16 17 18 19 20	<ul><li>A. Yes.</li><li>Q. Anyway, we know that these are the bars that you looked at?</li><li>A. Correct.</li><li>Q. Photographs of the bars that you looked at. You are saying that there may well somewhere be individual photos of each bar?</li></ul>
11 12 13 14 15 16 17 18 19 20 21	<ul> <li>A. Yes. I think you are talking more it's about 9 per cent, I guess.</li> <li>Q. Anyway, can I ask you to refer us to the photograph that you say you looked at. I'm not going to spend any more time discussing what we can see from photographs, because we can all see what's in the photograph. I just wish the professor to let us know, when he said instead of using percentage he counted the number of threads in</li> </ul>	14 15 16 17 18 19 20 21	<ul> <li>A. Yes.</li> <li>Q. Anyway, we know that these are the bars that you looked at?</li> <li>A. Correct.</li> <li>Q. Photographs of the bars that you looked at. You are saying that there may well somewhere be individual photos of each bar?</li> <li>A. Yes.</li> </ul>
111 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>A. Yes. I think you are talking more it's about 9 per cent, I guess.</li> <li>Q. Anyway, can I ask you to refer us to the photograph that you say you looked at. I'm not going to spend any more time discussing what we can see from photographs, because we can all see what's in the photograph. I just wish the professor to let us know, when he said instead of using percentage he counted the number of threads in the actual pulling-out results, I wish you to refer us</li> </ul>	14 15 16 17 18 19 20 21 22	<ul> <li>A. Yes.</li> <li>Q. Anyway, we know that these are the bars that you looked at?</li> <li>A. Correct.</li> <li>Q. Photographs of the bars that you looked at. You are saying that there may well somewhere be individual photos of each bar?</li> <li>A. Yes.</li> <li>Q. Maybe bigger?</li> </ul>
111 12 13 14 15 16 17 18 19 20 21 20 21 22 23	<ul> <li>A. Yes. I think you are talking more it's about 9 per cent, I guess.</li> <li>Q. Anyway, can I ask you to refer us to the photograph that you say you looked at. I'm not going to spend any more time discussing what we can see from photographs, because we can all see what's in the photograph. I just wish the professor to let us know, when he said instead of using percentage he counted the number of threads in the actual pulling-out results, I wish you to refer us to the actual photographs so we have on record where</li> </ul>	<ol> <li>14</li> <li>15</li> <li>16</li> <li>17</li> <li>18</li> <li>19</li> <li>20</li> <li>21</li> <li>22</li> <li>23</li> </ol>	<ul> <li>A. Yes.</li> <li>Q. Anyway, we know that these are the bars that you looked at?</li> <li>A. Correct.</li> <li>Q. Photographs of the bars that you looked at. You are saying that there may well somewhere be individual photos of each bar?</li> <li>A. Yes.</li> <li>Q. Maybe bigger?</li> <li>A. Yes.</li> </ul>
11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>A. Yes. I think you are talking more it's about 9 per cent, I guess.</li> <li>Q. Anyway, can I ask you to refer us to the photograph that you say you looked at. I'm not going to spend any more time discussing what we can see from photographs, because we can all see what's in the photograph. I just wish the professor to let us know, when he said instead of using percentage he counted the number of threads in the actual pulling-out results, I wish you to refer us to the actual photographs so we have on record where they are.</li> </ul>	14 15 16 17 18 19 20 21 22	<ul> <li>A. Yes.</li> <li>Q. Anyway, we know that these are the bars that you looked at?</li> <li>A. Correct.</li> <li>Q. Photographs of the bars that you looked at. You are saying that there may well somewhere be individual photos of each bar?</li> <li>A. Yes.</li> <li>Q. Maybe bigger?</li> </ul>

	Page 17		Page 19
1	MR SHIEH: Thank you.	1	I wonder if we can look at the transcript, at Day 30,
2	Thank you very much. I have no further questions.	2	page 142.
3	Further cross-examination by MR BOULDING	3	Have you had an opportunity to consider the
4	MR BOULDING: Thank you for allowing me to ask a few further	4	evidence, Prof Yeung?
5	questions, Commissioners.	5	A. Of whom?
6	Good morning, Prof Yeung.	6	Q. Of Andy Wong, MTR's Andy Wong.
7	A. Good morning.	7	A. No, no.
8	Q. Yesterday, you will remember we were talking about	8	Q. Let's have a little look together. Page 142, yes. Then
9	figure 4 in your report. I think we probably ought to	9	line 10, and I'm asking him questions here in
10	get it up. Bundle ER1, tab 8 at page 26.	10	re-examination:
11	A. Yes.	11	"Can you tell the Commissioners how you would check
12	Q. If we could go down to page 26, please. That's the one.	12	for compliance?
13	There we've got the "Visual inspection acceptable	13	Answer: First of all, as I said, I would do
14	thread tolerance", and we can see that zero tolerance is	14	a visual inspection, that is to see if there would be
15	acceptable, right up and including a maximum of	15	an over-exposure of threads. The correct ones would be
16	2 millimetres showing; correct?	16	just one or two threads. Then I would use my hand or
17	A. Will you repeat the last part of the question?	17	use my leg to push it, to see if they were steady. If
18	Q. Yes. If we look at the red arrow below the bottom of	18	there was too little connection, then it would not be
19	the photograph, we can see that zero tolerance is at one	19	stable or not aligned."
20	end, and then the maximum tolerance is the two threads	20	So whilst he doesn't refer to it expressly, it
21	we can see there; correct?	21	appears to be the case, does it not, that he has in mind
22	A. Correct.	22	this acceptable thread tolerance as referred to in
23	Q. Yesterday we were proceeding on the basis, were we not,	23	figure 4?
24	that the conscientious MTR site inspector, the	24	A. I agree.
25	conscientious worker, would have this document in his or	25	Q. Thank you. Then just reading on, line 18:
	Page 18		Page 20
1	her back pocket to be able to check on site what was	1	"Did you ever watch the rebar being screwed into the
2	acceptable? Do you remember proceeding on that basis?	2	couplers?
3	A. I recall.	3	Answer: Yes. Yes, I did. That is more or less
4	Q. You'll know, won't you and in any event we've	4	part of my daily duties. If there was the coupler
5	heard that at the time this check has to be carried	5	connection, I would watch it.
6	out, first of all you've got the D-wall constructed;	6	Question: I see. Is that something you did
7	correct?	7	throughout the whole of your 100 metres that you covered
8	A. Depending whether checking for the reinforcement of the	8	in C2/C3?
9	D-wall or checking on the reinforcement between the EWL	9	Answer: Yes. Well, at the same time, there would
10	slab and the D-wall. These are also used for the	10	be two or three teams of people. Say, for example, on
11	D-wall.	11	that day, on 22 September, that evening there were
12	Q. Yes. Well, I'm talking about the EWL slab to the	12	18 people on the night shift, so I can't say that I
13	D-wall.	13	would have seen everything, but I would do my best. "
14	A. Correct.	14	And I said, "Well done."
15	Q. So let's proceed on that basis. So you've got the	15	Proceeding on that basis, he sees a maximum of
16	D-wall concreted; correct?	16	2 millimetre exposed threads, two threads exposed, and
17	A. Correct.	17	he would be entitled, would he not, by reference to the
18	Q. And you've got the couplers in the D-wall encased in	18	figure 4 in your report, to say that's all right?
19	concrete?	19	A. I think you missed the second part of what he said,
20	A. Correct.	20	because he said he also pushed on that one.
21	Q. And one is looking to see whether the threaded rebar	21	Q. That's right.
22	which goes into the coupler is adequately engaged;	22	A. That's another thing. If you recall what BOSA put in
23	correct?	23	for us, if they are not spliced butt-to-butt, that one
24	A. Correct.	24	will be loose.
25	Q. We had some evidence on this particular matter.	25	Q. That's what I'm coming to. That's what I'm coming to.

	Page 21		Page 23
1	And it was in this context yesterday that you brought up	1	Q. Looking down, we can see, can we not, that the reader is
2	the so-called BOSA requirement for butt-to-butt; do you	2	being told here what the appropriate installation method
3	remember mentioning that to the Commissioners?	3	is; right?
4	A. Yes, I did.	4	A. Yes.
5	Q. We've been through the BOSA brochures overnight that	5	Q. And step 1, "Position the 1st stage rebar":
6	were available during the course of the contract and we	6	"Ensure the coupler is fully screwed into the bar
7	cannot find anything there.	7	prior to being cast in concrete.
8	I wonder if we can look at a document together,	8	Protective cap should be fitted on coupler end to
9	H4056. Thank you.	9	prevent ingress of foreign material."
10	A. Hang on. I haven't got the document yet.	10	Now, there we are talking about the D-wall, are we
11	Q. It's on the screen.	11	not?
12	A. Okay.	12	A. Yes.
13	Q. There we see, do we not, the MTR writing to the BD on		Q. Then step 2, "Connect the continuation bar". Now, here
14	8 July 2013; correct?	14	we are talking about the bar which goes from the slab
15	A. 8 July, correct.	15	into the coupler, which has already been cast in the
16	Q. They are making a submission, and we can see that they		D-wall; correct?
17	are sending the material submission of the proposed	17	A. I think if you look at the letter
18	coupler for diaphragm wall reinforcement cage and slab	18	Q. Which letter?
19	construction at Hung Hom Station; right?	19	A. The cover letter of this manual. It was this set of
20	A. Correct.	20	information are attached for the diaphragm wall
21	Q. If we look at the document I think if we go on to	21	construction.
22	H4142, I hope you see a BOSA catalogue entitled,	22	Q. But this also applies to the slab?
23	"Technical and quality assurance manual Seisplice	23	MR PENNICOTT: And slab. It says "slab".
24 25	standard ductility coupler type A (type II ductility	24 25	<ul><li>A. Okay. I take your word for it.</li><li>MR BOULDING: And step 2, "Connect the continuation bar":</li></ul>
23	coupler)"; do you see that?	23	
	Page 22		Page 24
1			
1 -	A. Correct.	1	"Position the continuation bar.
2	Q. If you look back at your report on page 26, one can see,	2	Remove both protective cap on the rebar and the
3	Q. If you look back at your report on page 26, one can see, can one not, in the summary, number 2:	2 3	Remove both protective cap on the rebar and the coupler.
3 4	<ul><li>Q. If you look back at your report on page 26, one can see, can one not, in the summary, number 2:</li><li>"Please refer to our Seisplice technical and quality</li></ul>	2 3 4	Remove both protective cap on the rebar and the coupler. Fully engage the thread using hand to the coupler.
3 4 5	<ul> <li>Q. If you look back at your report on page 26, one can see, can one not, in the summary, number 2:</li> <li>"Please refer to our Seisplice technical and quality assurance manual"</li> </ul>	2 3 4 5	Remove both protective cap on the rebar and the coupler. Fully engage the thread using hand to the coupler. This should develop full tensile strength of the splice
3 4 5 6	<ul> <li>Q. If you look back at your report on page 26, one can see, can one not, in the summary, number 2:</li> <li>"Please refer to our Seisplice technical and quality assurance manual"</li> <li>That is the same document, is it not, that we are</li> </ul>	2 3 4 5 6	Remove both protective cap on the rebar and the coupler. Fully engage the thread using hand to the coupler. This should develop full tensile strength of the splice once fully engaged."
3 4 5 6 7	<ul> <li>Q. If you look back at your report on page 26, one can see, can one not, in the summary, number 2:</li> <li>"Please refer to our Seisplice technical and quality assurance manual"</li> <li>That is the same document, is it not, that we are looking at at H4142?</li> </ul>	2 3 4 5 6 7	Remove both protective cap on the rebar and the coupler. Fully engage the thread using hand to the coupler. This should develop full tensile strength of the splice once fully engaged." Then step 3, "Lock the splice":
3 4 5 6 7 8	<ul> <li>Q. If you look back at your report on page 26, one can see, can one not, in the summary, number 2:</li> <li>"Please refer to our Seisplice technical and quality assurance manual"</li> <li>That is the same document, is it not, that we are looking at at H4142?</li> <li>A. Agree.</li> </ul>	2 3 4 5 6 7 8	Remove both protective cap on the rebar and the coupler. Fully engage the thread using hand to the coupler. This should develop full tensile strength of the splice once fully engaged." Then step 3, "Lock the splice": "Use a typical pipe wrench to tighten the splice.
3 4 5 6 7 8 9	<ul> <li>Q. If you look back at your report on page 26, one can see, can one not, in the summary, number 2:</li> <li>"Please refer to our Seisplice technical and quality assurance manual"</li> <li>That is the same document, is it not, that we are looking at at H4142?</li> <li>A. Agree.</li> <li>Q. Then if we go over to H4143, we've got a "Content" page,</li> </ul>	2 3 4 5 6 7 8 9	Remove both protective cap on the rebar and the coupler. Fully engage the thread using hand to the coupler. This should develop full tensile strength of the splice once fully engaged." Then step 3, "Lock the splice": "Use a typical pipe wrench to tighten the splice. No special torque amount is required."
3 4 5 6 7 8 9 10	<ul> <li>Q. If you look back at your report on page 26, one can see, can one not, in the summary, number 2:</li> <li>"Please refer to our Seisplice technical and quality assurance manual"</li> <li>That is the same document, is it not, that we are looking at at H4142?</li> <li>A. Agree.</li> <li>Q. Then if we go over to H4143, we've got a "Content" page, and if we look together at item 8, we can see, can we</li> </ul>	2 3 4 5 6 7 8 9 10	Remove both protective cap on the rebar and the coupler. Fully engage the thread using hand to the coupler. This should develop full tensile strength of the splice once fully engaged." Then step 3, "Lock the splice": "Use a typical pipe wrench to tighten the splice. No special torque amount is required." Now, it's obvious, is it not, that there's
3 4 5 6 7 8 9 10 11	<ul> <li>Q. If you look back at your report on page 26, one can see, can one not, in the summary, number 2:</li> <li>"Please refer to our Seisplice technical and quality assurance manual"</li> <li>That is the same document, is it not, that we are looking at at H4142?</li> <li>A. Agree.</li> <li>Q. Then if we go over to H4143, we've got a "Content" page, and if we look together at item 8, we can see, can we not, the "Seisplice standard ductility coupler</li> </ul>	2 3 4 5 6 7 8 9 10 11	Remove both protective cap on the rebar and the coupler. Fully engage the thread using hand to the coupler. This should develop full tensile strength of the splice once fully engaged." Then step 3, "Lock the splice": "Use a typical pipe wrench to tighten the splice. No special torque amount is required." Now, it's obvious, is it not, that there's absolutely no reference to, is there, to a requirement
3 4 5 6 7 8 9 10 11 12	<ul> <li>Q. If you look back at your report on page 26, one can see, can one not, in the summary, number 2: <ul> <li>"Please refer to our Seisplice technical and quality assurance manual"</li> <li>That is the same document, is it not, that we are looking at at H4142?</li> </ul> </li> <li>A. Agree.</li> <li>Q. Then if we go over to H4143, we've got a "Content" page, and if we look together at item 8, we can see, can we not, the "Seisplice standard ductility coupler coupler installation method"; do you see that?</li> </ul>	2 3 4 5 6 7 8 9 10 11 12	Remove both protective cap on the rebar and the coupler. Fully engage the thread using hand to the coupler. This should develop full tensile strength of the splice once fully engaged." Then step 3, "Lock the splice": "Use a typical pipe wrench to tighten the splice. No special torque amount is required." Now, it's obvious, is it not, that there's absolutely no reference to, is there, to a requirement for a butt-to-butt connection; that's correct, isn't it?
3 4 5 6 7 8 9 10 11 12 13	<ul> <li>Q. If you look back at your report on page 26, one can see, can one not, in the summary, number 2:</li> <li>"Please refer to our Seisplice technical and quality assurance manual"</li> <li>That is the same document, is it not, that we are looking at at H4142?</li> <li>A. Agree.</li> <li>Q. Then if we go over to H4143, we've got a "Content" page, and if we look together at item 8, we can see, can we not, the "Seisplice standard ductility coupler coupler installation method"; do you see that?</li> <li>A. Item?</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13	Remove both protective cap on the rebar and the coupler. Fully engage the thread using hand to the coupler. This should develop full tensile strength of the splice once fully engaged." Then step 3, "Lock the splice": "Use a typical pipe wrench to tighten the splice. No special torque amount is required." Now, it's obvious, is it not, that there's absolutely no reference to, is there, to a requirement for a butt-to-butt connection; that's correct, isn't it? A. No, it's not.
3 4 5 6 7 8 9 10 11 12 13 14	<ul> <li>Q. If you look back at your report on page 26, one can see, can one not, in the summary, number 2:</li> <li>"Please refer to our Seisplice technical and quality assurance manual"</li> <li>That is the same document, is it not, that we are looking at at H4142?</li> <li>A. Agree.</li> <li>Q. Then if we go over to H4143, we've got a "Content" page, and if we look together at item 8, we can see, can we not, the "Seisplice standard ductility coupler coupler installation method"; do you see that?</li> <li>A. Item?</li> <li>Q. Item 8. It's on page H4143.</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14	Remove both protective cap on the rebar and the coupler. Fully engage the thread using hand to the coupler. This should develop full tensile strength of the splice once fully engaged." Then step 3, "Lock the splice": "Use a typical pipe wrench to tighten the splice. No special torque amount is required." Now, it's obvious, is it not, that there's absolutely no reference to, is there, to a requirement for a butt-to-butt connection; that's correct, isn't it? A. No, it's not. Q. Well, where do you see it there?
3 4 5 6 7 8 9 10 11 12 13 14 15	<ul> <li>Q. If you look back at your report on page 26, one can see, can one not, in the summary, number 2: <ul> <li>"Please refer to our Seisplice technical and quality assurance manual"</li> <li>That is the same document, is it not, that we are looking at at H4142?</li> </ul> </li> <li>A. Agree.</li> <li>Q. Then if we go over to H4143, we've got a "Content" page, and if we look together at item 8, we can see, can we not, the "Seisplice standard ductility coupler coupler installation method"; do you see that?</li> <li>A. Item?</li> <li>Q. Item 8. It's on page H4143. Do you see it? Just there.</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15	Remove both protective cap on the rebar and the coupler. Fully engage the thread using hand to the coupler. This should develop full tensile strength of the splice once fully engaged." Then step 3, "Lock the splice": "Use a typical pipe wrench to tighten the splice. No special torque amount is required." Now, it's obvious, is it not, that there's absolutely no reference to, is there, to a requirement for a butt-to-butt connection; that's correct, isn't it? A. No, it's not. Q. Well, where do you see it there? A. If you follow these four steps as shown on the
3 4 5 6 7 8 9 10 11 12 13 14 15 16	<ul> <li>Q. If you look back at your report on page 26, one can see, can one not, in the summary, number 2: <ul> <li>"Please refer to our Seisplice technical and quality assurance manual"</li> <li>That is the same document, is it not, that we are looking at at H4142?</li> </ul> </li> <li>A. Agree.</li> <li>Q. Then if we go over to H4143, we've got a "Content" page, and if we look together at item 8, we can see, can we not, the "Seisplice standard ductility coupler coupler installation method"; do you see that?</li> <li>A. Item?</li> <li>Q. Item 8. It's on page H4143. Do you see it? Just there.</li> <li>A. Yes, yes.</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	<ul> <li>Remove both protective cap on the rebar and the coupler.</li> <li>Fully engage the thread using hand to the coupler.</li> <li>This should develop full tensile strength of the splice once fully engaged."</li> <li>Then step 3, "Lock the splice":</li> <li>"Use a typical pipe wrench to tighten the splice.</li> <li>No special torque amount is required."</li> <li>Now, it's obvious, is it not, that there's absolutely no reference to, is there, to a requirement for a butt-to-butt connection; that's correct, isn't it?</li> <li>A. No, it's not.</li> <li>Q. Well, where do you see it there?</li> <li>A. If you follow these four steps as shown on the instruction, I think for the first one, they say the</li> </ul>
3 4 5 6 7 8 9 10 11 12 13 14 15	<ul> <li>Q. If you look back at your report on page 26, one can see, can one not, in the summary, number 2: <ul> <li>"Please refer to our Seisplice technical and quality assurance manual"</li> <li>That is the same document, is it not, that we are looking at at H4142?</li> </ul> </li> <li>A. Agree.</li> <li>Q. Then if we go over to H4143, we've got a "Content" page, and if we look together at item 8, we can see, can we not, the "Seisplice standard ductility coupler coupler installation method"; do you see that?</li> <li>A. Item?</li> <li>Q. Item 8. It's on page H4143. Do you see it? Just there.</li> <li>A. Yes, yes.</li> <li>Q. Then we can pick that document up at H4173.</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	<ul> <li>Remove both protective cap on the rebar and the coupler.</li> <li>Fully engage the thread using hand to the coupler.</li> <li>This should develop full tensile strength of the splice once fully engaged."</li> <li>Then step 3, "Lock the splice":</li> <li>"Use a typical pipe wrench to tighten the splice. No special torque amount is required."</li> <li>Now, it's obvious, is it not, that there's absolutely no reference to, is there, to a requirement for a butt-to-butt connection; that's correct, isn't it?</li> <li>A. No, it's not.</li> <li>Q. Well, where do you see it there?</li> <li>A. If you follow these four steps as shown on the instruction, I think for the first one, they say the first one needs to be tightened to the end; right?</li> </ul>
3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	<ul> <li>Q. If you look back at your report on page 26, one can see, can one not, in the summary, number 2: <ul> <li>"Please refer to our Seisplice technical and quality assurance manual"</li> <li>That is the same document, is it not, that we are looking at at H4142?</li> </ul> </li> <li>A. Agree.</li> <li>Q. Then if we go over to H4143, we've got a "Content" page, and if we look together at item 8, we can see, can we not, the "Seisplice standard ductility coupler coupler installation method"; do you see that?</li> <li>A. Item?</li> <li>Q. Item 8. It's on page H4143. Do you see it? Just there.</li> <li>A. Yes, yes.</li> <li>Q. Then we can pick that document up at H4173.</li> <li>A. Yes.</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	<ul> <li>Remove both protective cap on the rebar and the coupler.</li> <li>Fully engage the thread using hand to the coupler.</li> <li>This should develop full tensile strength of the splice once fully engaged."</li> <li>Then step 3, "Lock the splice":</li> <li>"Use a typical pipe wrench to tighten the splice.</li> <li>No special torque amount is required."</li> <li>Now, it's obvious, is it not, that there's absolutely no reference to, is there, to a requirement for a butt-to-butt connection; that's correct, isn't it?</li> <li>A. No, it's not.</li> <li>Q. Well, where do you see it there?</li> <li>A. If you follow these four steps as shown on the instruction, I think for the first one, they say the first one needs to be tightened to the end; right?</li> <li>Q. Sorry, where are you looking?</li> </ul>
3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	<ul> <li>Q. If you look back at your report on page 26, one can see, can one not, in the summary, number 2: <ul> <li>"Please refer to our Seisplice technical and quality assurance manual"</li> <li>That is the same document, is it not, that we are looking at at H4142?</li> </ul> </li> <li>A. Agree.</li> <li>Q. Then if we go over to H4143, we've got a "Content" page, and if we look together at item 8, we can see, can we not, the "Seisplice standard ductility coupler coupler installation method"; do you see that?</li> <li>A. Item?</li> <li>Q. Item 8. It's on page H4143. Do you see it? Just there.</li> <li>A. Yes, yes.</li> <li>Q. Then we can pick that document up at H4173.</li> <li>A. Yes.</li> <li>Q. Do you see, at the top of the page, the BOSA logo? Do</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	<ul> <li>Remove both protective cap on the rebar and the coupler.</li> <li>Fully engage the thread using hand to the coupler.</li> <li>This should develop full tensile strength of the splice once fully engaged."</li> <li>Then step 3, "Lock the splice":</li> <li>"Use a typical pipe wrench to tighten the splice.</li> <li>No special torque amount is required."</li> <li>Now, it's obvious, is it not, that there's absolutely no reference to, is there, to a requirement for a butt-to-butt connection; that's correct, isn't it?</li> <li>A. No, it's not.</li> <li>Q. Well, where do you see it there?</li> <li>A. If you follow these four steps as shown on the instruction, I think for the first one, they say the first one needs to be tightened to the end; right?</li> <li>Q. Sorry, where are you looking?</li> <li>A. Step number 1.</li> </ul>
3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	<ul> <li>Q. If you look back at your report on page 26, one can see, can one not, in the summary, number 2: <ul> <li>"Please refer to our Seisplice technical and quality assurance manual"</li> <li>That is the same document, is it not, that we are looking at at H4142?</li> </ul> </li> <li>A. Agree.</li> <li>Q. Then if we go over to H4143, we've got a "Content" page, and if we look together at item 8, we can see, can we not, the "Seisplice standard ductility coupler coupler installation method"; do you see that?</li> <li>A. Item?</li> <li>Q. Item 8. It's on page H4143. Do you see it? Just there.</li> <li>A. Yes, yes.</li> <li>Q. Then we can pick that document up at H4173.</li> <li>A. Yes.</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	<ul> <li>Remove both protective cap on the rebar and the coupler.</li> <li>Fully engage the thread using hand to the coupler.</li> <li>This should develop full tensile strength of the splice once fully engaged."</li> <li>Then step 3, "Lock the splice":</li> <li>"Use a typical pipe wrench to tighten the splice.</li> <li>No special torque amount is required."</li> <li>Now, it's obvious, is it not, that there's absolutely no reference to, is there, to a requirement for a butt-to-butt connection; that's correct, isn't it?</li> <li>A. No, it's not.</li> <li>Q. Well, where do you see it there?</li> <li>A. If you follow these four steps as shown on the instruction, I think for the first one, they say the first one needs to be tightened to the end; right?</li> <li>Q. Sorry, where are you looking?</li> <li>A. Step number 1.</li> <li>Q. Right.</li> </ul>
3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	<ul> <li>Q. If you look back at your report on page 26, one can see, can one not, in the summary, number 2: <ul> <li>"Please refer to our Seisplice technical and quality assurance manual"</li> <li>That is the same document, is it not, that we are looking at at H4142?</li> </ul> </li> <li>A. Agree.</li> <li>Q. Then if we go over to H4143, we've got a "Content" page, and if we look together at item 8, we can see, can we not, the "Seisplice standard ductility coupler coupler installation method"; do you see that?</li> <li>A. Item?</li> <li>Q. Item 8. It's on page H4143. Do you see it? Just there.</li> <li>A. Yes, yes.</li> <li>Q. Then we can pick that document up at H4173.</li> <li>A. Yes.</li> <li>Q. Do you see, at the top of the page, the BOSA logo? Do you see that?</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	<ul> <li>Remove both protective cap on the rebar and the coupler.</li> <li>Fully engage the thread using hand to the coupler.</li> <li>This should develop full tensile strength of the splice once fully engaged."</li> <li>Then step 3, "Lock the splice":</li> <li>"Use a typical pipe wrench to tighten the splice.</li> <li>No special torque amount is required."</li> <li>Now, it's obvious, is it not, that there's absolutely no reference to, is there, to a requirement for a butt-to-butt connection; that's correct, isn't it?</li> <li>A. No, it's not.</li> <li>Q. Well, where do you see it there?</li> <li>A. If you follow these four steps as shown on the instruction, I think for the first one, they say the first one needs to be tightened to the end; right?</li> <li>Q. Sorry, where are you looking?</li> <li>A. Step number 1.</li> <li>Q. Right.</li> <li>A. The coupler needs to go all the way to the end of the</li> </ul>
3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	<ul> <li>Q. If you look back at your report on page 26, one can see, can one not, in the summary, number 2: <ul> <li>"Please refer to our Seisplice technical and quality assurance manual"</li> <li>That is the same document, is it not, that we are looking at at H4142?</li> </ul> </li> <li>A. Agree.</li> <li>Q. Then if we go over to H4143, we've got a "Content" page, and if we look together at item 8, we can see, can we not, the "Seisplice standard ductility coupler coupler installation method"; do you see that?</li> <li>A. Item?</li> <li>Q. Item 8. It's on page H4143. Do you see it? Just there.</li> <li>A. Yes, yes.</li> <li>Q. Then we can pick that document up at H4173.</li> <li>A. Yes.</li> <li>Q. Do you see, at the top of the page, the BOSA logo? Do you see that?</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	<ul> <li>Remove both protective cap on the rebar and the coupler.</li> <li>Fully engage the thread using hand to the coupler.</li> <li>This should develop full tensile strength of the splice once fully engaged."</li> <li>Then step 3, "Lock the splice":</li> <li>"Use a typical pipe wrench to tighten the splice.</li> <li>No special torque amount is required."</li> <li>Now, it's obvious, is it not, that there's absolutely no reference to, is there, to a requirement for a butt-to-butt connection; that's correct, isn't it?</li> <li>A. No, it's not.</li> <li>Q. Well, where do you see it there?</li> <li>A. If you follow these four steps as shown on the instruction, I think for the first one, they say the first one needs to be tightened to the end; right?</li> <li>Q. Sorry, where are you looking?</li> <li>A. Step number 1.</li> <li>Q. Right.</li> </ul>
3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>Q. If you look back at your report on page 26, one can see, can one not, in the summary, number 2: <ul> <li>"Please refer to our Seisplice technical and quality assurance manual"</li> <li>That is the same document, is it not, that we are looking at at H4142?</li> </ul> </li> <li>A. Agree.</li> <li>Q. Then if we go over to H4143, we've got a "Content" page, and if we look together at item 8, we can see, can we not, the "Seisplice standard ductility coupler coupler installation method"; do you see that?</li> <li>A. Item?</li> <li>Q. Item 8. It's on page H4143. Do you see it? Just there.</li> <li>A. Yes, yes.</li> <li>Q. Then we can pick that document up at H4173.</li> <li>A. Yes.</li> <li>Q. Do you see, at the top of the page, the BOSA logo? Do you see that?</li> <li>A. Yes.</li> <li>Q. Thank you. "Coupler installation method (standard</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>Remove both protective cap on the rebar and the coupler.</li> <li>Fully engage the thread using hand to the coupler.</li> <li>This should develop full tensile strength of the splice once fully engaged."</li> <li>Then step 3, "Lock the splice":</li> <li>"Use a typical pipe wrench to tighten the splice.</li> <li>No special torque amount is required."</li> <li>Now, it's obvious, is it not, that there's absolutely no reference to, is there, to a requirement for a butt-to-butt connection; that's correct, isn't it?</li> <li>A. No, it's not.</li> <li>Q. Well, where do you see it there?</li> <li>A. If you follow these four steps as shown on the instruction, I think for the first one, they say the first one needs to be tightened to the end; right?</li> <li>Q. Sorry, where are you looking?</li> <li>A. Step number 1.</li> <li>Q. Right.</li> <li>A. The coupler needs to go all the way to the end of the parent bar; right?</li> </ul>

	Page 25		Page 27
1	A. No, I try to answer the question. The way you know it	1	more." Then they will go on to the last step, "Put
2	is because when you tighten the coupler, you are using	2	a wrench on it and put more force on it to make sure it
3	up at the threads on the parent bar and your coupler	3	doesn't go in any further".
4	cannot go in any more. That's the way you know you	4	If at that point they still see threads exposing
5	reach the end of the parent bar.	5	from the coupler, that means the bar cannot go in, and
6	Q. Right. Then you've got the continuation bar.	6	the instruction they got is if the exposed bar is not
7	A. I've got the continuation bar to come in.	7	more than two, we can accept it.
8	Q. Absolutely, and you are allowed to have a maximum of two	8	Q. That's all very interesting, Prof Yeung, but none of the
9	threads showing; correct? That's correct, isn't it?	9	instructions that you would give your worker can be
10	A. You are allowed when your bar cannot go in any more.	10	found in this document, can they?
11	Q. No, you are allowed to have two threads showing. That	11	A. I can find it. It's "fully engage the threads".
12	is clear from your figure 4, "Summary":	12	Q. There, they are talking about the initial step, using
13	"After connection has been fully tightened, one	13	your hand to put the rebar into the coupler. That's
14	should see a maximum of two full threads to ensure	14	what they're talking about. That's the step you do by
15	a proper installation."	15	your hand, isn't it?
16	A. But during construction, if you look at the last step on	16	A. Fully engage?
17	this page that you have just shown me	17	Q. Yes, to make sure you can screw it in. Then, once you
18	Q. Step 3?	18	have done that, you use a typical pipe wrench to tighten
19	A. Step 3, you try to hand-tighten it, right, until the bar	19	the splice. So you put it in using your hand, that's
20	doesn't go in any more.	20	a manual operation, to make sure you can screw it in.
21	Q. Right.	21	You might have to get a bit of dust out or a little bit
22	A. How do you know the bar cannot go in any more? It's	22	of debris. Then once you've done that, you get
23	either this bar has the butt of this bar, of the	23	the wrench, and we've seen pictures of that, and you
24	continuation bar, hit the butt of the parent bar.	24	tighten it, and when you've got your two threads
25	That's why your bar cannot go in any more.	25	showing, you can say "job done", can't you?
	Page 26		Page 28
1	Q. No. It doesn't say anything here about putting the	1	A. I think you keep avoiding the word "fully" in the
2	continuation bar in until it cannot go any further.	2	instruction.
3	What it says is you position the continuation bar, you	3	Q. Well, there we are.
4	remove the protective cap on the rebar and the coupler,	4	Let me put this situation to you. Of course, when
5	and you fully engage the thread using hand to coupler.	5	you are screwing in this rebar, by hand or indeed by
6	"This should develop full tensile strength of the splice	6	a wrench, what would happen if you hit a bit of debris
7	once fully engaged.	7	there? How do you know that that wasn't the butt that
8	3: Lock the splice.	8	you contend for? If you hit a bit of debris, you would
9	Use a typical pipe wrench to tighten the splice.	9	be led to believe, wouldn't you, that you had hit the
10	No special torque amount is required."	10	butt; that's right, isn't it?
11	What I've got to suggest to you, Prof Yeung, this	11	A. That is correct, but that is not the intent, to leave
12	says absolutely nothing whatsoever about the need for	12	a gap in there. That means you are talking about
13	a butt-to-butt connection, does it?	13	an error in the construction.
14	A. I don't think so.	14	Q. We can all read that for ourselves and that's the BOSA
15	Q. Good. You are agreeing with me then?	15	coupler installation method.
16	A. No, I don't. If I'm going to tell my construction	16	We looked pretty hard and we can find one reference
17	worker I don't want to say something discriminating	17	to butt-to-butt and I want to discuss it with you. If
18 19	but in Hong Kong most construction workers are not really highly educated. I think that may apply to many	18 19	you would be kind enough to go to H4265. Here we've got the "Quality supervision plan on enhanced site
19 20		19 20	supervision and independent audit checking by MTRC and
20 21	parts of the world. So when I look at step number 3, what I would instruct my worker to do is, "Use your	20 21	RC for the installation of couplers", and we can see
21 22	hand, keep tighten it until you cannot go in any	21	that they're talking there, can we not, about the
22 23	nana, keep ugneen it until you calliot go ill ally		· ·
Z. 1	further" Isn't that another easier instruction to give	23	type II coupler: correct?
23 24	further". Isn't that another easier instruction to give to your worker? I think that's the easiest thing I can	23 24	type II coupler; correct? A. Correct.

7 (Pages 25 to 28)

	Page 29		Page 31
1	contained in the QSP, and then there's a box below it,	1	looking at, there is indeed a requirement for
2	and we've got managed to establish where that comes	2	a butt-to-butt connection, but I think that's a matter
3	from, but let's look at that together. It says:	3	of submission, Professor. Thank you very much indeed.
4	"The tolerance established in the table above	4	WITNESS: Thank you.
5	provides a lower limit on the permissible variation of	5	Questioning by THE COMMISSIONERS
6	the length of the threaded bar.	6	CHAIRMAN: Sorry, Professor, can I ask you this, and I do so
7	The larger the nominal size of the rebar, the	7	very much in the knowledge of what Mr Boulding has
8	greater the tolerance allowed."	8	commented, namely that your suggestion of what you would
9	Then there's a note:	9	say to workers on site, obviously it appears nowhere
10	"BOSA CNC threading machines are always programmed	10	here, but if butt-to-butt connection was vital or
11	by default to allow a positive tolerance on the thread	11	entirely necessary to ensure integrity, speaking as
12	length. This is to ensure butt-to-butt connections can	12	a layperson, would you not have something written down
13	always be achieved when the rebar are spliced inside the	13	saying, "Ensure there is butt-to-butt connection.
14	coupler[s]."	14	Important: ensure butt-to-butt connection", or something
15	Now, that's the only reference we can find to	15	like that, because then everybody on site knows the two
16	"butt-to-butt" at all, and it's a matter of legal	16	threads whatever the mathematics of that is we will
17	submission as to what that means, but what I would	17	come to later but you have to have butt-to-butt
18	suggest to you is that it's not setting out any sort of	18	connection, because if you don't, you could have
19	mandatory requirement, is it, that there always has to	19	difficulty?
20	be a butt-to-butt connection so far as the two pieces of	20	A. From a practical standpoint, when you are a construction
21	rebar are concerned?	21	worker trying to tighten bar in a coupler, there's no
22	A. Counsel, I think you have just mentioned to us this is	22	way you can really guarantee you get butt-to-butt. When
23	part of a legal submission.	23	you think about a normal construction worker, the only
24	Q. Yes.	24	thing he knows is, "I keep tightening, I clearly cannot
25	A. And this legal submission has been approved by the BD.	25	go any further in", and then my supervisor may ask me to
	Page 30		Page 32
1	Q. Yes.	1	check, "If you cannot go any further, how much is left
1 2	<ul><li>Q. Yes.</li><li>A. And on this construction site, this instruction becomes</li></ul>	1 2	check, "If you cannot go any further, how much is left outside the coupler? If there's only two, okay, take
	<ul><li>Q. Yes.</li><li>A. And on this construction site, this instruction becomes a mandatory instruction.</li></ul>		check, "If you cannot go any further, how much is left outside the coupler? If there's only two, okay, take it. More than two, take it out, do it again." The easy
2 3 4	<ul><li>Q. Yes.</li><li>A. And on this construction site, this instruction becomes a mandatory instruction.</li><li>Q. Well, it depends what it means, doesn't it? What I've</li></ul>	2 3 4	check, "If you cannot go any further, how much is left outside the coupler? If there's only two, okay, take it. More than two, take it out, do it again." The easy way to do it
2 3 4 5	<ul><li>Q. Yes.</li><li>A. And on this construction site, this instruction becomes a mandatory instruction.</li><li>Q. Well, it depends what it means, doesn't it? What I've got to suggest to you is that if you look back at your</li></ul>	2 3	check, "If you cannot go any further, how much is left outside the coupler? If there's only two, okay, take it. More than two, take it out, do it again." The easy way to do it CHAIRMAN: So if you're trying to get it in and for all
2 3 4 5 6	<ul><li>Q. Yes.</li><li>A. And on this construction site, this instruction becomes a mandatory instruction.</li><li>Q. Well, it depends what it means, doesn't it? What I've got to suggest to you is that if you look back at your figure 4, if you look at the BOSA acceptable thread</li></ul>	2 3 4 5 6	<ul> <li>check, "If you cannot go any further, how much is left outside the coupler? If there's only two, okay, take</li> <li>it. More than two, take it out, do it again." The easy way to do it</li> <li>CHAIRMAN: So if you're trying to get it in and for all sorts of reasons you can't get butt-to-butt, have</li> </ul>
2 3 4 5 6 7	<ul><li>Q. Yes.</li><li>A. And on this construction site, this instruction becomes a mandatory instruction.</li><li>Q. Well, it depends what it means, doesn't it? What I've got to suggest to you is that if you look back at your figure 4, if you look at the BOSA acceptable thread tolerance, and "After connection has been fully</li></ul>	2 3 4 5 6 7	<ul> <li>check, "If you cannot go any further, how much is left outside the coupler? If there's only two, okay, take it. More than two, take it out, do it again." The easy way to do it</li> <li>CHAIRMAN: So if you're trying to get it in and for all sorts of reasons you can't get butt-to-butt, have a look; if there's two there, you're okay. I'm the</li> </ul>
2 3 4 5 6 7 8	<ul> <li>Q. Yes.</li> <li>A. And on this construction site, this instruction becomes a mandatory instruction.</li> <li>Q. Well, it depends what it means, doesn't it? What I've got to suggest to you is that if you look back at your figure 4, if you look at the BOSA acceptable thread tolerance, and "After connection has been fully tightened, one should see a maximum of two full threads</li> </ul>	2 3 4 5 6 7 8	<ul> <li>check, "If you cannot go any further, how much is left outside the coupler? If there's only two, okay, take it. More than two, take it out, do it again." The easy way to do it</li> <li>CHAIRMAN: So if you're trying to get it in and for all sorts of reasons you can't get butt-to-butt, have a look; if there's two there, you're okay. I'm the world's worst do-it-yourself person, so I have lots of</li> </ul>
2 3 4 5 6 7 8 9	<ul> <li>Q. Yes.</li> <li>A. And on this construction site, this instruction becomes a mandatory instruction.</li> <li>Q. Well, it depends what it means, doesn't it? What I've got to suggest to you is that if you look back at your figure 4, if you look at the BOSA acceptable thread tolerance, and "After connection has been fully tightened, one should see a maximum of two full threads to ensure a proper installation", if you are allowed to</li> </ul>	2 3 4 5 6 7 8 9	<ul> <li>check, "If you cannot go any further, how much is left outside the coupler? If there's only two, okay, take it. More than two, take it out, do it again." The easy way to do it</li> <li>CHAIRMAN: So if you're trying to get it in and for all sorts of reasons you can't get butt-to-butt, have a look; if there's two there, you're okay. I'm the world's worst do-it-yourself person, so I have lots of experience in this. You take a screw, you try to screw</li> </ul>
2 3 4 5 6 7 8 9 10	<ul> <li>Q. Yes.</li> <li>A. And on this construction site, this instruction becomes a mandatory instruction.</li> <li>Q. Well, it depends what it means, doesn't it? What I've got to suggest to you is that if you look back at your figure 4, if you look at the BOSA acceptable thread tolerance, and "After connection has been fully tightened, one should see a maximum of two full threads to ensure a proper installation", if you are allowed to have a maximum of two full threads to ensure proper</li> </ul>	2 3 4 5 6 7 8 9 10	<ul> <li>check, "If you cannot go any further, how much is left outside the coupler? If there's only two, okay, take it. More than two, take it out, do it again." The easy way to do it</li> <li>CHAIRMAN: So if you're trying to get it in and for all sorts of reasons you can't get butt-to-butt, have a look; if there's two there, you're okay. I'm the world's worst do-it-yourself person, so I have lots of experience in this. You take a screw, you try to screw it into something where the wood perhaps is a little</li> </ul>
2 3 4 5 6 7 8 9 10 11	<ul> <li>Q. Yes.</li> <li>A. And on this construction site, this instruction becomes a mandatory instruction.</li> <li>Q. Well, it depends what it means, doesn't it? What I've got to suggest to you is that if you look back at your figure 4, if you look at the BOSA acceptable thread tolerance, and "After connection has been fully tightened, one should see a maximum of two full threads to ensure a proper installation", if you are allowed to have a maximum of two full threads to ensure proper installation, what I would suggest is you would never</li> </ul>	2 3 4 5 6 7 8 9 10 11	<ul> <li>check, "If you cannot go any further, how much is left outside the coupler? If there's only two, okay, take it. More than two, take it out, do it again." The easy way to do it</li> <li>CHAIRMAN: So if you're trying to get it in and for all sorts of reasons you can't get butt-to-butt, have a look; if there's two there, you're okay. I'm the world's worst do-it-yourself person, so I have lots of experience in this. You take a screw, you try to screw it into something where the wood perhaps is a little warped or difficult and you suddenly find you've still</li> </ul>
2 3 4 5 6 7 8 9 10 11 12	<ul> <li>Q. Yes.</li> <li>A. And on this construction site, this instruction becomes a mandatory instruction.</li> <li>Q. Well, it depends what it means, doesn't it? What I've got to suggest to you is that if you look back at your figure 4, if you look at the BOSA acceptable thread tolerance, and "After connection has been fully tightened, one should see a maximum of two full threads to ensure a proper installation", if you are allowed to have a maximum of two full threads to ensure proper installation, what I would suggest is you would never have a butt-to-butt connection; that's right, isn't it?</li> </ul>	2 3 4 5 6 7 8 9 10 11 12	<ul> <li>check, "If you cannot go any further, how much is left outside the coupler? If there's only two, okay, take it. More than two, take it out, do it again." The easy way to do it</li> <li>CHAIRMAN: So if you're trying to get it in and for all sorts of reasons you can't get butt-to-butt, have a look; if there's two there, you're okay. I'm the world's worst do-it-yourself person, so I have lots of experience in this. You take a screw, you try to screw it into something where the wood perhaps is a little warped or difficult and you suddenly find you've still got about three screws left on your screw but you can't</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13	<ul> <li>Q. Yes.</li> <li>A. And on this construction site, this instruction becomes a mandatory instruction.</li> <li>Q. Well, it depends what it means, doesn't it? What I've got to suggest to you is that if you look back at your figure 4, if you look at the BOSA acceptable thread tolerance, and "After connection has been fully tightened, one should see a maximum of two full threads to ensure a proper installation", if you are allowed to have a maximum of two full threads to ensure proper installation, what I would suggest is you would never have a butt-to-butt connection; that's right, isn't it?</li> <li>A. I don't agree. The number doesn't add up.</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13	<ul> <li>check, "If you cannot go any further, how much is left outside the coupler? If there's only two, okay, take it. More than two, take it out, do it again." The easy way to do it</li> <li>CHAIRMAN: So if you're trying to get it in and for all sorts of reasons you can't get butt-to-butt, have a look; if there's two there, you're okay. I'm the world's worst do-it-yourself person, so I have lots of experience in this. You take a screw, you try to screw it into something where the wood perhaps is a little warped or difficult and you suddenly find you've still got about three screws left on your screw but you can't get it in any further; okay? You then look and you test</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14	<ul> <li>Q. Yes.</li> <li>A. And on this construction site, this instruction becomes a mandatory instruction.</li> <li>Q. Well, it depends what it means, doesn't it? What I've got to suggest to you is that if you look back at your figure 4, if you look at the BOSA acceptable thread tolerance, and "After connection has been fully tightened, one should see a maximum of two full threads to ensure a proper installation", if you are allowed to have a maximum of two full threads to ensure proper installation, what I would suggest is you would never have a butt-to-butt connection; that's right, isn't it?</li> <li>A. I don't agree. The number doesn't add up.</li> <li>MR BOULDING: Thank you, Professor.</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14	<ul> <li>check, "If you cannot go any further, how much is left outside the coupler? If there's only two, okay, take it. More than two, take it out, do it again." The easy way to do it</li> <li>CHAIRMAN: So if you're trying to get it in and for all sorts of reasons you can't get butt-to-butt, have a look; if there's two there, you're okay. I'm the world's worst do-it-yourself person, so I have lots of experience in this. You take a screw, you try to screw it into something where the wood perhaps is a little warped or difficult and you suddenly find you've still got about three screws left on your screw but you can't get it in any further; okay? You then look and you test it and it doesn't look too good because it should really</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15	<ul> <li>Q. Yes.</li> <li>A. And on this construction site, this instruction becomes a mandatory instruction.</li> <li>Q. Well, it depends what it means, doesn't it? What I've got to suggest to you is that if you look back at your figure 4, if you look at the BOSA acceptable thread tolerance, and "After connection has been fully tightened, one should see a maximum of two full threads to ensure a proper installation", if you are allowed to have a maximum of two full threads to ensure proper installation, what I would suggest is you would never have a butt-to-butt connection; that's right, isn't it?</li> <li>A. I don't agree. The number doesn't add up.</li> <li>MR BOULDING: Thank you, Professor.</li> <li>A. I would add one more point to the Commissioners.</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15	<ul> <li>check, "If you cannot go any further, how much is left outside the coupler? If there's only two, okay, take it. More than two, take it out, do it again." The easy way to do it</li> <li>CHAIRMAN: So if you're trying to get it in and for all sorts of reasons you can't get butt-to-butt, have a look; if there's two there, you're okay. I'm the world's worst do-it-yourself person, so I have lots of experience in this. You take a screw, you try to screw it into something where the wood perhaps is a little warped or difficult and you suddenly find you've still got about three screws left on your screw but you can't get it in any further; okay? You then look and you test it and it doesn't look too good because it should really be in fully, but that's as far as you can go; you've</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	<ul> <li>Q. Yes.</li> <li>A. And on this construction site, this instruction becomes a mandatory instruction.</li> <li>Q. Well, it depends what it means, doesn't it? What I've got to suggest to you is that if you look back at your figure 4, if you look at the BOSA acceptable thread tolerance, and "After connection has been fully tightened, one should see a maximum of two full threads to ensure a proper installation", if you are allowed to have a maximum of two full threads to ensure proper installation, what I would suggest is you would never have a butt-to-butt connection; that's right, isn't it?</li> <li>A. I don't agree. The number doesn't add up.</li> <li>MR BOULDING: Thank you, Professor.</li> <li>A. I would add one more point to the Commissioners. I think you may have seen the TV, doing the</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	<ul> <li>check, "If you cannot go any further, how much is left outside the coupler? If there's only two, okay, take it. More than two, take it out, do it again." The easy way to do it</li> <li>CHAIRMAN: So if you're trying to get it in and for all sorts of reasons you can't get butt-to-butt, have a look; if there's two there, you're okay. I'm the world's worst do-it-yourself person, so I have lots of experience in this. You take a screw, you try to screw it into something where the wood perhaps is a little warped or difficult and you suddenly find you've still got about three screws left on your screw but you can't get it in any further; okay? You then look and you test it and it doesn't look too good because it should really be in fully, but that's as far as you can go; you've achieved what you can. Is that not the same thing here?</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	<ul> <li>Q. Yes.</li> <li>A. And on this construction site, this instruction becomes a mandatory instruction.</li> <li>Q. Well, it depends what it means, doesn't it? What I've got to suggest to you is that if you look back at your figure 4, if you look at the BOSA acceptable thread tolerance, and "After connection has been fully tightened, one should see a maximum of two full threads to ensure a proper installation", if you are allowed to have a maximum of two full threads to ensure proper installation, what I would suggest is you would never have a butt-to-butt connection; that's right, isn't it?</li> <li>A. I don't agree. The number doesn't add up.</li> <li>MR BOULDING: Thank you, Professor.</li> <li>A. I would add one more point to the Commissioners. I think you may have seen the TV, doing the interview, the project director of MTR can do this</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	<ul> <li>check, "If you cannot go any further, how much is left outside the coupler? If there's only two, okay, take it. More than two, take it out, do it again." The easy way to do it</li> <li>CHAIRMAN: So if you're trying to get it in and for all sorts of reasons you can't get butt-to-butt, have a look; if there's two there, you're okay. I'm the world's worst do-it-yourself person, so I have lots of experience in this. You take a screw, you try to screw it into something where the wood perhaps is a little warped or difficult and you suddenly find you've still got about three screws left on your screw but you can't get it in any further; okay? You then look and you test it and it doesn't look too good because it should really be in fully, but that's as far as you can go; you've achieved what you can. Is that not the same thing here? It doesn't say it must be butt-to-butt because (a) you</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	<ul> <li>Q. Yes.</li> <li>A. And on this construction site, this instruction becomes a mandatory instruction.</li> <li>Q. Well, it depends what it means, doesn't it? What I've got to suggest to you is that if you look back at your figure 4, if you look at the BOSA acceptable thread tolerance, and "After connection has been fully tightened, one should see a maximum of two full threads to ensure a proper installation", if you are allowed to have a maximum of two full threads to ensure proper installation, what I would suggest is you would never have a butt-to-butt connection; that's right, isn't it?</li> <li>A. I don't agree. The number doesn't add up.</li> <li>MR BOULDING: Thank you, Professor.</li> <li>A. I would add one more point to the Commissioners. I think you may have seen the TV, doing the interview, the project director of MTR can do this connection by hand, even like us in suits. So that</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	check, "If you cannot go any further, how much is left outside the coupler? If there's only two, okay, take it. More than two, take it out, do it again." The easy way to do it CHAIRMAN: So if you're trying to get it in and for all sorts of reasons you can't get butt-to-butt, have a look; if there's two there, you're okay. I'm the world's worst do-it-yourself person, so I have lots of experience in this. You take a screw, you try to screw it into something where the wood perhaps is a little warped or difficult and you suddenly find you've still got about three screws left on your screw but you can't get it in any further; okay? You then look and you test it and it doesn't look too good because it should really be in fully, but that's as far as you can go; you've achieved what you can. Is that not the same thing here? It doesn't say it must be butt-to-butt because (a) you can never tell if it in fact is, unless you have x-ray
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	<ul> <li>Q. Yes.</li> <li>A. And on this construction site, this instruction becomes a mandatory instruction.</li> <li>Q. Well, it depends what it means, doesn't it? What I've got to suggest to you is that if you look back at your figure 4, if you look at the BOSA acceptable thread tolerance, and "After connection has been fully tightened, one should see a maximum of two full threads to ensure a proper installation", if you are allowed to have a maximum of two full threads to ensure proper installation, what I would suggest is you would never have a butt-to-butt connection; that's right, isn't it?</li> <li>A. I don't agree. The number doesn't add up.</li> <li>MR BOULDING: Thank you, Professor.</li> <li>A. I would add one more point to the Commissioners. I think you may have seen the TV, doing the interview, the project director of MTR can do this connection by hand, even like us in suits. So that tells you one thing. Even though you try to fit it by</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	check, "If you cannot go any further, how much is left outside the coupler? If there's only two, okay, take it. More than two, take it out, do it again." The easy way to do it CHAIRMAN: So if you're trying to get it in and for all sorts of reasons you can't get butt-to-butt, have a look; if there's two there, you're okay. I'm the world's worst do-it-yourself person, so I have lots of experience in this. You take a screw, you try to screw it into something where the wood perhaps is a little warped or difficult and you suddenly find you've still got about three screws left on your screw but you can't get it in any further; okay? You then look and you test it and it doesn't look too good because it should really be in fully, but that's as far as you can go; you've achieved what you can. Is that not the same thing here? It doesn't say it must be butt-to-butt because (a) you can never tell if it in fact is, unless you have x-ray eyes, and we don't
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	<ul> <li>Q. Yes.</li> <li>A. And on this construction site, this instruction becomes a mandatory instruction.</li> <li>Q. Well, it depends what it means, doesn't it? What I've got to suggest to you is that if you look back at your figure 4, if you look at the BOSA acceptable thread tolerance, and "After connection has been fully tightened, one should see a maximum of two full threads to ensure a proper installation", if you are allowed to have a maximum of two full threads to ensure proper installation, what I would suggest is you would never have a butt-to-butt connection; that's right, isn't it?</li> <li>A. I don't agree. The number doesn't add up.</li> <li>MR BOULDING: Thank you, Professor.</li> <li>A. I would add one more point to the Commissioners. I think you may have seen the TV, doing the interview, the project director of MTR can do this connection by hand, even like us in suits. So that tells you one thing. Even though you try to fit it by hand, it's very easy to fit in. There's no point for</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	<ul> <li>check, "If you cannot go any further, how much is left outside the coupler? If there's only two, okay, take it. More than two, take it out, do it again." The easy way to do it</li> <li>CHAIRMAN: So if you're trying to get it in and for all sorts of reasons you can't get butt-to-butt, have a look; if there's two there, you're okay. I'm the world's worst do-it-yourself person, so I have lots of experience in this. You take a screw, you try to screw it into something where the wood perhaps is a little warped or difficult and you suddenly find you've still got about three screws left on your screw but you can't get it in any further; okay? You then look and you test it and it doesn't look too good because it should really be in fully, but that's as far as you can go; you've achieved what you can. Is that not the same thing here? It doesn't say it must be butt-to-butt because (a) you can never tell if it in fact is, unless you have x-ray eyes, and we don't</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	<ul> <li>Q. Yes.</li> <li>A. And on this construction site, this instruction becomes a mandatory instruction.</li> <li>Q. Well, it depends what it means, doesn't it? What I've got to suggest to you is that if you look back at your figure 4, if you look at the BOSA acceptable thread tolerance, and "After connection has been fully tightened, one should see a maximum of two full threads to ensure a proper installation", if you are allowed to have a maximum of two full threads to ensure proper installation, what I would suggest is you would never have a butt-to-butt connection; that's right, isn't it?</li> <li>A. I don't agree. The number doesn't add up.</li> <li>MR BOULDING: Thank you, Professor.</li> <li>A. I would add one more point to the Commissioners. I think you may have seen the TV, doing the interview, the project director of MTR can do this connection by hand, even like us in suits. So that tells you one thing. Even though you try to fit it by hand, it's very easy to fit in. There's no point for a construction worker to try to stop somewhere in</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	<ul> <li>check, "If you cannot go any further, how much is left outside the coupler? If there's only two, okay, take it. More than two, take it out, do it again." The easy way to do it</li> <li>CHAIRMAN: So if you're trying to get it in and for all sorts of reasons you can't get butt-to-butt, have a look; if there's two there, you're okay. I'm the world's worst do-it-yourself person, so I have lots of experience in this. You take a screw, you try to screw it into something where the wood perhaps is a little warped or difficult and you suddenly find you've still got about three screws left on your screw but you can't get it in any further; okay? You then look and you test it and it doesn't look too good because it should really be in fully, but that's as far as you can go; you've achieved what you can. Is that not the same thing here? It doesn't say it must be butt-to-butt because (a) you can never tell if it in fact is, unless you have x-ray eyes, and we don't</li> <li>A. Yes.</li> <li>CHAIRMAN: that's number one. But number two, accepting</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>Q. Yes.</li> <li>A. And on this construction site, this instruction becomes a mandatory instruction.</li> <li>Q. Well, it depends what it means, doesn't it? What I've got to suggest to you is that if you look back at your figure 4, if you look at the BOSA acceptable thread tolerance, and "After connection has been fully tightened, one should see a maximum of two full threads to ensure a proper installation", if you are allowed to have a maximum of two full threads to ensure proper installation, what I would suggest is you would never have a butt-to-butt connection; that's right, isn't it?</li> <li>A. I don't agree. The number doesn't add up.</li> <li>MR BOULDING: Thank you, Professor.</li> <li>A. I would add one more point to the Commissioners. I think you may have seen the TV, doing the interview, the project director of MTR can do this connection by hand, even like us in suits. So that tells you one thing. Even though you try to fit it by hand, it's very easy to fit in. There's no point for a construction worker to try to stop somewhere in between without getting into a butt-to-butt situation.</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>check, "If you cannot go any further, how much is left outside the coupler? If there's only two, okay, take it. More than two, take it out, do it again." The easy way to do it</li> <li>CHAIRMAN: So if you're trying to get it in and for all sorts of reasons you can't get butt-to-butt, have a look; if there's two there, you're okay. I'm the world's worst do-it-yourself person, so I have lots of experience in this. You take a screw, you try to screw it into something where the wood perhaps is a little warped or difficult and you suddenly find you've still got about three screws left on your screw but you can't get it in any further; okay? You then look and you test it and it doesn't look too good because it should really be in fully, but that's as far as you can go; you've achieved what you can. Is that not the same thing here? It doesn't say it must be butt-to-butt because (a) you can never tell if it in fact is, unless you have x-ray eyes, and we don't</li> <li>A. Yes.</li> <li>CHAIRMAN: that's number one. But number two, accepting that, providing there's only two screws there or two</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	<ul> <li>Q. Yes.</li> <li>A. And on this construction site, this instruction becomes a mandatory instruction.</li> <li>Q. Well, it depends what it means, doesn't it? What I've got to suggest to you is that if you look back at your figure 4, if you look at the BOSA acceptable thread tolerance, and "After connection has been fully tightened, one should see a maximum of two full threads to ensure a proper installation", if you are allowed to have a maximum of two full threads to ensure proper installation, what I would suggest is you would never have a butt-to-butt connection; that's right, isn't it?</li> <li>A. I don't agree. The number doesn't add up.</li> <li>MR BOULDING: Thank you, Professor.</li> <li>A. I would add one more point to the Commissioners. I think you may have seen the TV, doing the interview, the project director of MTR can do this connection by hand, even like us in suits. So that tells you one thing. Even though you try to fit it by hand, it's very easy to fit in. There's no point for a construction worker to try to stop somewhere in between without getting into a butt-to-butt situation.</li> <li>COMMISSIONER HANSFORD: I've not seen that.</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	<ul> <li>check, "If you cannot go any further, how much is left outside the coupler? If there's only two, okay, take it. More than two, take it out, do it again." The easy way to do it</li> <li>CHAIRMAN: So if you're trying to get it in and for all sorts of reasons you can't get butt-to-butt, have a look; if there's two there, you're okay. I'm the world's worst do-it-yourself person, so I have lots of experience in this. You take a screw, you try to screw it into something where the wood perhaps is a little warped or difficult and you suddenly find you've still got about three screws left on your screw but you can't get it in any further; okay? You then look and you test it and it doesn't look too good because it should really be in fully, but that's as far as you can go; you've achieved what you can. Is that not the same thing here? It doesn't say it must be butt-to-butt because (a) you can never tell if it in fact is, unless you have x-ray eyes, and we don't</li> <li>A. Yes.</li> <li>CHAIRMAN: that's number one. But number two, accepting that, providing there's only two screws there or two threads showing, you're okay. If there are four threads</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>Q. Yes.</li> <li>A. And on this construction site, this instruction becomes a mandatory instruction.</li> <li>Q. Well, it depends what it means, doesn't it? What I've got to suggest to you is that if you look back at your figure 4, if you look at the BOSA acceptable thread tolerance, and "After connection has been fully tightened, one should see a maximum of two full threads to ensure a proper installation", if you are allowed to have a maximum of two full threads to ensure proper installation, what I would suggest is you would never have a butt-to-butt connection; that's right, isn't it?</li> <li>A. I don't agree. The number doesn't add up.</li> <li>MR BOULDING: Thank you, Professor.</li> <li>A. I would add one more point to the Commissioners. I think you may have seen the TV, doing the interview, the project director of MTR can do this connection by hand, even like us in suits. So that tells you one thing. Even though you try to fit it by hand, it's very easy to fit in. There's no point for a construction worker to try to stop somewhere in between without getting into a butt-to-butt situation.</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	<ul> <li>check, "If you cannot go any further, how much is left outside the coupler? If there's only two, okay, take it. More than two, take it out, do it again." The easy way to do it</li> <li>CHAIRMAN: So if you're trying to get it in and for all sorts of reasons you can't get butt-to-butt, have a look; if there's two there, you're okay. I'm the world's worst do-it-yourself person, so I have lots of experience in this. You take a screw, you try to screw it into something where the wood perhaps is a little warped or difficult and you suddenly find you've still got about three screws left on your screw but you can't get it in any further; okay? You then look and you test it and it doesn't look too good because it should really be in fully, but that's as far as you can go; you've achieved what you can. Is that not the same thing here? It doesn't say it must be butt-to-butt because (a) you can never tell if it in fact is, unless you have x-ray eyes, and we don't</li> <li>A. Yes.</li> <li>CHAIRMAN: that's number one. But number two, accepting that, providing there's only two screws there or two</li> </ul>

	Page 33		Page 35
1	threads showing."	1	I haven't got butt-to-butt but I've got a run of nine or
2	A. Mm-hmm.	2	ten of these which are only showing two threads."
3	CHAIRMAN: If he comes across and says, "No, you can't	3	Wouldn't BOSA say that's okay?
4	count, there's two", and you say, "Sorry, yes, there's	4	A. If I'm the resident engineer on site, as a resident
5	two", then everybody is happy. So there hasn't been	5	engineer on site, although I work full-time on site, I'm
6	butt-to-butt but there has been the tolerance level	6	not really full-time on the site because I may be in the
7	of two has been met. Now, that's on what I might call	7	site office, working on paperwork and other things.
8	the workability basis on site.	8	CHAIRMAN: No, I appreciate that.
9	Now, whether in fact two itself is over-engineering,	9	A. But I still inspect my site from time to time. If
10	I don't know. That's something else. That's like in	10	I encounter the hypothetical situation you have
11	pharmacy they say, "Only take two pills a day", but in	11	mentioned, that I got 30 bars there and all 30 bars got
12	fact, if you take three, that's okay, but they don't	12	two threads sticking out, I would do an evaluation to
13	want to be sued if somebody's got some particular	13	see what happened.
14	problem. Do you see what I mean?	14	CHAIRMAN: But you are a professor and you are involved at
15	A. I fully understand what you mean. That's exactly the	15	a much higher level. I'm talking about ordinary,
16	condition while you are working on site. I tell my	16	everyday construction methodology. What I'm saying,
17	worker, "Go as far as you can, until you cannot go in	17	I suppose, is this: surely, if BOSA demanded
18	any further", but if you like, what you have mentioned,	18	butt-to-butt, and they would only demand it for safety
19	you come back and say, "I tried my best, still two out	19	and structural integrity reasons, they would say so.
20	there", and we understand construction is never perfect	20	But they don't, they say two threads is okay. That's
20	and this is the kind of thing we need to allow for, and	21	not an invitation not to have two threads, because
21	exactly what we talk about in this Commission, I think	22	by and large if everything's lined up, you can just
22	many engineers will mention to you what a factor of	23	screw away and clunk, you've hit the butt; do you see
23	safety is, and so. Those are something we try to cover,	24	what I mean?
25	some of the imperfections in construction.	25	A. And then two threads was caused by the tolerance,
25			
			Page 36
1	Page 34 CHAIRMAN: So BOSA must then build into their engineering of	1	Page 36 because that's the one mentioned about full tolerance.
1	CHAIRMAN: So BOSA must then build into their engineering of		because that's the one mentioned about full tolerance,
2	CHAIRMAN: So BOSA must then build into their engineering of these things a situation where because maybe the angle	2	because that's the one mentioned about full tolerance, that means the threaded section is longer than design.
2 3	CHAIRMAN: So BOSA must then build into their engineering of these things a situation where because maybe the angle is not 100 per cent right, because the thread perhaps is	2 3	because that's the one mentioned about full tolerance, that means the threaded section is longer than design. So you can still maintain the ten threads in the
2 3 4	CHAIRMAN: So BOSA must then build into their engineering of these things a situation where because maybe the angle is not 100 per cent right, because the thread perhaps is not fully beautifully honed, that you might not get	2 3 4	because that's the one mentioned about full tolerance, that means the threaded section is longer than design. So you can still maintain the ten threads in the coupler. That's what they mean by full tolerance on the
2 3 4 5	CHAIRMAN: So BOSA must then build into their engineering of these things a situation where because maybe the angle is not 100 per cent right, because the thread perhaps is not fully beautifully honed, that you might not get fully in, so you don't have to have butt-to-butt,	2 3 4 5	because that's the one mentioned about full tolerance, that means the threaded section is longer than design. So you can still maintain the ten threads in the coupler. That's what they mean by full tolerance on the right side of the figure.
2 3 4 5 6	CHAIRMAN: So BOSA must then build into their engineering of these things a situation where because maybe the angle is not 100 per cent right, because the thread perhaps is not fully beautifully honed, that you might not get fully in, so you don't have to have butt-to-butt, provided you are close enough that only two threads	2 3 4 5 6	because that's the one mentioned about full tolerance, that means the threaded section is longer than design. So you can still maintain the ten threads in the coupler. That's what they mean by full tolerance on the right side of the figure. COMMISSIONER HANSFORD: How do we know that? How do we know
2 3 4 5 6 7	CHAIRMAN: So BOSA must then build into their engineering of these things a situation where because maybe the angle is not 100 per cent right, because the thread perhaps is not fully beautifully honed, that you might not get fully in, so you don't have to have butt-to-butt, provided you are close enough that only two threads show; that will be sufficient?	2 3 4 5 6 7	because that's the one mentioned about full tolerance, that means the threaded section is longer than design. So you can still maintain the ten threads in the coupler. That's what they mean by full tolerance on the right side of the figure. COMMISSIONER HANSFORD: How do we know that? How do we know that's what they mean?
2 3 4 5 6 7 8	<ul><li>CHAIRMAN: So BOSA must then build into their engineering of these things a situation where because maybe the angle is not 100 per cent right, because the thread perhaps is not fully beautifully honed, that you might not get fully in, so you don't have to have butt-to-butt, provided you are close enough that only two threads show; that will be sufficient?</li><li>A. Or I think another very good suggestion is by</li></ul>	2 3 4 5 6	<ul> <li>because that's the one mentioned about full tolerance,</li> <li>that means the threaded section is longer than design.</li> <li>So you can still maintain the ten threads in the</li> <li>coupler. That's what they mean by full tolerance on the</li> <li>right side of the figure.</li> <li>COMMISSIONER HANSFORD: How do we know that? How do we know</li> <li>that's what they mean?</li> <li>A. Because they say "maximum tolerance". That means both</li> </ul>
2 3 4 5 6 7 8 9	<ul><li>CHAIRMAN: So BOSA must then build into their engineering of these things a situation where because maybe the angle is not 100 per cent right, because the thread perhaps is not fully beautifully honed, that you might not get fully in, so you don't have to have butt-to-butt, provided you are close enough that only two threads show; that will be sufficient?</li><li>A. Or I think another very good suggestion is by Mr Boulding, maybe you've got a small piece of debris in</li></ul>	2 3 4 5 6 7 8 9	<ul> <li>because that's the one mentioned about full tolerance,</li> <li>that means the threaded section is longer than design.</li> <li>So you can still maintain the ten threads in the</li> <li>coupler. That's what they mean by full tolerance on the</li> <li>right side of the figure.</li> <li>COMMISSIONER HANSFORD: How do we know that? How do we know</li> <li>that's what they mean?</li> <li>A. Because they say "maximum tolerance". That means both</li> <li>bars get a maximum tolerance and both bars are 48 the</li> </ul>
2 3 4 5 6 7 8 9 10	<ul><li>CHAIRMAN: So BOSA must then build into their engineering of these things a situation where because maybe the angle is not 100 per cent right, because the thread perhaps is not fully beautifully honed, that you might not get fully in, so you don't have to have butt-to-butt, provided you are close enough that only two threads show; that will be sufficient?</li><li>A. Or I think another very good suggestion is by Mr Boulding, maybe you've got a small piece of debris in there, and then simply your bar gets jammed and cannot</li></ul>	2 3 4 5 6 7 8 9 10	<ul> <li>because that's the one mentioned about full tolerance, that means the threaded section is longer than design. So you can still maintain the ten threads in the coupler. That's what they mean by full tolerance on the right side of the figure.</li> <li>COMMISSIONER HANSFORD: How do we know that? How do we know that's what they mean?</li> <li>A. Because they say "maximum tolerance". That means both bars get a maximum tolerance and both bars are 48 the threaded section, both bars are 48mm long.</li> </ul>
2 3 4 5 6 7 8 9 10 11	<ul><li>CHAIRMAN: So BOSA must then build into their engineering of these things a situation where because maybe the angle is not 100 per cent right, because the thread perhaps is not fully beautifully honed, that you might not get fully in, so you don't have to have butt-to-butt, provided you are close enough that only two threads show; that will be sufficient?</li><li>A. Or I think another very good suggestion is by Mr Boulding, maybe you've got a small piece of debris in there, and then simply your bar gets jammed and cannot go in any further.</li></ul>	2 3 4 5 6 7 8 9	<ul> <li>because that's the one mentioned about full tolerance, that means the threaded section is longer than design. So you can still maintain the ten threads in the coupler. That's what they mean by full tolerance on the right side of the figure.</li> <li>COMMISSIONER HANSFORD: How do we know that? How do we know that's what they mean?</li> <li>A. Because they say "maximum tolerance". That means both bars get a maximum tolerance and both bars are 48 the threaded section, both bars are 48mm long.</li> <li>CHAIRMAN: Sorry, so you are saying please forgive me</li> </ul>
2 3 4 5 6 7 8 9 10 11 12	<ul> <li>CHAIRMAN: So BOSA must then build into their engineering of these things a situation where because maybe the angle is not 100 per cent right, because the thread perhaps is not fully beautifully honed, that you might not get fully in, so you don't have to have butt-to-butt, provided you are close enough that only two threads show; that will be sufficient?</li> <li>A. Or I think another very good suggestion is by Mr Boulding, maybe you've got a small piece of debris in there, and then simply your bar gets jammed and cannot go in any further.</li> <li>CHAIRMAN: Yes, but the point I'm making is assuming you've</li> </ul>	2 3 4 5 6 7 8 9 10 11	<ul> <li>because that's the one mentioned about full tolerance, that means the threaded section is longer than design. So you can still maintain the ten threads in the coupler. That's what they mean by full tolerance on the right side of the figure.</li> <li>COMMISSIONER HANSFORD: How do we know that? How do we know that's what they mean?</li> <li>A. Because they say "maximum tolerance". That means both bars get a maximum tolerance and both bars are 48 the threaded section, both bars are 48mm long.</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13	<ul> <li>CHAIRMAN: So BOSA must then build into their engineering of these things a situation where because maybe the angle is not 100 per cent right, because the thread perhaps is not fully beautifully honed, that you might not get fully in, so you don't have to have butt-to-butt, provided you are close enough that only two threads show; that will be sufficient?</li> <li>A. Or I think another very good suggestion is by Mr Boulding, maybe you've got a small piece of debris in there, and then simply your bar gets jammed and cannot go in any further.</li> <li>CHAIRMAN: Yes, but the point I'm making is assuming you've got the diaphragm wall and it's all concreted and you've</li> </ul>	2 3 4 5 6 7 8 9 10 11 12	<ul> <li>because that's the one mentioned about full tolerance, that means the threaded section is longer than design. So you can still maintain the ten threads in the coupler. That's what they mean by full tolerance on the right side of the figure.</li> <li>COMMISSIONER HANSFORD: How do we know that? How do we know that's what they mean?</li> <li>A. Because they say "maximum tolerance". That means both bars get a maximum tolerance and both bars are 48 the threaded section, both bars are 48mm long.</li> <li>CHAIRMAN: Sorry, so you are saying please forgive me the two threads means that you still hit the butt because that's the tolerance?</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14	<ul> <li>CHAIRMAN: So BOSA must then build into their engineering of these things a situation where because maybe the angle is not 100 per cent right, because the thread perhaps is not fully beautifully honed, that you might not get fully in, so you don't have to have butt-to-butt, provided you are close enough that only two threads show; that will be sufficient?</li> <li>A. Or I think another very good suggestion is by Mr Boulding, maybe you've got a small piece of debris in there, and then simply your bar gets jammed and cannot go in any further.</li> <li>CHAIRMAN: Yes, but the point I'm making is assuming you've got the diaphragm wall and it's all concreted and you've used your hydraulics, and actually it presents a rather</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13	<ul> <li>because that's the one mentioned about full tolerance,</li> <li>that means the threaded section is longer than design.</li> <li>So you can still maintain the ten threads in the</li> <li>coupler. That's what they mean by full tolerance on the</li> <li>right side of the figure.</li> <li>COMMISSIONER HANSFORD: How do we know that? How do we know</li> <li>that's what they mean?</li> <li>A. Because they say "maximum tolerance". That means both</li> <li>bars get a maximum tolerance and both bars are 48 the</li> <li>threaded section, both bars are 48mm long.</li> <li>CHAIRMAN: Sorry, so you are saying please forgive me</li> <li>the two threads means that you still hit the butt</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15	<ul> <li>CHAIRMAN: So BOSA must then build into their engineering of these things a situation where because maybe the angle is not 100 per cent right, because the thread perhaps is not fully beautifully honed, that you might not get fully in, so you don't have to have butt-to-butt, provided you are close enough that only two threads show; that will be sufficient?</li> <li>A. Or I think another very good suggestion is by Mr Boulding, maybe you've got a small piece of debris in there, and then simply your bar gets jammed and cannot go in any further.</li> <li>CHAIRMAN: Yes, but the point I'm making is assuming you've got the diaphragm wall and it's all concreted and you've used your hydraulics, and actually it presents a rather difficult situation, some are off at bad angles but</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14	<ul> <li>because that's the one mentioned about full tolerance, that means the threaded section is longer than design. So you can still maintain the ten threads in the coupler. That's what they mean by full tolerance on the right side of the figure.</li> <li>COMMISSIONER HANSFORD: How do we know that? How do we know that's what they mean?</li> <li>A. Because they say "maximum tolerance". That means both bars get a maximum tolerance and both bars are 48 the threaded section, both bars are 48mm long.</li> <li>CHAIRMAN: Sorry, so you are saying please forgive me the two threads means that you still hit the butt because that's the tolerance?</li> <li>A. Yes. I can give you a simple example on the numbers.</li> <li>CHAIRMAN: No, no, I understand that. All right. I'm just</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	<ul> <li>CHAIRMAN: So BOSA must then build into their engineering of these things a situation where because maybe the angle is not 100 per cent right, because the thread perhaps is not fully beautifully honed, that you might not get fully in, so you don't have to have butt-to-butt, provided you are close enough that only two threads show; that will be sufficient?</li> <li>A. Or I think another very good suggestion is by Mr Boulding, maybe you've got a small piece of debris in there, and then simply your bar gets jammed and cannot go in any further.</li> <li>CHAIRMAN: Yes, but the point I'm making is assuming you've got the diaphragm wall and it's all concreted and you've used your hydraulics, and actually it presents a rather difficult situation, some are off at bad angles but a lot of them, shall we say a run of say ten of them,</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15	<ul> <li>because that's the one mentioned about full tolerance, that means the threaded section is longer than design. So you can still maintain the ten threads in the coupler. That's what they mean by full tolerance on the right side of the figure.</li> <li>COMMISSIONER HANSFORD: How do we know that? How do we know that's what they mean?</li> <li>A. Because they say "maximum tolerance". That means both bars get a maximum tolerance and both bars are 48 the threaded section, both bars are 48mm long.</li> <li>CHAIRMAN: Sorry, so you are saying please forgive me the two threads means that you still hit the butt because that's the tolerance?</li> <li>A. Yes. I can give you a simple example on the numbers.</li> <li>CHAIRMAN: No, no, I understand that. All right. I'm just trying to bring it down to a level that I can</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	<ul> <li>CHAIRMAN: So BOSA must then build into their engineering of these things a situation where because maybe the angle is not 100 per cent right, because the thread perhaps is not fully beautifully honed, that you might not get fully in, so you don't have to have butt-to-butt, provided you are close enough that only two threads show; that will be sufficient?</li> <li>A. Or I think another very good suggestion is by Mr Boulding, maybe you've got a small piece of debris in there, and then simply your bar gets jammed and cannot go in any further.</li> <li>CHAIRMAN: Yes, but the point I'm making is assuming you've got the diaphragm wall and it's all concreted and you've used your hydraulics, and actually it presents a rather difficult situation, some are off at bad angles but a lot of them, shall we say a run of say ten of them, are not that badly off but are just a little bit off and</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	<ul> <li>because that's the one mentioned about full tolerance, that means the threaded section is longer than design. So you can still maintain the ten threads in the coupler. That's what they mean by full tolerance on the right side of the figure.</li> <li>COMMISSIONER HANSFORD: How do we know that? How do we know that's what they mean?</li> <li>A. Because they say "maximum tolerance". That means both bars get a maximum tolerance and both bars are 48 the threaded section, both bars are 48mm long.</li> <li>CHAIRMAN: Sorry, so you are saying please forgive me the two threads means that you still hit the butt because that's the tolerance?</li> <li>A. Yes. I can give you a simple example on the numbers.</li> <li>CHAIRMAN: No, no, I understand that. All right. I'm just trying to bring it down to a level that I can understand; okay? Because I'm thinking to myself, "Why</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	<ul> <li>CHAIRMAN: So BOSA must then build into their engineering of these things a situation where because maybe the angle is not 100 per cent right, because the thread perhaps is not fully beautifully honed, that you might not get fully in, so you don't have to have butt-to-butt, provided you are close enough that only two threads show; that will be sufficient?</li> <li>A. Or I think another very good suggestion is by Mr Boulding, maybe you've got a small piece of debris in there, and then simply your bar gets jammed and cannot go in any further.</li> <li>CHAIRMAN: Yes, but the point I'm making is assuming you've got the diaphragm wall and it's all concreted and you've used your hydraulics, and actually it presents a rather difficult situation, some are off at bad angles but a lot of them, shall we say a run of say ten of them, are not that badly off but are just a little bit off and you try to get it in, and each time you get as far as</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	<ul> <li>because that's the one mentioned about full tolerance, that means the threaded section is longer than design. So you can still maintain the ten threads in the coupler. That's what they mean by full tolerance on the right side of the figure.</li> <li>COMMISSIONER HANSFORD: How do we know that? How do we know that's what they mean?</li> <li>A. Because they say "maximum tolerance". That means both bars get a maximum tolerance and both bars are 48 the threaded section, both bars are 48mm long.</li> <li>CHAIRMAN: Sorry, so you are saying please forgive me the two threads means that you still hit the butt because that's the tolerance?</li> <li>A. Yes. I can give you a simple example on the numbers.</li> <li>CHAIRMAN: No, no, I understand that. All right. I'm just trying to bring it down to a level that I can understand; okay? Because I'm thinking to myself, "Why say this, why not say it"; do you see what I mean? To</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	<ul> <li>CHAIRMAN: So BOSA must then build into their engineering of these things a situation where because maybe the angle is not 100 per cent right, because the thread perhaps is not fully beautifully honed, that you might not get fully in, so you don't have to have butt-to-butt, provided you are close enough that only two threads show; that will be sufficient?</li> <li>A. Or I think another very good suggestion is by Mr Boulding, maybe you've got a small piece of debris in there, and then simply your bar gets jammed and cannot go in any further.</li> <li>CHAIRMAN: Yes, but the point I'm making is assuming you've got the diaphragm wall and it's all concreted and you've used your hydraulics, and actually it presents a rather difficult situation, some are off at bad angles but a lot of them, shall we say a run of say ten of them, are not that badly off but are just a little bit off and you try to get it in, and each time you get as far as you can, two screws showing you know?</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	<ul> <li>because that's the one mentioned about full tolerance, that means the threaded section is longer than design. So you can still maintain the ten threads in the coupler. That's what they mean by full tolerance on the right side of the figure.</li> <li>COMMISSIONER HANSFORD: How do we know that? How do we know that's what they mean?</li> <li>A. Because they say "maximum tolerance". That means both bars get a maximum tolerance and both bars are 48 the threaded section, both bars are 48mm long.</li> <li>CHAIRMAN: Sorry, so you are saying please forgive me the two threads means that you still hit the butt because that's the tolerance?</li> <li>A. Yes. I can give you a simple example on the numbers.</li> <li>CHAIRMAN: No, no, I understand that. All right. I'm just trying to bring it down to a level that I can understand; okay? Because I'm thinking to myself, "Why say this, why not say it"; do you see what I mean? To an ordinary worker, "I've come on site, and it doesn't</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	<ul> <li>CHAIRMAN: So BOSA must then build into their engineering of these things a situation where because maybe the angle is not 100 per cent right, because the thread perhaps is not fully beautifully honed, that you might not get fully in, so you don't have to have butt-to-butt, provided you are close enough that only two threads show; that will be sufficient?</li> <li>A. Or I think another very good suggestion is by Mr Boulding, maybe you've got a small piece of debris in there, and then simply your bar gets jammed and cannot go in any further.</li> <li>CHAIRMAN: Yes, but the point I'm making is assuming you've got the diaphragm wall and it's all concreted and you've used your hydraulics, and actually it presents a rather difficult situation, some are off at bad angles but a lot of them, shall we say a run of say ten of them, are not that badly off but are just a little bit off and you try to get it in, and each time you get as far as you can, two screws showing you know? Now, the foreman comes across and says that's okay.</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	<ul> <li>because that's the one mentioned about full tolerance, that means the threaded section is longer than design. So you can still maintain the ten threads in the coupler. That's what they mean by full tolerance on the right side of the figure.</li> <li>COMMISSIONER HANSFORD: How do we know that? How do we know that's what they mean?</li> <li>A. Because they say "maximum tolerance". That means both bars get a maximum tolerance and both bars are 48 the threaded section, both bars are 48mm long.</li> <li>CHAIRMAN: Sorry, so you are saying please forgive me the two threads means that you still hit the butt because that's the tolerance?</li> <li>A. Yes. I can give you a simple example on the numbers.</li> <li>CHAIRMAN: No, no, I understand that. All right. I'm just trying to bring it down to a level that I can understand; okay? Because I'm thinking to myself, "Why say this, why not say it"; do you see what I mean? To an ordinary worker, "Tve come on site, and it doesn't say anything about you've got to do butt-to-butt. It</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	<ul> <li>CHAIRMAN: So BOSA must then build into their engineering of these things a situation where because maybe the angle is not 100 per cent right, because the thread perhaps is not fully beautifully honed, that you might not get fully in, so you don't have to have butt-to-butt, provided you are close enough that only two threads show; that will be sufficient?</li> <li>A. Or I think another very good suggestion is by Mr Boulding, maybe you've got a small piece of debris in there, and then simply your bar gets jammed and cannot go in any further.</li> <li>CHAIRMAN: Yes, but the point I'm making is assuming you've got the diaphragm wall and it's all concreted and you've used your hydraulics, and actually it presents a rather difficult situation, some are off at bad angles but a lot of them, shall we say a run of say ten of them, are not that badly off but are just a little bit off and you try to get it in, and each time you get as far as you can, two screws showing you know? Now, the foreman comes across and says that's okay. You know it's okay because BOSA have told you it's okay,</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	<ul> <li>because that's the one mentioned about full tolerance, that means the threaded section is longer than design. So you can still maintain the ten threads in the coupler. That's what they mean by full tolerance on the right side of the figure.</li> <li>COMMISSIONER HANSFORD: How do we know that? How do we know that's what they mean?</li> <li>A. Because they say "maximum tolerance". That means both bars get a maximum tolerance and both bars are 48 the threaded section, both bars are 48mm long.</li> <li>CHAIRMAN: Sorry, so you are saying please forgive me the two threads means that you still hit the butt because that's the tolerance?</li> <li>A. Yes. I can give you a simple example on the numbers.</li> <li>CHAIRMAN: No, no, I understand that. All right. I'm just trying to bring it down to a level that I can understand; okay? Because I'm thinking to myself, "Why say this, why not say it"; do you see what I mean? To an ordinary worker, "I've come on site, and it doesn't say anything about you've got to do butt-to-butt. It says try to get full engagement, which I understand as</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>CHAIRMAN: So BOSA must then build into their engineering of these things a situation where because maybe the angle is not 100 per cent right, because the thread perhaps is not fully beautifully honed, that you might not get fully in, so you don't have to have butt-to-butt, provided you are close enough that only two threads show; that will be sufficient?</li> <li>A. Or I think another very good suggestion is by Mr Boulding, maybe you've got a small piece of debris in there, and then simply your bar gets jammed and cannot go in any further.</li> <li>CHAIRMAN: Yes, but the point I'm making is assuming you've got the diaphragm wall and it's all concreted and you've used your hydraulics, and actually it presents a rather difficult situation, some are off at bad angles but a lot of them, shall we say a run of say ten of them, are not that badly off but are just a little bit off and you try to get it in, and each time you get as far as you can, two screws showing you know? Now, the foreman comes across and says that's okay. You know it's okay because BOSA have told you it's okay, and you've done that on a run of say six or seven or</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>because that's the one mentioned about full tolerance, that means the threaded section is longer than design. So you can still maintain the ten threads in the coupler. That's what they mean by full tolerance on the right side of the figure.</li> <li>COMMISSIONER HANSFORD: How do we know that? How do we know that's what they mean?</li> <li>A. Because they say "maximum tolerance". That means both bars get a maximum tolerance and both bars are 48 the threaded section, both bars are 48mm long.</li> <li>CHAIRMAN: Sorry, so you are saying please forgive me the two threads means that you still hit the butt because that's the tolerance?</li> <li>A. Yes. I can give you a simple example on the numbers.</li> <li>CHAIRMAN: No, no, I understand that. All right. I'm just trying to bring it down to a level that I can understand; okay? Because I'm thinking to myself, "Why say this, why not say it"; do you see what I mean? To an ordinary worker, "Tve come on site, and it doesn't say anything about you've got to do butt-to-butt. It says try to get full engagement, which I understand as meaning unless you get them lined up, you can't get them</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	<ul> <li>CHAIRMAN: So BOSA must then build into their engineering of these things a situation where because maybe the angle is not 100 per cent right, because the thread perhaps is not fully beautifully honed, that you might not get fully in, so you don't have to have butt-to-butt, provided you are close enough that only two threads show; that will be sufficient?</li> <li>A. Or I think another very good suggestion is by Mr Boulding, maybe you've got a small piece of debris in there, and then simply your bar gets jammed and cannot go in any further.</li> <li>CHAIRMAN: Yes, but the point I'm making is assuming you've got the diaphragm wall and it's all concreted and you've used your hydraulics, and actually it presents a rather difficult situation, some are off at bad angles but a lot of them, shall we say a run of say ten of them, are not that badly off but are just a little bit off and you try to get it in, and each time you get as far as you can, two screws showing you know? Now, the foreman comes across and says that's okay. You know it's okay because BOSA have told you it's okay, and you've done that on a run of say six or seven or even ten of them. None of them are butt-to-butt, but</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	<ul> <li>because that's the one mentioned about full tolerance, that means the threaded section is longer than design. So you can still maintain the ten threads in the coupler. That's what they mean by full tolerance on the right side of the figure.</li> <li>COMMISSIONER HANSFORD: How do we know that? How do we know that's what they mean?</li> <li>A. Because they say "maximum tolerance". That means both bars get a maximum tolerance and both bars are 48 the threaded section, both bars are 48mm long.</li> <li>CHAIRMAN: Sorry, so you are saying please forgive me the two threads means that you still hit the butt because that's the tolerance?</li> <li>A. Yes. I can give you a simple example on the numbers.</li> <li>CHAIRMAN: No, no, I understand that. All right. I'm just trying to bring it down to a level that I can understand; okay? Because I'm thinking to myself, "Why say this, why not say it"; do you see what I mean? To an ordinary worker, "Tve come on site, and it doesn't say anything about you've got to do butt-to-butt. It says try to get full engagement, which I understand as meaning unless you get them lined up, you can't get them screwed in." So line them up, get full engagement, and</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>CHAIRMAN: So BOSA must then build into their engineering of these things a situation where because maybe the angle is not 100 per cent right, because the thread perhaps is not fully beautifully honed, that you might not get fully in, so you don't have to have butt-to-butt, provided you are close enough that only two threads show; that will be sufficient?</li> <li>A. Or I think another very good suggestion is by Mr Boulding, maybe you've got a small piece of debris in there, and then simply your bar gets jammed and cannot go in any further.</li> <li>CHAIRMAN: Yes, but the point I'm making is assuming you've got the diaphragm wall and it's all concreted and you've used your hydraulics, and actually it presents a rather difficult situation, some are off at bad angles but a lot of them, shall we say a run of say ten of them, are not that badly off but are just a little bit off and you try to get it in, and each time you get as far as you can, two screws showing you know? Now, the foreman comes across and says that's okay. You know it's okay because BOSA have told you it's okay, and you've done that on a run of say six or seven or</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>because that's the one mentioned about full tolerance, that means the threaded section is longer than design. So you can still maintain the ten threads in the coupler. That's what they mean by full tolerance on the right side of the figure.</li> <li>COMMISSIONER HANSFORD: How do we know that? How do we know that's what they mean?</li> <li>A. Because they say "maximum tolerance". That means both bars get a maximum tolerance and both bars are 48 the threaded section, both bars are 48mm long.</li> <li>CHAIRMAN: Sorry, so you are saying please forgive me the two threads means that you still hit the butt because that's the tolerance?</li> <li>A. Yes. I can give you a simple example on the numbers.</li> <li>CHAIRMAN: No, no, I understand that. All right. I'm just trying to bring it down to a level that I can understand; okay? Because I'm thinking to myself, "Why say this, why not say it"; do you see what I mean? To an ordinary worker, "Tve come on site, and it doesn't say anything about you've got to do butt-to-butt. It says try to get full engagement, which I understand as meaning unless you get them lined up, you can't get them</li> </ul>

1	Page 37		Page 39
1	is weighing a lot and you've got some guy at the other	1	for you.
2	end holding it up, then get the wrench and you turn the	2	CHAIRMAN: Sorry, Mr Chow. Please continue.
3	wrench until you feel, "Right, I can't go any further",	3	MR CHOW: No problem, sir.
4	you can still see two threads. What you are saying is	4	The first topic I would like to explore with you,
5	that means that in fact, even though you can't see it,	5	again, relates to the butt-to-butt requirement.
6	you are now butt-to-butt or as close such that it	6	A. Okay.
7	doesn't matter if you're not you're within a tiny	7	Q. You recall that yesterday, in your discussion with
8	millimetre of not being butt-to-butt so therefore you	8	Mr Boulding, acting on behalf of MTRC, it was suggested
9	don't have to worry so two threads showing means	9	by Mr Boulding that the requirement for butt-to-butt
10	butt-to-butt?	10	splicing is not part of the contract, and by "contract"
11	A. Let me explain that to you in a simple way.	11	my understanding is the contract between MTRC and
12	CHAIRMAN: No, my question, ordinary I'm wearing my	12	Leighton. Do you recall that?
13	wellies, I've got my hard hat on two threads showing	13	A. Yes.
14	means butt-to-butt?	14	Q. Do you agree that the couplers manufactured by BOSA is
15	A. It's still butt-to-butt.	15	a kind of proprietary product of BOSA?
16	COMMISSIONER HANSFORD: Just as a supplementary to the	16	A. Yes.
17	Chairman's question, Prof Yeung on page 26 of your	17	Q. Meaning that if one used that product, one has to go to
18	witness statement can we go to it, actually?	18	BOSA to purchase it?
19	In the summary under your diagrams, why have you	19	A. That may not be necessary. You may get one of BOSA's
20	underlined why have you got in capitals and	20	distributors, if they have one.
20	underlined "why have you got in capitals and underlined "two full threads"?	20	Q. And it's a product developed by BOSA with the necessary
21	A. The summary is a verbatim copy from BOSA.	21	testing data?
22	COMMISSIONER HANSFORD: So BOSA have underlined and have in		-
23	capitals "two full threads"?	24	<ul><li>A. For them to get approval from the government.</li><li>Q. And the property of BOSA's coupler, the party who knows</li></ul>
24	A. You are perfectly correct.	24 25	the best would be BOSA; am I correct?
25		23	
	Page 38		Page 40
1	COMMISSIONER HANSFORD: Thank you.	1	A. Yes, you are correct.
2	CHAIRMAN: Because, to repeat, "two full threads" means it's	2	Q. And the requirement in relation to installation, to
3	butt-to-butt anyway?	3	ensure that the couplers will perform as designed, the
4	A. The thread get exposed because the threaded section is		
5		4	best party to define how it should be installed should
5	longer than the design value.	4 5	best party to define how it should be installed should be BOSA; do you agree?
6	longer than the design value. CHAIRMAN: That's correct, yes. But then again, please	5 6	<ul><li>best party to define how it should be installed should</li><li>be BOSA; do you agree?</li><li>A. Of course.</li></ul>
6 7	longer than the design value. CHAIRMAN: That's correct, yes. But then again, please forgive me, I've stopped being a worker, first day	5 6 7	<ul><li>best party to define how it should be installed should be BOSA; do you agree?</li><li>A. Of course.</li><li>Q. Just now, Mr Boulding took you to look at a material</li></ul>
6 7 8	longer than the design value. CHAIRMAN: That's correct, yes. But then again, please forgive me, I've stopped being a worker, first day on site, I'm back to being a lawyer, and I can't help	5 6	<ul><li>best party to define how it should be installed should be BOSA; do you agree?</li><li>A. Of course.</li><li>Q. Just now, Mr Boulding took you to look at a material submission</li></ul>
6 7 8 9	longer than the design value. CHAIRMAN: That's correct, yes. But then again, please forgive me, I've stopped being a worker, first day on site, I'm back to being a lawyer, and I can't help but think to myself, the guy who writes the	5 6 7	<ul><li>best party to define how it should be installed should be BOSA; do you agree?</li><li>A. Of course.</li><li>Q. Just now, Mr Boulding took you to look at a material submission</li><li>A. Counsel, I want to go back to one point you mentioned</li></ul>
6 7 8	longer than the design value. CHAIRMAN: That's correct, yes. But then again, please forgive me, I've stopped being a worker, first day on site, I'm back to being a lawyer, and I can't help but think to myself, the guy who writes the instructions, he would say, "There will always be two	5 6 7 8 9 10	<ul><li>best party to define how it should be installed should be BOSA; do you agree?</li><li>A. Of course.</li><li>Q. Just now, Mr Boulding took you to look at a material submission</li><li>A. Counsel, I want to go back to one point you mentioned earlier, whether this installation procedure is in the</li></ul>
6 7 8 9 10 11	longer than the design value. CHAIRMAN: That's correct, yes. But then again, please forgive me, I've stopped being a worker, first day on site, I'm back to being a lawyer, and I can't help but think to myself, the guy who writes the instructions, he would say, "There will always be two threads showing; that's proof that you are now	5 6 7 8 9 10 11	<ul> <li>best party to define how it should be installed should be BOSA; do you agree?</li> <li>A. Of course.</li> <li>Q. Just now, Mr Boulding took you to look at a material submission</li> <li>A. Counsel, I want to go back to one point you mentioned earlier, whether this installation procedure is in the contract. I would say exact specific instruction may</li> </ul>
6 7 8 9 10 11 12	longer than the design value. CHAIRMAN: That's correct, yes. But then again, please forgive me, I've stopped being a worker, first day on site, I'm back to being a lawyer, and I can't help but think to myself, the guy who writes the instructions, he would say, "There will always be two threads showing; that's proof that you are now butt-to-butt"?	5 6 7 8 9 10 11 12	<ul> <li>best party to define how it should be installed should be BOSA; do you agree?</li> <li>A. Of course.</li> <li>Q. Just now, Mr Boulding took you to look at a material submission</li> <li>A. Counsel, I want to go back to one point you mentioned earlier, whether this installation procedure is in the contract. I would say exact specific instruction may not be in the contract, but in the contract there must</li> </ul>
6 7 8 9 10 11	<ul> <li>longer than the design value.</li> <li>CHAIRMAN: That's correct, yes. But then again, please forgive me, I've stopped being a worker, first day on site, I'm back to being a lawyer, and I can't help but think to myself, the guy who writes the instructions, he would say, "There will always be two threads showing; that's proof that you are now butt-to-butt"?</li> <li>A. If the threads are 44mm long, both will go in, you won't</li> </ul>	5 6 7 8 9 10 11	<ul> <li>best party to define how it should be installed should be BOSA; do you agree?</li> <li>A. Of course.</li> <li>Q. Just now, Mr Boulding took you to look at a material submission</li> <li>A. Counsel, I want to go back to one point you mentioned earlier, whether this installation procedure is in the contract. I would say exact specific instruction may not be in the contract, but in the contract there must be something saying you need to follow the instruction</li> </ul>
6 7 8 9 10 11 12 13 14	<ul> <li>longer than the design value.</li> <li>CHAIRMAN: That's correct, yes. But then again, please forgive me, I've stopped being a worker, first day on site, I'm back to being a lawyer, and I can't help but think to myself, the guy who writes the instructions, he would say, "There will always be two threads showing; that's proof that you are now butt-to-butt"?</li> <li>A. If the threads are 44mm long, both will go in, you won't have any threads exposed, because 44 plus 44 is 88. The</li> </ul>	5 6 7 8 9 10 11 12	<ul> <li>best party to define how it should be installed should be BOSA; do you agree?</li> <li>A. Of course.</li> <li>Q. Just now, Mr Boulding took you to look at a material submission</li> <li>A. Counsel, I want to go back to one point you mentioned earlier, whether this installation procedure is in the contract. I would say exact specific instruction may not be in the contract, but in the contract there must be something saying you need to follow the instruction from time to time as the project goes on.</li> </ul>
6 7 8 9 10 11 12 13	<ul> <li>longer than the design value.</li> <li>CHAIRMAN: That's correct, yes. But then again, please forgive me, I've stopped being a worker, first day on site, I'm back to being a lawyer, and I can't help but think to myself, the guy who writes the instructions, he would say, "There will always be two threads showing; that's proof that you are now butt-to-butt"?</li> <li>A. If the threads are 44mm long, both will go in, you won't have any threads exposed, because 44 plus 44 is 88. The reason we got this thread cannot get in is because</li> </ul>	5 6 7 8 9 10 11 12 13	<ul> <li>best party to define how it should be installed should be BOSA; do you agree?</li> <li>A. Of course.</li> <li>Q. Just now, Mr Boulding took you to look at a material submission</li> <li>A. Counsel, I want to go back to one point you mentioned earlier, whether this installation procedure is in the contract. I would say exact specific instruction may not be in the contract, but in the contract there must be something saying you need to follow the instruction from time to time as the project goes on. So indirectly that installation procedure is part of</li> </ul>
6 7 8 9 10 11 12 13 14	<ul> <li>longer than the design value.</li> <li>CHAIRMAN: That's correct, yes. But then again, please forgive me, I've stopped being a worker, first day on site, I'm back to being a lawyer, and I can't help but think to myself, the guy who writes the instructions, he would say, "There will always be two threads showing; that's proof that you are now butt-to-butt"?</li> <li>A. If the threads are 44mm long, both will go in, you won't have any threads exposed, because 44 plus 44 is 88. The reason we got this thread cannot get in is because you've got one section with 48mm long. So once the</li> </ul>	5 6 7 8 9 10 11 12 13 14	<ul> <li>best party to define how it should be installed should be BOSA; do you agree?</li> <li>A. Of course.</li> <li>Q. Just now, Mr Boulding took you to look at a material submission</li> <li>A. Counsel, I want to go back to one point you mentioned earlier, whether this installation procedure is in the contract. I would say exact specific instruction may not be in the contract, but in the contract there must be something saying you need to follow the instruction from time to time as the project goes on. So indirectly that installation procedure is part of the contract, although it may not be explicitly spelt</li> </ul>
6 7 8 9 10 11 12 13 14 15 16 17	<ul> <li>longer than the design value.</li> <li>CHAIRMAN: That's correct, yes. But then again, please forgive me, I've stopped being a worker, first day on site, I'm back to being a lawyer, and I can't help but think to myself, the guy who writes the instructions, he would say, "There will always be two threads showing; that's proof that you are now butt-to-butt"?</li> <li>A. If the threads are 44mm long, both will go in, you won't have any threads exposed, because 44 plus 44 is 88. The reason we got this thread cannot get in is because you've got one section with 48mm long. So once the first one goes in, there's only 40mm left for the</li> </ul>	5 6 7 8 9 10 11 12 13 14 15	<ul> <li>best party to define how it should be installed should be BOSA; do you agree?</li> <li>A. Of course.</li> <li>Q. Just now, Mr Boulding took you to look at a material submission</li> <li>A. Counsel, I want to go back to one point you mentioned earlier, whether this installation procedure is in the contract. I would say exact specific instruction may not be in the contract, but in the contract there must be something saying you need to follow the instruction from time to time as the project goes on. So indirectly that installation procedure is part of the contract, although it may not be explicitly spelt out in the contract.</li> </ul>
6 7 8 9 10 11 12 13 14 15 16 17 18	<ul> <li>longer than the design value.</li> <li>CHAIRMAN: That's correct, yes. But then again, please forgive me, I've stopped being a worker, first day on site, I'm back to being a lawyer, and I can't help but think to myself, the guy who writes the instructions, he would say, "There will always be two threads showing; that's proof that you are now butt-to-butt"?</li> <li>A. If the threads are 44mm long, both will go in, you won't have any threads exposed, because 44 plus 44 is 88. The reason we got this thread cannot get in is because you've got one section with 48mm long. So once the</li> </ul>	5 6 7 8 9 10 11 12 13 14 15 16	<ul> <li>best party to define how it should be installed should be BOSA; do you agree?</li> <li>A. Of course.</li> <li>Q. Just now, Mr Boulding took you to look at a material submission</li> <li>A. Counsel, I want to go back to one point you mentioned earlier, whether this installation procedure is in the contract. I would say exact specific instruction may not be in the contract, but in the contract there must be something saying you need to follow the instruction from time to time as the project goes on.</li> <li>So indirectly that installation procedure is part of the contract, although it may not be explicitly spelt out in the contract.</li> <li>CHAIRMAN: We don't need to argue the matter, but if</li> </ul>
6 7 8 9 10 11 12 13 14 15 16 17	<ul> <li>longer than the design value.</li> <li>CHAIRMAN: That's correct, yes. But then again, please forgive me, I've stopped being a worker, first day on site, I'm back to being a lawyer, and I can't help but think to myself, the guy who writes the instructions, he would say, "There will always be two threads showing; that's proof that you are now butt-to-butt"?</li> <li>A. If the threads are 44mm long, both will go in, you won't have any threads exposed, because 44 plus 44 is 88. The reason we got this thread cannot get in is because you've got one section with 48mm long. So once the first one goes in, there's only 40mm left for the continuation bar, and that's why the two threads gets out.</li> </ul>	5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	<ul> <li>best party to define how it should be installed should be BOSA; do you agree?</li> <li>A. Of course.</li> <li>Q. Just now, Mr Boulding took you to look at a material submission</li> <li>A. Counsel, I want to go back to one point you mentioned earlier, whether this installation procedure is in the contract. I would say exact specific instruction may not be in the contract, but in the contract there must be something saying you need to follow the instruction from time to time as the project goes on.</li> <li>So indirectly that installation procedure is part of the contract, although it may not be explicitly spelt out in the contract.</li> <li>CHAIRMAN: We don't need to argue the matter, but if everything is meant to meet specifications, so you</li> </ul>
6 7 8 9 10 11 12 13 14 15 16 17 18	<ul> <li>longer than the design value.</li> <li>CHAIRMAN: That's correct, yes. But then again, please forgive me, I've stopped being a worker, first day on site, I'm back to being a lawyer, and I can't help but think to myself, the guy who writes the instructions, he would say, "There will always be two threads showing; that's proof that you are now butt-to-butt"?</li> <li>A. If the threads are 44mm long, both will go in, you won't have any threads exposed, because 44 plus 44 is 88. The reason we got this thread cannot get in is because you've got one section with 48mm long. So once the first one goes in, there's only 40mm left for the continuation bar, and that's why the two threads gets</li> </ul>	5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	<ul> <li>best party to define how it should be installed should be BOSA; do you agree?</li> <li>A. Of course.</li> <li>Q. Just now, Mr Boulding took you to look at a material submission</li> <li>A. Counsel, I want to go back to one point you mentioned earlier, whether this installation procedure is in the contract. I would say exact specific instruction may not be in the contract, but in the contract there must be something saying you need to follow the instruction from time to time as the project goes on. So indirectly that installation procedure is part of the contract.</li> <li>CHAIRMAN: We don't need to argue the matter, but if everything is meant to meet specifications, so you assume, if it's going to be that proprietary product it</li> </ul>
6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	<ul> <li>longer than the design value.</li> <li>CHAIRMAN: That's correct, yes. But then again, please forgive me, I've stopped being a worker, first day on site, I'm back to being a lawyer, and I can't help but think to myself, the guy who writes the instructions, he would say, "There will always be two threads showing; that's proof that you are now butt-to-butt"?</li> <li>A. If the threads are 44mm long, both will go in, you won't have any threads exposed, because 44 plus 44 is 88. The reason we got this thread cannot get in is because you've got one section with 48mm long. So once the first one goes in, there's only 40mm left for the continuation bar, and that's why the two threads gets out.</li> </ul>	5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	<ul> <li>best party to define how it should be installed should be BOSA; do you agree?</li> <li>A. Of course.</li> <li>Q. Just now, Mr Boulding took you to look at a material submission</li> <li>A. Counsel, I want to go back to one point you mentioned earlier, whether this installation procedure is in the contract. I would say exact specific instruction may not be in the contract, but in the contract there must be something saying you need to follow the instruction from time to time as the project goes on. So indirectly that installation procedure is part of the contract, although it may not be explicitly spelt out in the contract.</li> <li>CHAIRMAN: We don't need to argue the matter, but if everything is meant to meet specifications, so you assume, if it's going to be that proprietary product it will need specifications, and you assume that it will be</li> </ul>
6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	<ul> <li>longer than the design value.</li> <li>CHAIRMAN: That's correct, yes. But then again, please forgive me, I've stopped being a worker, first day on site, I'm back to being a lawyer, and I can't help but think to myself, the guy who writes the instructions, he would say, "There will always be two threads showing; that's proof that you are now butt-to-butt"?</li> <li>A. If the threads are 44mm long, both will go in, you won't have any threads exposed, because 44 plus 44 is 88. The reason we got this thread cannot get in is because you've got one section with 48mm long. So once the first one goes in, there's only 40mm left for the continuation bar, and that's why the two threads gets out.</li> <li>CHAIRMAN: Okay. Good. Thank you very much. That helps me. Cross-examination by MR CHOW</li> </ul>	5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>best party to define how it should be installed should be BOSA; do you agree?</li> <li>A. Of course.</li> <li>Q. Just now, Mr Boulding took you to look at a material submission</li> <li>A. Counsel, I want to go back to one point you mentioned earlier, whether this installation procedure is in the contract. I would say exact specific instruction may not be in the contract, but in the contract there must be something saying you need to follow the instruction from time to time as the project goes on.</li> <li>So indirectly that installation procedure is part of the contract.</li> <li>CHAIRMAN: We don't need to argue the matter, but if everything is meant to meet specifications, so you assume, if it's going to be that proprietary product it will need specifications, and you assume that it will be properly installed. I don't think you need provided</li> </ul>
6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	<ul> <li>longer than the design value.</li> <li>CHAIRMAN: That's correct, yes. But then again, please forgive me, I've stopped being a worker, first day on site, I'm back to being a lawyer, and I can't help but think to myself, the guy who writes the instructions, he would say, "There will always be two threads showing; that's proof that you are now butt-to-butt"?</li> <li>A. If the threads are 44mm long, both will go in, you won't have any threads exposed, because 44 plus 44 is 88. The reason we got this thread cannot get in is because you've got one section with 48mm long. So once the first one goes in, there's only 40mm left for the continuation bar, and that's why the two threads gets out.</li> <li>CHAIRMAN: Okay. Good. Thank you very much. That helps me. Cross-examination by MR CHOW</li> <li>MR CHOW: Good morning, Prof Yeung.</li> </ul>	5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	<ul> <li>best party to define how it should be installed should be BOSA; do you agree?</li> <li>A. Of course.</li> <li>Q. Just now, Mr Boulding took you to look at a material submission</li> <li>A. Counsel, I want to go back to one point you mentioned earlier, whether this installation procedure is in the contract. I would say exact specific instruction may not be in the contract, but in the contract there must be something saying you need to follow the instruction from time to time as the project goes on.</li> <li>So indirectly that installation procedure is part of the contract.</li> <li>CHAIRMAN: We don't need to argue the matter, but if everything is meant to meet specifications, so you assume, if it's going to be that proprietary product it will need specifications, and you assume that it will be properly installed. I don't think you need provided your and in this case we know that BOSA gave</li> </ul>
6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>longer than the design value.</li> <li>CHAIRMAN: That's correct, yes. But then again, please forgive me, I've stopped being a worker, first day on site, I'm back to being a lawyer, and I can't help but think to myself, the guy who writes the instructions, he would say, "There will always be two threads showing; that's proof that you are now butt-to-butt"?</li> <li>A. If the threads are 44mm long, both will go in, you won't have any threads exposed, because 44 plus 44 is 88. The reason we got this thread cannot get in is because you've got one section with 48mm long. So once the first one goes in, there's only 40mm left for the continuation bar, and that's why the two threads gets out.</li> <li>CHAIRMAN: Okay. Good. Thank you very much. That helps me. Cross-examination by MR CHOW</li> </ul>	5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>best party to define how it should be installed should be BOSA; do you agree?</li> <li>A. Of course.</li> <li>Q. Just now, Mr Boulding took you to look at a material submission</li> <li>A. Counsel, I want to go back to one point you mentioned earlier, whether this installation procedure is in the contract. I would say exact specific instruction may not be in the contract, but in the contract there must be something saying you need to follow the instruction from time to time as the project goes on.</li> <li>So indirectly that installation procedure is part of the contract.</li> <li>CHAIRMAN: We don't need to argue the matter, but if everything is meant to meet specifications, so you assume, if it's going to be that proprietary product it will need specifications, and you assume that it will be properly installed. I don't think you need provided</li> </ul>

	Page 41		Page 43
1	A. Correct. Because sometimes, in some contract,	1	see that reference?
2	something we may not know what product to use, so	2	A. No, I don't.
3	that means then we use the provision in the contract	3	Q. Page 4276.
4	called engineer's instruction.	4	A. 4276, yes.
5	CHAIRMAN: Good. Thank you very much.	5	CHAIRMAN: Sorry, can I get back I'm just slightly behind
6	MR CHOW: Thank you, sir.	6	you paragraph 4:
7	Just now, Mr Boulding took you to look at a material	7	"Once couplers are fully engaged and tightened."
8	submission from MTRC to the Buildings Department. Do	8	And the answer to that was?
9	you recall that?	9	A. That would ensure butt-to-butt.
10	A. Yes.	10	MR CHOW: Butt-to-butt, yes.
11	Q. It seems there is no dispute that the material or the	11	CHAIRMAN: Then why put in "then use a regular wrench to
12	use of BOSA's proprietary product is proposed by MTRC?	12	tighten"? What that means, surely, is once the couplers
13	A. Correct.	13	are fully engaged and you actually move them in a bit,
14	Q. Mr Boulding also took you just now to the quality	14	then what you do is you take your wrench to tighten the
15	supervision plan. Can I trouble you to go to the	15	splice. So the first sentence doesn't say butt-to-butt,
16	supervision plan again, at bundle H9, starting at	16	it just says engage it and screw it in, probably as far
17	page 4263.	17	as is comfortable doing it by hand, and then you use
18	A. Yes.	18	your wrench to tighten; would that be correct?
19	Q. This is a supervision plan, again, submitted by MTRC to	19	A. That's normally what they do, but if
20	the Buildings Department for the Buildings Department's	20	CHAIRMAN: The reading of that instruction.
21	acceptance.	21	COMMISSIONER HANSFORD: And further to that, isn't it the
22	If we then turn over the page and go to page 4265.	22	case that if it was already butt-to-butt, you wouldn't
23	That is the quality supervision plan. At the top of the	23	be able to tighten it with a pipe wrench?
24	page we have Leighton's logo on the left, and on the	24	A. You are correct, but that's one thing you do as a check
25	right we have BOSA's logo as well.	25	on site, because sometimes, as what the Commissioner has
	Page 42		Page 44
1	So do you agree that this is a document, on the face	1	mentioned, they may not be properly aligned, so
2	of it, jointly prepared by Leighton and BOSA?	2	sometimes you need to use a little bit more force.
3	A. I think it's more likely it's Leighton adopt BOSA's	3	COMMISSIONER HANSFORD: Okay. But it doesn't say that
4	document to submit.	4	CHAIRMAN: All right. Continue, sorry.
5	Q. Right.	5	MR CHOW: At the bottom of that page, 4276, there is
6	Can I then ask you to go to page 4276. This is part	6	a reference to a sample inspection record; do you see
7	of the quality supervision plan that we are now looking	7	that?
8	at, and this part talks about the installation procedure	8	A. You mean the sample or just the sentence?
9	or method. Do you see that?	9	Q. The sentence. Under section (v), the phrase within the
10	A. You mean the five points on the top?	10	brackets; do you see that? It refers to a sample
11	Q. That's correct.	11	inspection record sheet.
12	Now, paragraph 4 describes one of the steps. It	12	A. Okay. You mean the last sentence on the whole page?
13	says:	13	Q. Yes. So if you look at the sample inspection sheet on
14	"Once couplers are fully engaged and tightened. Use	14	the next page, 4277 you see there a number of
15	a regular pipe wrench/chain wrench to tighten the	15	columns; do you see that?
16	splice."	16	A. Yes.
17	Do you see that?	17	Q. The first column is just for putting in the bar's
18	A. Yes.	18	reference; do you see that?
19	Q. Just now, according to what you have told the	19	A. Yes.
20	Commissioners earlier, fully engaged, given the	20	Q. The second column is supposed to record one of the
21	dimensions of the thread produced by BOSA, it actually	21	things that you need to check and inspect, right, and
1 ~ ~			this requires the inspector to make sure that the
22	would result in a butt-to-butt splicing condition?	22	
23	A. Correct.	23	coupler is fully screwed and fitted; do you see that?
		23 24	

	Page 45		Page 47
1	to type I, ie the non-ductile couplers; is that right?	1	Q. So this is what BOSA tell us.
2	A. I think so, yes, because the coupler is only 86mm long	2	Then if we can move on, turn over the page, BOSA
3	rather than 88.	3	then go on to say, the first line of the first
4	Q. We have a similar rectangular box at the bottom of the	4	paragraph:
5	page, and the last line inside the box asks for similar	5	" we do not have any test data on correlating
6	requirement:	6	partial thread engagement of coupler to its structural
7	"This is to ensure butt-to-butt connections can	7	performance. We have no intention in conducting such
8	always be achieved"	8	tests as it should serve no useful purpose for our
9	Do you see that?	9	products. Our products are designed for butt-to-butt
10	A. Yes.	10	full thread engagement and that is what we sell."
11	Q. Now, the following page is the page Mr Boulding has	11	Right?
12	taken you to, so we don't need to go to that. So do you	12	A. Right.
12	agree that "fully engage" the threaded bars and "to	12	Q. Then if we can jump to the second paragraph:
13	ensure butt-to-butt connections" actually applies to	14	"Regarding your question on how a partially engaged
15	both non-ductile and ductile couplers?	15	coupler would perform in permanent elongation test,
16	A. Correct.	16	static compression and tension tests and cyclic
17	Q. Then, if I may, I would like you to go to have a look at	17	tension-and-compression tests, it is our opinion as
18	the letter from BOSA dated 7 January 2019. Bundle H26,		explained in paragraph 4 above, that it is unlikely that
19	page 45640, please.	19	such couplers, without being spliced butt-to-butt and
20	A. Yes.	20	are therefore loose, will survive permanent elongation,
21	Q. Prof Yeung, this letter, actually you should be quite	21	and cyclic tension-and-compression tests."
22	familiar with, because you have also referred to this	22	Now, this is what the owner of the proprietary
23	letter	23	products tells us as to the property of his own product.
24	A. Yes.	24	Now, leaving aside whether the butt-to-butt
25	Q in your report. Just now you agreed you actually	25	requirement is part of the contract between Leighton and
	Page 46		Page 48
1	confirmed that the couplers that were being used by	1	MTRC, purely from a technical point of view, for BOSA's
2	Leighton in this project is a proprietary product from	2	couplers to function properly and serve its intended
3	BOSA; correct?	3	purpose of splicing two pieces of rebar together, does
4	A. Correct.	4	it matter whether the butt-to-butt requirement is
5	Q. In this letter, we have BOSA telling us something very	5	clearly set out in somebody else's contract, if someone
6	important, at least it appears to me, which relates to	6	decided to use its own product?
7	the specific property of its own product.	7	CHAIRMAN: Sorry, I have difficulty with that.
8	Can I ask you to go to the bottom paragraph on	8	COMMISSIONER HANSFORD: Yes, I don't understand that.
9	page 1, the first page of the letter, where BOSA said	9	CHAIRMAN: I would say I have difficulty with this letter
10	"we confirm" do you see that, the first line of the	10	too, because with the greatest of respect, this letter
11	bottom paragraph?	11	is written by January 2019, by which stage this whole
12	" we confirm the maximum positive tolerance is	12	thing had blown up.
12	one thread or 4mm. The tolerance is always positive,	13	MR PENNICOTT: Exactly.
13	and we wish to emphasise here that this is an important	14	CHAIRMAN: And anybody worth half an ounce of salt is going
14	feature of our design to ensure butt-to-butt connections	15	to make sure their position is secured as possible in
16	can always be achieved when the rebars are spliced	16	law. So it's a defensive letter in that respect.
17	together inside the coupler."	17	That's not a criticism, it's a statement of common
18	A. Yes.	18	sense. So I have difficulty with the contents of that
19	Q. It goes on to say:	19	letter.
20	"Please refer to the last remark in the table at	20	MR CHOW: Very well, sir. We can attach different weight to
20	appendix A. Please note further if rebars are not	21	any of the documents.
21	spliced butt-to-butt, the coupler assembly will be	22	CHAIRMAN: Yes.
		23	MR CHOW: I just want to ask Prof Yeung, as an expert.
23 24	loose." Do you see that?	23 24	MR CHOW: I just want to ask Prof Yeung, as an expert, whether from a technical point of view, given what the

	Page 49		Page 51
1	property of his its product, what his view is going to	1	A. Yes.
2	be. But of course the views of BOSA are set out in	2	COMMISSIONER HANSFORD: So, just to complete this,
3	a letter which was only issued recently, after all this	3	engagement less than is always shorter than embedment
4	has blown up, is something that the Commission can take	4	length?
5	into consideration.	5	A. Correct.
6	CHAIRMAN: We will obviously do that, should this be put	6	COMMISSIONER HANSFORD: Thank you.
7	before us and argued on that basis.	7	MR PENNICOTT: Sir, the information we are getting on the
8	MR CHOW: My last question on this topic is: if the measured	18	table is headed "Engagement length".
9	engaged length is less than 37mm, in your opinion, is it	9	COMMISSIONER HANSFORD: That's why thank you. I don't
10	still possible that the splicing inside the couplers is	10	know if that's helpful or not.
11	still butt-to-butt?	11	MR PENNICOTT: I'm just telling you, it's a fact.
12	A. Counsel, I think you are referring to the embedment	12	COMMISSIONER HANSFORD: So the table calls it "Engagement
13	length, not the engagement length, because that's not	13	length"?
14	what we measure.	14	MR PENNICOTT: It does, sir.
15	Q. Okay. How about	15	COMMISSIONER HANSFORD: But Prof Yeung would call that
16	A. If the embedment length is less than 37, even though we	16	"embedment length"; is that correct?
17	take into account of the measurement tolerance of 3mm,	17	A. That's why I'm very careful.
18	it won't have a minimum of 40. So there's no way you	18	COMMISSIONER HANSFORD: You're being careful but it appears
19	can guarantee them to be butt-to-butt. Very simple	19	that those providing us with the regular tables are not.
20	mathematics we can look at it is because the coupler	20	So when they say "engagement length" you would say that
21	is 88mm long, if the bar, the parent bar, has a full	21	really means embedment length, and engagement length is
22	tolerance, it will be 48mm long. So that still have	22	something shorter?
23	40mm for it to be butt-to-butt. If what you measure is	23	A. Correct.
24	less than 37, there's no way the threaded length into	24	COMMISSIONER HANSFORD: Thank you.
25	the coupler can reach the value of 40, so that means it	25	A. I can
	Page 50		Page 52
	r ugo 50		rage 52
1	won't be butt-to-butt.	1	COMMISSIONER HANSFORD: No, that's unless you need to
1 2		1 2	-
	won't be butt-to-butt.		COMMISSIONER HANSFORD: No, that's unless you need to
2 3 4	won't be butt-to-butt. COMMISSIONER HANSFORD: Sorry, Prof Yeung, can you just enlighten me, what's the difference between embedment length and engagement length?	2	COMMISSIONER HANSFORD: No, that's unless you need to elaborate, I've understood that.
2 3 4	<ul><li>won't be butt-to-butt.</li><li>COMMISSIONER HANSFORD: Sorry, Prof Yeung, can you just enlighten me, what's the difference between embedment length and engagement length?</li><li>A. Engagement length will be, when you put the thread in,</li></ul>	2 3	COMMISSIONER HANSFORD: No, that's unless you need to elaborate, I've understood that. MR CHOW: Sir, my understanding is so far that people take
2 3 4	won't be butt-to-butt. COMMISSIONER HANSFORD: Sorry, Prof Yeung, can you just enlighten me, what's the difference between embedment length and engagement length?	2 3 4	<ul><li>COMMISSIONER HANSFORD: No, that's unless you need to elaborate, I've understood that.</li><li>MR CHOW: Sir, my understanding is so far that people take the reading from the ultrasonic tests as representing</li></ul>
2 3 4 5	<ul><li>won't be butt-to-butt.</li><li>COMMISSIONER HANSFORD: Sorry, Prof Yeung, can you just enlighten me, what's the difference between embedment length and engagement length?</li><li>A. Engagement length will be, when you put the thread in,</li></ul>	2 3 4 5	<ul><li>COMMISSIONER HANSFORD: No, that's unless you need to elaborate, I've understood that.</li><li>MR CHOW: Sir, my understanding is so far that people take the reading from the ultrasonic tests as representing the engagement length for the purpose of our discussion,</li></ul>
2 3 4 5 6	<ul><li>won't be butt-to-butt.</li><li>COMMISSIONER HANSFORD: Sorry, Prof Yeung, can you just enlighten me, what's the difference between embedment length and engagement length?</li><li>A. Engagement length will be, when you put the thread in, the thread will engage the thread inside the coupler.</li></ul>	2 3 4 5 6	<ul> <li>COMMISSIONER HANSFORD: No, that's unless you need to elaborate, I've understood that.</li> <li>MR CHOW: Sir, my understanding is so far that people take the reading from the ultrasonic tests as representing the engagement length for the purpose of our discussion, but</li> <li>COMMISSIONER HANSFORD: Prof Yeung calls it something slightly different.</li> </ul>
2 3 4 5 6 7	<ul> <li>won't be butt-to-butt.</li> <li>COMMISSIONER HANSFORD: Sorry, Prof Yeung, can you just enlighten me, what's the difference between embedment length and engagement length?</li> <li>A. Engagement length will be, when you put the thread in, the thread will engage the thread inside the coupler. And what we measure now is we can measure the end of the bar, and depending on how many from that measurement, we cannot really deduce we can do some</li> </ul>	2 3 4 5 6 7	<ul> <li>COMMISSIONER HANSFORD: No, that's unless you need to elaborate, I've understood that.</li> <li>MR CHOW: Sir, my understanding is so far that people take the reading from the ultrasonic tests as representing the engagement length for the purpose of our discussion, but</li> <li>COMMISSIONER HANSFORD: Prof Yeung calls it something</li> </ul>
2 3 4 5 6 7 8 9 10	<ul> <li>won't be butt-to-butt.</li> <li>COMMISSIONER HANSFORD: Sorry, Prof Yeung, can you just enlighten me, what's the difference between embedment length and engagement length?</li> <li>A. Engagement length will be, when you put the thread in, the thread will engage the thread inside the coupler. And what we measure now is we can measure the end of the bar, and depending on how many from that measurement, we cannot really deduce we can do some deduction but we cannot guarantee how many threads are</li> </ul>	2 3 4 5 6 7 8 9 10	<ul> <li>COMMISSIONER HANSFORD: No, that's unless you need to elaborate, I've understood that.</li> <li>MR CHOW: Sir, my understanding is so far that people take the reading from the ultrasonic tests as representing the engagement length for the purpose of our discussion, but</li> <li>COMMISSIONER HANSFORD: Prof Yeung calls it something slightly different.</li> </ul>
2 3 4 5 6 7 8 9 10 11	<ul> <li>won't be butt-to-butt.</li> <li>COMMISSIONER HANSFORD: Sorry, Prof Yeung, can you just enlighten me, what's the difference between embedment length and engagement length?</li> <li>A. Engagement length will be, when you put the thread in, the thread will engage the thread inside the coupler. And what we measure now is we can measure the end of the bar, and depending on how many from that measurement, we cannot really deduce we can do some deduction but we cannot guarantee how many threads are actually engaged, because we only measure how long is</li> </ul>	2 3 4 5 6 7 8 9 10 11	<ul> <li>COMMISSIONER HANSFORD: No, that's unless you need to elaborate, I've understood that.</li> <li>MR CHOW: Sir, my understanding is so far that people take the reading from the ultrasonic tests as representing the engagement length for the purpose of our discussion, but</li> <li>COMMISSIONER HANSFORD: Prof Yeung calls it something slightly different.</li> <li>A. That's actually the embedment length.</li> <li>MR CHOW: Thank you. Prof Yeung, I would like to move on to a new topic.</li> </ul>
2 3 4 5 6 7 8 9 10	<ul> <li>won't be butt-to-butt.</li> <li>COMMISSIONER HANSFORD: Sorry, Prof Yeung, can you just enlighten me, what's the difference between embedment length and engagement length?</li> <li>A. Engagement length will be, when you put the thread in, the thread will engage the thread inside the coupler. And what we measure now is we can measure the end of the bar, and depending on how many from that measurement, we cannot really deduce we can do some deduction but we cannot guarantee how many threads are actually engaged, because we only measure how long is the bar into the coupler.</li> </ul>	2 3 4 5 6 7 8 9 10 11 12	<ul> <li>COMMISSIONER HANSFORD: No, that's unless you need to elaborate, I've understood that.</li> <li>MR CHOW: Sir, my understanding is so far that people take the reading from the ultrasonic tests as representing the engagement length for the purpose of our discussion, but</li> <li>COMMISSIONER HANSFORD: Prof Yeung calls it something slightly different.</li> <li>A. That's actually the embedment length.</li> <li>MR CHOW: Thank you. Prof Yeung, I would like to move on to a new topic.</li> <li>A. Okay.</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13	<ul> <li>won't be butt-to-butt.</li> <li>COMMISSIONER HANSFORD: Sorry, Prof Yeung, can you just enlighten me, what's the difference between embedment length and engagement length?</li> <li>A. Engagement length will be, when you put the thread in, the thread will engage the thread inside the coupler. And what we measure now is we can measure the end of the bar, and depending on how many from that measurement, we cannot really deduce we can do some deduction but we cannot guarantee how many threads are actually engaged, because we only measure how long is the bar into the coupler.</li> <li>COMMISSIONER HANSFORD: Sorry, we are receiving almost daily</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 7 13	<ul> <li>COMMISSIONER HANSFORD: No, that's unless you need to elaborate, I've understood that.</li> <li>MR CHOW: Sir, my understanding is so far that people take the reading from the ultrasonic tests as representing the engagement length for the purpose of our discussion, but</li> <li>COMMISSIONER HANSFORD: Prof Yeung calls it something slightly different.</li> <li>A. That's actually the embedment length.</li> <li>MR CHOW: Thank you. Prof Yeung, I would like to move on to a new topic.</li> <li>A. Okay.</li> <li>Q. You recall yesterday Mr Pennicott took you to</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14	<ul> <li>won't be butt-to-butt.</li> <li>COMMISSIONER HANSFORD: Sorry, Prof Yeung, can you just enlighten me, what's the difference between embedment length and engagement length?</li> <li>A. Engagement length will be, when you put the thread in, the thread will engage the thread inside the coupler. And what we measure now is we can measure the end of the bar, and depending on how many from that measurement, we cannot really deduce we can do some deduction but we cannot guarantee how many threads are actually engaged, because we only measure how long is the bar into the coupler.</li> <li>COMMISSIONER HANSFORD: Sorry, we are receiving almost daily reports of the opening-up exercise. Are we being</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 7 13 14	<ul> <li>COMMISSIONER HANSFORD: No, that's unless you need to elaborate, I've understood that.</li> <li>MR CHOW: Sir, my understanding is so far that people take the reading from the ultrasonic tests as representing the engagement length for the purpose of our discussion, but</li> <li>COMMISSIONER HANSFORD: Prof Yeung calls it something slightly different.</li> <li>A. That's actually the embedment length.</li> <li>MR CHOW: Thank you. Prof Yeung, I would like to move on to a new topic.</li> <li>A. Okay.</li> <li>Q. You recall yesterday Mr Pennicott took you to Prof McQuillan's report, paragraph 89. Can I ask you to</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15	<ul> <li>won't be butt-to-butt.</li> <li>COMMISSIONER HANSFORD: Sorry, Prof Yeung, can you just enlighten me, what's the difference between embedment length and engagement length?</li> <li>A. Engagement length will be, when you put the thread in, the thread will engage the thread inside the coupler. And what we measure now is we can measure the end of the bar, and depending on how many from that measurement, we cannot really deduce we can do some deduction but we cannot guarantee how many threads are actually engaged, because we only measure how long is the bar into the coupler.</li> <li>COMMISSIONER HANSFORD: Sorry, we are receiving almost daily reports of the opening-up exercise. Are we being advised I need to check of engagement length or</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 7 13 14 15	<ul> <li>COMMISSIONER HANSFORD: No, that's unless you need to elaborate, I've understood that.</li> <li>MR CHOW: Sir, my understanding is so far that people take the reading from the ultrasonic tests as representing the engagement length for the purpose of our discussion, but</li> <li>COMMISSIONER HANSFORD: Prof Yeung calls it something slightly different.</li> <li>A. That's actually the embedment length.</li> <li>MR CHOW: Thank you. Prof Yeung, I would like to move on to a new topic.</li> <li>A. Okay.</li> <li>Q. You recall yesterday Mr Pennicott took you to Prof McQuillan's report, paragraph 89. Can I ask you to go to the report, and I think it's in tab 1 of the</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14	<ul> <li>won't be butt-to-butt.</li> <li>COMMISSIONER HANSFORD: Sorry, Prof Yeung, can you just enlighten me, what's the difference between embedment length and engagement length?</li> <li>A. Engagement length will be, when you put the thread in, the thread will engage the thread inside the coupler. And what we measure now is we can measure the end of the bar, and depending on how many from that measurement, we cannot really deduce we can do some deduction but we cannot guarantee how many threads are actually engaged, because we only measure how long is the bar into the coupler.</li> <li>COMMISSIONER HANSFORD: Sorry, we are receiving almost daily reports of the opening-up exercise. Are we being advised I need to check of engagement length or embedment length?</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 7 13 14	<ul> <li>COMMISSIONER HANSFORD: No, that's unless you need to elaborate, I've understood that.</li> <li>MR CHOW: Sir, my understanding is so far that people take the reading from the ultrasonic tests as representing the engagement length for the purpose of our discussion, but</li> <li>COMMISSIONER HANSFORD: Prof Yeung calls it something slightly different.</li> <li>A. That's actually the embedment length.</li> <li>MR CHOW: Thank you. Prof Yeung, I would like to move on to a new topic.</li> <li>A. Okay.</li> <li>Q. You recall yesterday Mr Pennicott took you to Prof McQuillan's report, paragraph 89. Can I ask you to go to the report, and I think it's in tab 1 of the bundle, at page 38, paragraph 89.</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	<ul> <li>won't be butt-to-butt.</li> <li>COMMISSIONER HANSFORD: Sorry, Prof Yeung, can you just enlighten me, what's the difference between embedment length and engagement length?</li> <li>A. Engagement length will be, when you put the thread in, the thread will engage the thread inside the coupler. And what we measure now is we can measure the end of the bar, and depending on how many from that measurement, we cannot really deduce we can do some deduction but we cannot guarantee how many threads are actually engaged, because we only measure how long is the bar into the coupler.</li> <li>COMMISSIONER HANSFORD: Sorry, we are receiving almost daily reports of the opening-up exercise. Are we being advised I need to check of engagement length or embedment length?</li> <li>A. We are measuring embedment length, because we can only</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 7 13 14 15 16 17	<ul> <li>COMMISSIONER HANSFORD: No, that's unless you need to elaborate, I've understood that.</li> <li>MR CHOW: Sir, my understanding is so far that people take the reading from the ultrasonic tests as representing the engagement length for the purpose of our discussion, but</li> <li>COMMISSIONER HANSFORD: Prof Yeung calls it something slightly different.</li> <li>A. That's actually the embedment length.</li> <li>MR CHOW: Thank you. Prof Yeung, I would like to move on to a new topic.</li> <li>A. Okay.</li> <li>Q. You recall yesterday Mr Pennicott took you to Prof McQuillan's report, paragraph 89. Can I ask you to go to the report, and I think it's in tab 1 of the bundle, at page 38, paragraph 89.</li> <li>A. Yes.</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	<ul> <li>won't be butt-to-butt.</li> <li>COMMISSIONER HANSFORD: Sorry, Prof Yeung, can you just enlighten me, what's the difference between embedment length and engagement length?</li> <li>A. Engagement length will be, when you put the thread in, the thread will engage the thread inside the coupler. And what we measure now is we can measure the end of the bar, and depending on how many from that measurement, we cannot really deduce we can do some deduction but we cannot guarantee how many threads are actually engaged, because we only measure how long is the bar into the coupler.</li> <li>COMMISSIONER HANSFORD: Sorry, we are receiving almost daily reports of the opening-up exercise. Are we being advised I need to check of engagement length or embedment length?</li> <li>A. We are measuring embedment length, because we can only measure where the end of the bar is.</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 7 13 14 15 16 17 18	<ul> <li>COMMISSIONER HANSFORD: No, that's unless you need to elaborate, I've understood that.</li> <li>MR CHOW: Sir, my understanding is so far that people take the reading from the ultrasonic tests as representing the engagement length for the purpose of our discussion, but</li> <li>COMMISSIONER HANSFORD: Prof Yeung calls it something slightly different.</li> <li>A. That's actually the embedment length.</li> <li>MR CHOW: Thank you. Prof Yeung, I would like to move on to a new topic.</li> <li>A. Okay.</li> <li>Q. You recall yesterday Mr Pennicott took you to Prof McQuillan's report, paragraph 89. Can I ask you to go to the report, and I think it's in tab 1 of the bundle, at page 38, paragraph 89.</li> <li>A. Yes.</li> <li>Q. You have been taken to subparagraph 2; do you recall</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	<ul> <li>won't be butt-to-butt.</li> <li>COMMISSIONER HANSFORD: Sorry, Prof Yeung, can you just enlighten me, what's the difference between embedment length and engagement length?</li> <li>A. Engagement length will be, when you put the thread in, the thread will engage the thread inside the coupler. And what we measure now is we can measure the end of the bar, and depending on how many from that measurement, we cannot really deduce we can do some deduction but we cannot guarantee how many threads are actually engaged, because we only measure how long is the bar into the coupler.</li> <li>COMMISSIONER HANSFORD: Sorry, we are receiving almost daily reports of the opening-up exercise. Are we being advised I need to check of engagement length or embedment length?</li> <li>A. We are measuring embedment length, because we can only measure where the end of the bar is.</li> <li>COMMISSIONER HANSFORD: Right. Okay. Thank you.</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 7 13 14 15 16 17 18 19	<ul> <li>COMMISSIONER HANSFORD: No, that's unless you need to elaborate, I've understood that.</li> <li>MR CHOW: Sir, my understanding is so far that people take the reading from the ultrasonic tests as representing the engagement length for the purpose of our discussion, but</li> <li>COMMISSIONER HANSFORD: Prof Yeung calls it something slightly different.</li> <li>A. That's actually the embedment length.</li> <li>MR CHOW: Thank you. Prof Yeung, I would like to move on to a new topic.</li> <li>A. Okay.</li> <li>Q. You recall yesterday Mr Pennicott took you to Prof McQuillan's report, paragraph 89. Can I ask you to go to the report, and I think it's in tab 1 of the bundle, at page 38, paragraph 89.</li> <li>A. Yes.</li> <li>Q. You have been taken to subparagraph 2; do you recall that? Where Prof McQuillan says:</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	<ul> <li>won't be butt-to-butt.</li> <li>COMMISSIONER HANSFORD: Sorry, Prof Yeung, can you just enlighten me, what's the difference between embedment length and engagement length?</li> <li>A. Engagement length will be, when you put the thread in, the thread will engage the thread inside the coupler. And what we measure now is we can measure the end of the bar, and depending on how many from that measurement, we cannot really deduce we can do some deduction but we cannot guarantee how many threads are actually engaged, because we only measure how long is the bar into the coupler.</li> <li>COMMISSIONER HANSFORD: Sorry, we are receiving almost daily reports of the opening-up exercise. Are we being advised I need to check of engagement length or embedment length?</li> <li>A. We are measuring embedment length, because we can only measure where the end of the bar is.</li> <li>COMMISSIONER HANSFORD: Right. Okay. Thank you.</li> <li>CHAIRMAN: So, in very simple terms again, embedment length</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 7 13 14 15 16 17 18 19 20	<ul> <li>COMMISSIONER HANSFORD: No, that's unless you need to elaborate, I've understood that.</li> <li>MR CHOW: Sir, my understanding is so far that people take the reading from the ultrasonic tests as representing the engagement length for the purpose of our discussion, but</li> <li>COMMISSIONER HANSFORD: Prof Yeung calls it something slightly different.</li> <li>A. That's actually the embedment length.</li> <li>MR CHOW: Thank you. Prof Yeung, I would like to move on to a new topic.</li> <li>A. Okay.</li> <li>Q. You recall yesterday Mr Pennicott took you to Prof McQuillan's report, paragraph 89. Can I ask you to go to the report, and I think it's in tab 1 of the bundle, at page 38, paragraph 89.</li> <li>A. Yes.</li> <li>Q. You have been taken to subparagraph 2; do you recall that? Where Prof McQuillan says: "The geometry of the connection between the EWL slab</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	<ul> <li>won't be butt-to-butt.</li> <li>COMMISSIONER HANSFORD: Sorry, Prof Yeung, can you just enlighten me, what's the difference between embedment length and engagement length?</li> <li>A. Engagement length will be, when you put the thread in, the thread will engage the thread inside the coupler. And what we measure now is we can measure the end of the bar, and depending on how many from that measurement, we cannot really deduce we can do some deduction but we cannot guarantee how many threads are actually engaged, because we only measure how long is the bar into the coupler.</li> <li>COMMISSIONER HANSFORD: Sorry, we are receiving almost daily reports of the opening-up exercise. Are we being advised I need to check of engagement length or embedment length?</li> <li>A. We are measuring embedment length, because we can only measure where the end of the bar is.</li> <li>COMMISSIONER HANSFORD: Right. Okay. Thank you.</li> <li>CHAIRMAN: So, in very simple terms again, embedment length means it's a 10 foot bar, it's now 6 foot, so 4 feet of</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	<ul> <li>COMMISSIONER HANSFORD: No, that's unless you need to elaborate, I've understood that.</li> <li>MR CHOW: Sir, my understanding is so far that people take the reading from the ultrasonic tests as representing the engagement length for the purpose of our discussion, but</li> <li>COMMISSIONER HANSFORD: Prof Yeung calls it something slightly different.</li> <li>A. That's actually the embedment length.</li> <li>MR CHOW: Thank you. Prof Yeung, I would like to move on to a new topic.</li> <li>A. Okay.</li> <li>Q. You recall yesterday Mr Pennicott took you to Prof McQuillan's report, paragraph 89. Can I ask you to go to the report, and I think it's in tab 1 of the bundle, at page 38, paragraph 89.</li> <li>A. Yes.</li> <li>Q. You have been taken to subparagraph 2; do you recall that? Where Prof McQuillan says: "The geometry of the connection between the EWL slab and the east diaphragm wall, however, precludes any</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>won't be butt-to-butt.</li> <li>COMMISSIONER HANSFORD: Sorry, Prof Yeung, can you just enlighten me, what's the difference between embedment length and engagement length?</li> <li>A. Engagement length will be, when you put the thread in, the thread will engage the thread inside the coupler. And what we measure now is we can measure the end of the bar, and depending on how many from that measurement, we cannot really deduce we can do some deduction but we cannot guarantee how many threads are actually engaged, because we only measure how long is the bar into the coupler.</li> <li>COMMISSIONER HANSFORD: Sorry, we are receiving almost daily reports of the opening-up exercise. Are we being advised I need to check of engagement length or embedment length?</li> <li>A. We are measuring embedment length, because we can only measure where the end of the bar is.</li> <li>COMMISSIONER HANSFORD: Right. Okay. Thank you.</li> <li>CHAIRMAN: So, in very simple terms again, embedment length means it's a 10 foot bar, it's now 6 foot, so 4 feet of it's gone into the structure; that's embedment.</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 7 13 14 15 16 17 18 19 20 21 22	<ul> <li>COMMISSIONER HANSFORD: No, that's unless you need to elaborate, I've understood that.</li> <li>MR CHOW: Sir, my understanding is so far that people take the reading from the ultrasonic tests as representing the engagement length for the purpose of our discussion, but</li> <li>COMMISSIONER HANSFORD: Prof Yeung calls it something slightly different.</li> <li>A. That's actually the embedment length.</li> <li>MR CHOW: Thank you. Prof Yeung, I would like to move on to a new topic.</li> <li>A. Okay.</li> <li>Q. You recall yesterday Mr Pennicott took you to Prof McQuillan's report, paragraph 89. Can I ask you to go to the report, and I think it's in tab 1 of the bundle, at page 38, paragraph 89.</li> <li>A. Yes.</li> <li>Q. You have been taken to subparagraph 2; do you recall that? Where Prof McQuillan says: "The geometry of the connection between the EWL slab and the east diaphragm wall, however, precludes any ductility. The structural 'plastic' deformation which</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	<ul> <li>won't be butt-to-butt.</li> <li>COMMISSIONER HANSFORD: Sorry, Prof Yeung, can you just enlighten me, what's the difference between embedment length and engagement length?</li> <li>A. Engagement length will be, when you put the thread in, the thread will engage the thread inside the coupler.</li> <li>And what we measure now is we can measure the end of the bar, and depending on how many from that measurement, we cannot really deduce we can do some deduction but we cannot guarantee how many threads are actually engaged, because we only measure how long is the bar into the coupler.</li> <li>COMMISSIONER HANSFORD: Sorry, we are receiving almost daily reports of the opening-up exercise. Are we being advised I need to check of engagement length or embedment length?</li> <li>A. We are measuring embedment length, because we can only measure where the end of the bar is.</li> <li>COMMISSIONER HANSFORD: Right. Okay. Thank you.</li> <li>CHAIRMAN: So, in very simple terms again, embedment length means it's a 10 foot bar, it's now 6 foot, so 4 feet of it's gone into the structure; that's embedment. Engagement is we've got X number of threads and it</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	<ul> <li>COMMISSIONER HANSFORD: No, that's unless you need to elaborate, I've understood that.</li> <li>MR CHOW: Sir, my understanding is so far that people take the reading from the ultrasonic tests as representing the engagement length for the purpose of our discussion, but</li> <li>COMMISSIONER HANSFORD: Prof Yeung calls it something slightly different.</li> <li>A. That's actually the embedment length.</li> <li>MR CHOW: Thank you. Prof Yeung, I would like to move on to a new topic.</li> <li>A. Okay.</li> <li>Q. You recall yesterday Mr Pennicott took you to Prof McQuillan's report, paragraph 89. Can I ask you to go to the report, and I think it's in tab 1 of the bundle, at page 38, paragraph 89.</li> <li>A. Yes.</li> <li>Q. You have been taken to subparagraph 2; do you recall that? Where Prof McQuillan says:     <ul> <li>"The geometry of the connection between the EWL slab and the east diaphragm wall, however, precludes any ductility. The structural 'plastic' deformation which might occur during seismic activity will develop lower</li> </ul> </li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>won't be butt-to-butt.</li> <li>COMMISSIONER HANSFORD: Sorry, Prof Yeung, can you just enlighten me, what's the difference between embedment length and engagement length?</li> <li>A. Engagement length will be, when you put the thread in, the thread will engage the thread inside the coupler. And what we measure now is we can measure the end of the bar, and depending on how many from that measurement, we cannot really deduce we can do some deduction but we cannot guarantee how many threads are actually engaged, because we only measure how long is the bar into the coupler.</li> <li>COMMISSIONER HANSFORD: Sorry, we are receiving almost daily reports of the opening-up exercise. Are we being advised I need to check of engagement length or embedment length?</li> <li>A. We are measuring embedment length, because we can only measure where the end of the bar is.</li> <li>COMMISSIONER HANSFORD: Right. Okay. Thank you.</li> <li>CHAIRMAN: So, in very simple terms again, embedment length means it's a 10 foot bar, it's now 6 foot, so 4 feet of it's gone into the structure; that's embedment.</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 7 13 14 15 16 17 18 19 20 21 22	<ul> <li>COMMISSIONER HANSFORD: No, that's unless you need to elaborate, I've understood that.</li> <li>MR CHOW: Sir, my understanding is so far that people take the reading from the ultrasonic tests as representing the engagement length for the purpose of our discussion, but</li> <li>COMMISSIONER HANSFORD: Prof Yeung calls it something slightly different.</li> <li>A. That's actually the embedment length.</li> <li>MR CHOW: Thank you. Prof Yeung, I would like to move on to a new topic.</li> <li>A. Okay.</li> <li>Q. You recall yesterday Mr Pennicott took you to Prof McQuillan's report, paragraph 89. Can I ask you to go to the report, and I think it's in tab 1 of the bundle, at page 38, paragraph 89.</li> <li>A. Yes.</li> <li>Q. You have been taken to subparagraph 2; do you recall that? Where Prof McQuillan says: "The geometry of the connection between the EWL slab and the east diaphragm wall, however, precludes any ductility. The structural 'plastic' deformation which</li> </ul>

	Page 53		Page 55
1	A. Yes.	1	Q. All right. I'm not sure that it is the true position.
2	Q. The part I would like you to focus on is the first two	2	Let's see if I can get you to clarify. Can I first ask
3	sentences that I've just read to you.	3	you to take a look at the acceptance letter issued by
4	A. Mm-hmm.	4	the Buildings Department, dated 25 February 2013.
5	Q. My question is this. Well, you have given an answer	5	Bundle H9, page 3908, please.
6	yesterday. Your answer was something like, "It depends,	6	A. Yes.
7	there may be many different loading cases"; that was	7	Q. This is an acceptance letter sorry, I have some
8	your answer. Irrespective of that, do you agree with me	8	problem with my iPad. Just bear with me, please. Like
9	that to be able to form a plastic hinge at the diaphragm	9	Mr Shieh, I cannot rotate the page.
10	wall below, as suggested by Prof McQuillan, there is one	10	This is the first page of the acceptance letter. If
11	very important prerequisite or assumption, the joint,	11	we can then now go to the relevant part, the specific
12	the connection between the EWL slab and the east	12	requirement for ductile couplers, at page 3931, please.
13	diaphragm wall, is strong enough to transfer the	13	You see, under paragraph 5 paragraph 5 is part of
14	loading. If the joint failed, then the plastic hinge	14	the requirement imposed by the Buildings Department. It
15	under the connection may never form. Do you agree or	15	relates to the various tests
16	not?	16	A. Yes.
17	A. When you mentioned the joint failure, what is the	17	Q that the contractor has to perform for the use of
18	failure mechanism of the joint, before I can answer your	18	couplers in the project.
19	question?	19	A. Yes.
20	Q. How about shear failure?	20	Q. Under subparagraph (a), it refers to tests specified
21	A. On the slab?	21	under the American code, AC133; do you see that?
22	Q. No, within the joint.	22	A. I think it's the acceptance criteria.
23	A. I think without a detailed analysis I cannot definitely	23	Q. Yes.
24	answer that question.	24	In subparagraph (c), it refers to a requirement in
25	Q. All right. Thank you.	25	relation to permanent elongation of the splicing
	Page 54		Page 56
1	Do you recall yesterday you mentioned that you are	1	assemblies after loading to 0.6 of the yield strength
2	also of the view that the stresses inside the joint has	2	1 11 / 101 111 / 1 1 111
~		2	should not exceed 0.1 millimetre in accordance with the
3	to be checked?	2 3	requirements stated in clause 3.2.8.2 of the Code of
3 4	to be checked? A. I think I mean the construction joint.		
		3	requirements stated in clause 3.2.8.2 of the Code of
4	<ul><li>A. I think I mean the construction joint.</li><li>Q. Yes, the additional construction joint?</li><li>A. Yes.</li></ul>	3 4	requirements stated in clause 3.2.8.2 of the Code of Practice for Structural Use of Concrete 2004; do you see
4 5	<ul><li>A. I think I mean the construction joint.</li><li>Q. Yes, the additional construction joint?</li><li>A. Yes.</li><li>Q. So, to that extent, you agree with the opinion of</li></ul>	3 4 5	<ul><li>requirements stated in clause 3.2.8.2 of the Code of Practice for Structural Use of Concrete 2004; do you see that?</li><li>A. Yes.</li><li>Q. So that is some requirement in the Concrete Code in</li></ul>
4 5 6	<ul><li>A. I think I mean the construction joint.</li><li>Q. Yes, the additional construction joint?</li><li>A. Yes.</li><li>Q. So, to that extent, you agree with the opinion of Prof Francis Au; right?</li></ul>	3 4 5 6	<ul><li>requirements stated in clause 3.2.8.2 of the Code of Practice for Structural Use of Concrete 2004; do you see that?</li><li>A. Yes.</li><li>Q. So that is some requirement in the Concrete Code in relation to maximum elongation after certain level of</li></ul>
4 5 6 7	<ul> <li>A. I think I mean the construction joint.</li> <li>Q. Yes, the additional construction joint?</li> <li>A. Yes.</li> <li>Q. So, to that extent, you agree with the opinion of Prof Francis Au; right?</li> <li>A. Yes. But we are not saying it is not adequate. I think</li> </ul>	3 4 5 6 7	<ul><li>requirements stated in clause 3.2.8.2 of the Code of Practice for Structural Use of Concrete 2004; do you see that?</li><li>A. Yes.</li><li>Q. So that is some requirement in the Concrete Code in relation to maximum elongation after certain level of loading is applied?</li></ul>
4 5 6 7 8	<ul> <li>A. I think I mean the construction joint.</li> <li>Q. Yes, the additional construction joint?</li> <li>A. Yes.</li> <li>Q. So, to that extent, you agree with the opinion of Prof Francis Au; right?</li> <li>A. Yes. But we are not saying it is not adequate. I think we need to check it to make sure it's adequate. Without</li> </ul>	3 4 5 6 7 8	<ul><li>requirements stated in clause 3.2.8.2 of the Code of Practice for Structural Use of Concrete 2004; do you see that?</li><li>A. Yes.</li><li>Q. So that is some requirement in the Concrete Code in relation to maximum elongation after certain level of loading is applied?</li><li>A. Yes.</li></ul>
4 5 6 7 8 9 10 11	<ul> <li>A. I think I mean the construction joint.</li> <li>Q. Yes, the additional construction joint?</li> <li>A. Yes.</li> <li>Q. So, to that extent, you agree with the opinion of Prof Francis Au; right?</li> <li>A. Yes. But we are not saying it is not adequate. I think we need to check it to make sure it's adequate. Without the analysis at this point in time, we cannot say the</li> </ul>	3 4 5 6 7 8 9	<ul><li>requirements stated in clause 3.2.8.2 of the Code of Practice for Structural Use of Concrete 2004; do you see that?</li><li>A. Yes.</li><li>Q. So that is some requirement in the Concrete Code in relation to maximum elongation after certain level of loading is applied?</li><li>A. Yes.</li><li>Q. There is also reference to AC133, which you have also</li></ul>
4 5 7 8 9 10 11 12	<ul> <li>A. I think I mean the construction joint.</li> <li>Q. Yes, the additional construction joint?</li> <li>A. Yes.</li> <li>Q. So, to that extent, you agree with the opinion of Prof Francis Au; right?</li> <li>A. Yes. But we are not saying it is not adequate. I think we need to check it to make sure it's adequate. Without the analysis at this point in time, we cannot say the joint is not structurally adequate. We won't make that</li> </ul>	3 4 5 6 7 8 9 10 11 12	<ul> <li>requirements stated in clause 3.2.8.2 of the Code of Practice for Structural Use of Concrete 2004; do you see that?</li> <li>A. Yes.</li> <li>Q. So that is some requirement in the Concrete Code in relation to maximum elongation after certain level of loading is applied?</li> <li>A. Yes.</li> <li>Q. There is also reference to AC133, which you have also attached to your report. Can I ask you to go to</li> </ul>
4 5 6 7 8 9 10 11 12 13	<ul> <li>A. I think I mean the construction joint.</li> <li>Q. Yes, the additional construction joint?</li> <li>A. Yes.</li> <li>Q. So, to that extent, you agree with the opinion of Prof Francis Au; right?</li> <li>A. Yes. But we are not saying it is not adequate. I think we need to check it to make sure it's adequate. Without the analysis at this point in time, we cannot say the joint is not structurally adequate. We won't make that opinion for the time being.</li> </ul>	3 4 5 6 7 8 9 10 11 12 13	<ul> <li>requirements stated in clause 3.2.8.2 of the Code of Practice for Structural Use of Concrete 2004; do you see that?</li> <li>A. Yes.</li> <li>Q. So that is some requirement in the Concrete Code in relation to maximum elongation after certain level of loading is applied?</li> <li>A. Yes.</li> <li>Q. There is also reference to AC133, which you have also attached to your report. Can I ask you to go to appendix II of your report, please. Appendix II of the</li> </ul>
4 5 7 8 9 10 11 12 13 14	<ul> <li>A. I think I mean the construction joint.</li> <li>Q. Yes, the additional construction joint?</li> <li>A. Yes.</li> <li>Q. So, to that extent, you agree with the opinion of Prof Francis Au; right?</li> <li>A. Yes. But we are not saying it is not adequate. I think we need to check it to make sure it's adequate. Without the analysis at this point in time, we cannot say the joint is not structurally adequate. We won't make that opinion for the time being.</li> <li>Q. Yes. This is also the position taken by Prof Au as</li> </ul>	3 4 5 6 7 8 9 10 11 12 13 14	<ul> <li>requirements stated in clause 3.2.8.2 of the Code of Practice for Structural Use of Concrete 2004; do you see that?</li> <li>A. Yes.</li> <li>Q. So that is some requirement in the Concrete Code in relation to maximum elongation after certain level of loading is applied?</li> <li>A. Yes.</li> <li>Q. There is also reference to AC133, which you have also attached to your report. Can I ask you to go to appendix II of your report, please. Appendix II of the bundle ER1, tab 8.</li> </ul>
4 5 6 7 8 9 10 11 12 13 14 15	<ul> <li>A. I think I mean the construction joint.</li> <li>Q. Yes, the additional construction joint?</li> <li>A. Yes.</li> <li>Q. So, to that extent, you agree with the opinion of Prof Francis Au; right?</li> <li>A. Yes. But we are not saying it is not adequate. I think we need to check it to make sure it's adequate. Without the analysis at this point in time, we cannot say the joint is not structurally adequate. We won't make that opinion for the time being.</li> <li>Q. Yes. This is also the position taken by Prof Au as well.</li> </ul>	3 4 5 6 7 8 9 10 11 12 13 14 15	<ul> <li>requirements stated in clause 3.2.8.2 of the Code of Practice for Structural Use of Concrete 2004; do you see that?</li> <li>A. Yes.</li> <li>Q. So that is some requirement in the Concrete Code in relation to maximum elongation after certain level of loading is applied?</li> <li>A. Yes.</li> <li>Q. There is also reference to AC133, which you have also attached to your report. Can I ask you to go to appendix II of your report, please. Appendix II of the bundle ER1, tab 8.</li> <li>A. Yes.</li> </ul>
4 5 6 7 8 9 10 11 12 13 14 15 16	<ul> <li>A. I think I mean the construction joint.</li> <li>Q. Yes, the additional construction joint?</li> <li>A. Yes.</li> <li>Q. So, to that extent, you agree with the opinion of Prof Francis Au; right?</li> <li>A. Yes. But we are not saying it is not adequate. I think we need to check it to make sure it's adequate. Without the analysis at this point in time, we cannot say the joint is not structurally adequate. We won't make that opinion for the time being.</li> <li>Q. Yes. This is also the position taken by Prof Au as well.</li> <li>If I may move on to another topic, about the</li> </ul>	3 4 5 6 7 8 9 10 11 12 13 14 15 16	<ul> <li>requirements stated in clause 3.2.8.2 of the Code of Practice for Structural Use of Concrete 2004; do you see that?</li> <li>A. Yes.</li> <li>Q. So that is some requirement in the Concrete Code in relation to maximum elongation after certain level of loading is applied?</li> <li>A. Yes.</li> <li>Q. There is also reference to AC133, which you have also attached to your report. Can I ask you to go to appendix II of your report, please. Appendix II of the bundle ER1, tab 8.</li> <li>A. Yes.</li> <li>Q. If you go to page 3, can you confirm that the</li> </ul>
4 5 6 7 8 9 10 11 12 13 14 15 16 17	<ul> <li>A. I think I mean the construction joint.</li> <li>Q. Yes, the additional construction joint?</li> <li>A. Yes.</li> <li>Q. So, to that extent, you agree with the opinion of Prof Francis Au; right?</li> <li>A. Yes. But we are not saying it is not adequate. I think we need to check it to make sure it's adequate. Without the analysis at this point in time, we cannot say the joint is not structurally adequate. We won't make that opinion for the time being.</li> <li>Q. Yes. This is also the position taken by Prof Au as well.</li> <li>If I may move on to another topic, about the question of whether there is requirement in relation to</li> </ul>	3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	<ul> <li>requirements stated in clause 3.2.8.2 of the Code of Practice for Structural Use of Concrete 2004; do you see that?</li> <li>A. Yes.</li> <li>Q. So that is some requirement in the Concrete Code in relation to maximum elongation after certain level of loading is applied?</li> <li>A. Yes.</li> <li>Q. There is also reference to AC133, which you have also attached to your report. Can I ask you to go to appendix II of your report, please. Appendix II of the bundle ER1, tab 8.</li> <li>A. Yes.</li> <li>Q. If you go to page 3, can you confirm that the section 4.1.2 contains requirement for various tests to</li> </ul>
4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	<ul> <li>A. I think I mean the construction joint.</li> <li>Q. Yes, the additional construction joint?</li> <li>A. Yes.</li> <li>Q. So, to that extent, you agree with the opinion of Prof Francis Au; right?</li> <li>A. Yes. But we are not saying it is not adequate. I think we need to check it to make sure it's adequate. Without the analysis at this point in time, we cannot say the joint is not structurally adequate. We won't make that opinion for the time being.</li> <li>Q. Yes. This is also the position taken by Prof Au as well.</li> <li>If I may move on to another topic, about the question of whether there is requirement in relation to the use of couplers in the 2004 Concrete Code. Do you</li> </ul>	3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	<ul> <li>requirements stated in clause 3.2.8.2 of the Code of Practice for Structural Use of Concrete 2004; do you see that?</li> <li>A. Yes.</li> <li>Q. So that is some requirement in the Concrete Code in relation to maximum elongation after certain level of loading is applied?</li> <li>A. Yes.</li> <li>Q. There is also reference to AC133, which you have also attached to your report. Can I ask you to go to appendix II of your report, please. Appendix II of the bundle ER1, tab 8.</li> <li>A. Yes.</li> <li>Q. If you go to page 3, can you confirm that the section 4.1.2 contains requirement for various tests to be performed on ductile couplers?</li> </ul>
4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	<ul> <li>A. I think I mean the construction joint.</li> <li>Q. Yes, the additional construction joint?</li> <li>A. Yes.</li> <li>Q. So, to that extent, you agree with the opinion of Prof Francis Au; right?</li> <li>A. Yes. But we are not saying it is not adequate. I think we need to check it to make sure it's adequate. Without the analysis at this point in time, we cannot say the joint is not structurally adequate. We won't make that opinion for the time being.</li> <li>Q. Yes. This is also the position taken by Prof Au as well.</li> <li>If I may move on to another topic, about the question of whether there is requirement in relation to the use of couplers in the 2004 Concrete Code. Do you recall that?</li> </ul>	3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	<ul> <li>requirements stated in clause 3.2.8.2 of the Code of Practice for Structural Use of Concrete 2004; do you see that?</li> <li>A. Yes.</li> <li>Q. So that is some requirement in the Concrete Code in relation to maximum elongation after certain level of loading is applied?</li> <li>A. Yes.</li> <li>Q. There is also reference to AC133, which you have also attached to your report. Can I ask you to go to appendix II of your report, please. Appendix II of the bundle ER1, tab 8.</li> <li>A. Yes.</li> <li>Q. If you go to page 3, can you confirm that the section 4.1.2 contains requirement for various tests to be performed on ductile couplers?</li> <li>A. Correct.</li> </ul>
4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	<ul> <li>A. I think I mean the construction joint.</li> <li>Q. Yes, the additional construction joint?</li> <li>A. Yes.</li> <li>Q. So, to that extent, you agree with the opinion of Prof Francis Au; right?</li> <li>A. Yes. But we are not saying it is not adequate. I think we need to check it to make sure it's adequate. Without the analysis at this point in time, we cannot say the joint is not structurally adequate. We won't make that opinion for the time being.</li> <li>Q. Yes. This is also the position taken by Prof Au as well.</li> <li>If I may move on to another topic, about the question of whether there is requirement in relation to the use of couplers in the 2004 Concrete Code. Do you recall that?</li> <li>A. Yes.</li> </ul>	3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	<ul> <li>requirements stated in clause 3.2.8.2 of the Code of Practice for Structural Use of Concrete 2004; do you see that?</li> <li>A. Yes.</li> <li>Q. So that is some requirement in the Concrete Code in relation to maximum elongation after certain level of loading is applied?</li> <li>A. Yes.</li> <li>Q. There is also reference to AC133, which you have also attached to your report. Can I ask you to go to appendix II of your report, please. Appendix II of the bundle ER1, tab 8.</li> <li>A. Yes.</li> <li>Q. If you go to page 3, can you confirm that the section 4.1.2 contains requirement for various tests to be performed on ductile couplers?</li> <li>A. Correct.</li> <li>Q. And also, if we go back to section 4.1.1, which refers</li> </ul>
4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	<ul> <li>A. I think I mean the construction joint.</li> <li>Q. Yes, the additional construction joint?</li> <li>A. Yes.</li> <li>Q. So, to that extent, you agree with the opinion of Prof Francis Au; right?</li> <li>A. Yes. But we are not saying it is not adequate. I think we need to check it to make sure it's adequate. Without the analysis at this point in time, we cannot say the joint is not structurally adequate. We won't make that opinion for the time being.</li> <li>Q. Yes. This is also the position taken by Prof Au as well. If I may move on to another topic, about the question of whether there is requirement in relation to the use of couplers in the 2004 Concrete Code. Do you recall that? A. Yes. Q. At one point, you seemed to agree with Mr Pennicott that</li></ul>	3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	<ul> <li>requirements stated in clause 3.2.8.2 of the Code of Practice for Structural Use of Concrete 2004; do you see that?</li> <li>A. Yes.</li> <li>Q. So that is some requirement in the Concrete Code in relation to maximum elongation after certain level of loading is applied?</li> <li>A. Yes.</li> <li>Q. There is also reference to AC133, which you have also attached to your report. Can I ask you to go to appendix II of your report, please. Appendix II of the bundle ER1, tab 8.</li> <li>A. Yes.</li> <li>Q. If you go to page 3, can you confirm that the section 4.1.2 contains requirement for various tests to be performed on ductile couplers?</li> <li>A. Correct.</li> <li>Q. And also, if we go back to section 4.1.1, which refers to "Type 1 splice", am I right to say that "type 1</li> </ul>
4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>A. I think I mean the construction joint.</li> <li>Q. Yes, the additional construction joint?</li> <li>A. Yes.</li> <li>Q. So, to that extent, you agree with the opinion of Prof Francis Au; right?</li> <li>A. Yes. But we are not saying it is not adequate. I think we need to check it to make sure it's adequate. Without the analysis at this point in time, we cannot say the joint is not structurally adequate. We won't make that opinion for the time being.</li> <li>Q. Yes. This is also the position taken by Prof Au as well. <ul> <li>If I may move on to another topic, about the question of whether there is requirement in relation to the use of couplers in the 2004 Concrete Code. Do you recall that?</li> <li>A. Yes.</li> </ul> </li> </ul>	3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>requirements stated in clause 3.2.8.2 of the Code of Practice for Structural Use of Concrete 2004; do you see that?</li> <li>A. Yes.</li> <li>Q. So that is some requirement in the Concrete Code in relation to maximum elongation after certain level of loading is applied?</li> <li>A. Yes.</li> <li>Q. There is also reference to AC133, which you have also attached to your report. Can I ask you to go to appendix II of your report, please. Appendix II of the bundle ER1, tab 8.</li> <li>A. Yes.</li> <li>Q. If you go to page 3, can you confirm that the section 4.1.2 contains requirement for various tests to be performed on ductile couplers?</li> <li>A. Correct.</li> <li>Q. And also, if we go back to section 4.1.1, which refers to "Type 1 splice", am I right to say that "type 1 splice" referring to this American code, actually refers</li> </ul>
4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	<ul> <li>A. I think I mean the construction joint.</li> <li>Q. Yes, the additional construction joint?</li> <li>A. Yes.</li> <li>Q. So, to that extent, you agree with the opinion of Prof Francis Au; right?</li> <li>A. Yes. But we are not saying it is not adequate. I think we need to check it to make sure it's adequate. Without the analysis at this point in time, we cannot say the joint is not structurally adequate. We won't make that opinion for the time being.</li> <li>Q. Yes. This is also the position taken by Prof Au as well.</li> <li>If I may move on to another topic, about the question of whether there is requirement in relation to the use of couplers in the 2004 Concrete Code. Do you recall that?</li> <li>A. Yes.</li> <li>Q. At one point, you seemed to agree with Mr Pennicott that there was no requirement in relation to couplers in the Concrete Code 2004. Do you recall that?</li> </ul>	3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	<ul> <li>requirements stated in clause 3.2.8.2 of the Code of Practice for Structural Use of Concrete 2004; do you see that?</li> <li>A. Yes.</li> <li>Q. So that is some requirement in the Concrete Code in relation to maximum elongation after certain level of loading is applied?</li> <li>A. Yes.</li> <li>Q. There is also reference to AC133, which you have also attached to your report. Can I ask you to go to appendix II of your report, please. Appendix II of the bundle ER1, tab 8.</li> <li>A. Yes.</li> <li>Q. If you go to page 3, can you confirm that the section 4.1.2 contains requirement for various tests to be performed on ductile couplers?</li> <li>A. Correct.</li> <li>Q. And also, if we go back to section 4.1.1, which refers to "Type 1 splice", am I right to say that "type 1 splice" referring to this American code, actually refers to non-ductile couplers?</li> </ul>
4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>A. I think I mean the construction joint.</li> <li>Q. Yes, the additional construction joint?</li> <li>A. Yes.</li> <li>Q. So, to that extent, you agree with the opinion of Prof Francis Au; right?</li> <li>A. Yes. But we are not saying it is not adequate. I think we need to check it to make sure it's adequate. Without the analysis at this point in time, we cannot say the joint is not structurally adequate. We won't make that opinion for the time being.</li> <li>Q. Yes. This is also the position taken by Prof Au as well. <ul> <li>If I may move on to another topic, about the question of whether there is requirement in relation to the use of couplers in the 2004 Concrete Code. Do you recall that?</li> <li>A. Yes.</li> </ul> </li> </ul>	3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>requirements stated in clause 3.2.8.2 of the Code of Practice for Structural Use of Concrete 2004; do you see that?</li> <li>A. Yes.</li> <li>Q. So that is some requirement in the Concrete Code in relation to maximum elongation after certain level of loading is applied?</li> <li>A. Yes.</li> <li>Q. There is also reference to AC133, which you have also attached to your report. Can I ask you to go to appendix II of your report, please. Appendix II of the bundle ER1, tab 8.</li> <li>A. Yes.</li> <li>Q. If you go to page 3, can you confirm that the section 4.1.2 contains requirement for various tests to be performed on ductile couplers?</li> <li>A. Correct.</li> <li>Q. And also, if we go back to section 4.1.1, which refers to "Type 1 splice", am I right to say that "type 1 splice" referring to this American code, actually refers</li> </ul>

	Page 57		Page 59
1	A. Actually, they match the type I and type II of BOSA.	1	permanent elongation also applies to non-ductile
2	Q. I see. So you mean "type 1 splice" referred to in	2	couplers.
3	AC133, under section 4.1.1, corresponds to the	3	A. Correct.
4	non-ductile	4	Q. So am I right in saying that irrespective of whether it
5	A. The type I of BOSA.	5	is a ductile or non-ductile coupler, one has to comply
6	Q. The type I of BOSA, and "type 2 splice" referred to in	6	with the requirement as to the permanent elongation of,
7	paragraph 4.1.2 corresponds to type II ductile couplers	7	you know, the maximum 0.1 millimetre after a loading of
8	of BOSA?	8	up to 0.6 yield strength?
9	A. Correct.	9	A. Correct.
10	Q. So we can see there are requirements for various tests	10	Q. And as far as you know, BOSA has not performed
11	to be conducted for both ductile and non-ductile	11	elongation tests to any of the partially engaged
12	couplers to be used?	12	couplers?
13	A. Correct.	13	A. You mean the tests they conducted specifically for this
14	Q. Do you want me to refer you to the relevant section of	14	Commission?
15	the 2004 Concrete Code, just so make sure there are	15	Q. No.
16	requirements for testing?	16	A. No, they didn't.
17	A. It would be good to look at it, yes.	17	MR CHOW: Sir, I think it's a convenient moment to have the
18	Q. Sure. Can I take you to bundle H8, page 2852. This is	18	morning break. I have just one more topic to go
19	the Code of Practice 2004. Clause 3.2.8.2, regarding	19	through. It will take maybe another five minutes.
20	"Bars in tension":	20	CHAIRMAN: Then I think finishing your examination would be
21	"The only acceptable full strength butt joint	21	good. Thank you.
22	between bars in tension is formed using a mechanical	22	MR CHOW: Prof Yeung, the last topic I would like to explore
23	coupler satisfying the following criteria".	23	with you
24	If you can turn over the page, the first bullet	24	CHAIRMAN: Sorry, just before we move on, the question and
25	point:	25	the answer that was just exchanged, it suggests that
	Page 58		Daga 60
1	I uge b o		Page 60
1	-	1	
1 2	" when a representative gauge length assembly	1 2	BOSA were not requested to do this or that BOSA failed
2	" when a representative gauge length assembly comprising reinforcement of the diameter, grade and	2	BOSA were not requested to do this or that BOSA failed to do it. There's quite a difference, because BOSA is
2 3	" when a representative gauge length assembly comprising reinforcement of the diameter, grade and profile to be used, and a coupler of the precise type to	2 3	BOSA were not requested to do this or that BOSA failed to do it. There's quite a difference, because BOSA is not a party, and that would be a criticism of BOSA if we
2 3 4	" when a representative gauge length assembly comprising reinforcement of the diameter, grade and profile to be used, and a coupler of the precise type to be used, is tested in tension the permanent elongation	2 3 4	BOSA were not requested to do this or that BOSA failed to do it. There's quite a difference, because BOSA is not a party, and that would be a criticism of BOSA if we use the suggestion "failed". But if they were not asked
2 3 4 5	" when a representative gauge length assembly comprising reinforcement of the diameter, grade and profile to be used, and a coupler of the precise type to be used, is tested in tension the permanent elongation after loading to 0.6 [yield strength] should not exceed	2 3 4 5	BOSA were not requested to do this or that BOSA failed to do it. There's quite a difference, because BOSA is not a party, and that would be a criticism of BOSA if we use the suggestion "failed". But if they were not asked to do it by way of later testing, that's a different
2 3 4 5 6	" when a representative gauge length assembly comprising reinforcement of the diameter, grade and profile to be used, and a coupler of the precise type to be used, is tested in tension the permanent elongation after loading to 0.6 [yield strength] should not exceed 0.1 millimetre; and	2 3 4	BOSA were not requested to do this or that BOSA failed to do it. There's quite a difference, because BOSA is not a party, and that would be a criticism of BOSA if we use the suggestion "failed". But if they were not asked to do it by way of later testing, that's a different matter.
2 3 4 5 6 7	" when a representative gauge length assembly comprising reinforcement of the diameter, grade and profile to be used, and a coupler of the precise type to be used, is tested in tension the permanent elongation after loading to 0.6 [yield strength] should not exceed 0.1 millimetre; and the coupled bar assembly tensile strength	2 3 4 5 6 7	<ul><li>BOSA were not requested to do this or that BOSA failed to do it. There's quite a difference, because BOSA is not a party, and that would be a criticism of BOSA if we use the suggestion "failed". But if they were not asked to do it by way of later testing, that's a different matter.</li><li>MR CHOW: Sir, the last line of questions that I asked</li></ul>
2 3 4 5 6 7 8	" when a representative gauge length assembly comprising reinforcement of the diameter, grade and profile to be used, and a coupler of the precise type to be used, is tested in tension the permanent elongation after loading to 0.6 [yield strength] should not exceed 0.1 millimetre; and the coupled bar assembly tensile strength should exceed 287.5 newtons per millimetre squared for	2 3 4 5 6	<ul><li>BOSA were not requested to do this or that BOSA failed to do it. There's quite a difference, because BOSA is not a party, and that would be a criticism of BOSA if we use the suggestion "failed". But if they were not asked to do it by way of later testing, that's a different matter.</li><li>MR CHOW: Sir, the last line of questions that I asked actually related to the test carried out by BOSA to the</li></ul>
2 3 4 5 6 7	" when a representative gauge length assembly comprising reinforcement of the diameter, grade and profile to be used, and a coupler of the precise type to be used, is tested in tension the permanent elongation after loading to 0.6 [yield strength] should not exceed 0.1 millimetre; and the coupled bar assembly tensile strength	2 3 4 5 6 7 8	<ul><li>BOSA were not requested to do this or that BOSA failed to do it. There's quite a difference, because BOSA is not a party, and that would be a criticism of BOSA if we use the suggestion "failed". But if they were not asked to do it by way of later testing, that's a different matter.</li><li>MR CHOW: Sir, the last line of questions that I asked</li></ul>
2 3 4 5 6 7 8 9	" when a representative gauge length assembly comprising reinforcement of the diameter, grade and profile to be used, and a coupler of the precise type to be used, is tested in tension the permanent elongation after loading to 0.6 [yield strength] should not exceed 0.1 millimetre; and the coupled bar assembly tensile strength should exceed 287.5 newtons per millimetre squared for grade 250, and 483 newtons per millimetre squared for	2 3 4 5 6 7 8 9	<ul><li>BOSA were not requested to do this or that BOSA failed to do it. There's quite a difference, because BOSA is not a party, and that would be a criticism of BOSA if we use the suggestion "failed". But if they were not asked to do it by way of later testing, that's a different matter.</li><li>MR CHOW: Sir, the last line of questions that I asked actually related to the test carried out by BOSA to the partially engaged couplers for the purpose of the</li></ul>
2 3 4 5 6 7 8 9 10	" when a representative gauge length assembly comprising reinforcement of the diameter, grade and profile to be used, and a coupler of the precise type to be used, is tested in tension the permanent elongation after loading to 0.6 [yield strength] should not exceed 0.1 millimetre; and the coupled bar assembly tensile strength should exceed 287.5 newtons per millimetre squared for grade 250, and 483 newtons per millimetre squared for grade 460."	2 3 4 5 6 7 8 9 10	<ul> <li>BOSA were not requested to do this or that BOSA failed to do it. There's quite a difference, because BOSA is not a party, and that would be a criticism of BOSA if we use the suggestion "failed". But if they were not asked to do it by way of later testing, that's a different matter.</li> <li>MR CHOW: Sir, the last line of questions that I asked actually related to the test carried out by BOSA to the partially engaged couplers for the purpose of the Commission, in relation to which my instruction is that</li> </ul>
2 3 4 5 6 7 8 9 10 11	" when a representative gauge length assembly comprising reinforcement of the diameter, grade and profile to be used, and a coupler of the precise type to be used, is tested in tension the permanent elongation after loading to 0.6 [yield strength] should not exceed 0.1 millimetre; and the coupled bar assembly tensile strength should exceed 287.5 newtons per millimetre squared for grade 250, and 483 newtons per millimetre squared for grade 460." So you confirm it's actually a requirement under the	2 3 4 5 6 7 8 9 10 11	<ul> <li>BOSA were not requested to do this or that BOSA failed to do it. There's quite a difference, because BOSA is not a party, and that would be a criticism of BOSA if we use the suggestion "failed". But if they were not asked to do it by way of later testing, that's a different matter.</li> <li>MR CHOW: Sir, the last line of questions that I asked actually related to the test carried out by BOSA to the partially engaged couplers for the purpose of the Commission, in relation to which my instruction is that the test was carried out by BOSA without the request of</li> </ul>
2 3 4 5 6 7 8 9 10 11 12	" when a representative gauge length assembly comprising reinforcement of the diameter, grade and profile to be used, and a coupler of the precise type to be used, is tested in tension the permanent elongation after loading to 0.6 [yield strength] should not exceed 0.1 millimetre; and the coupled bar assembly tensile strength should exceed 287.5 newtons per millimetre squared for grade 250, and 483 newtons per millimetre squared for grade 460." So you confirm it's actually a requirement under the 2004 Concrete Code?	2 3 4 5 6 7 8 9 10 11 12	<ul> <li>BOSA were not requested to do this or that BOSA failed to do it. There's quite a difference, because BOSA is not a party, and that would be a criticism of BOSA if we use the suggestion "failed". But if they were not asked to do it by way of later testing, that's a different matter.</li> <li>MR CHOW: Sir, the last line of questions that I asked actually related to the test carried out by BOSA to the partially engaged couplers for the purpose of the Commission, in relation to which my instruction is that the test was carried out by BOSA without the request of the Buildings Department, and the Buildings Department</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13	" when a representative gauge length assembly comprising reinforcement of the diameter, grade and profile to be used, and a coupler of the precise type to be used, is tested in tension the permanent elongation after loading to 0.6 [yield strength] should not exceed 0.1 millimetre; and the coupled bar assembly tensile strength should exceed 287.5 newtons per millimetre squared for grade 250, and 483 newtons per millimetre squared for grade 460." So you confirm it's actually a requirement under the 2004 Concrete Code? A. For couplers, yes.	2 3 4 5 6 7 8 9 10 11 12 13	<ul> <li>BOSA were not requested to do this or that BOSA failed to do it. There's quite a difference, because BOSA is not a party, and that would be a criticism of BOSA if we use the suggestion "failed". But if they were not asked to do it by way of later testing, that's a different matter.</li> <li>MR CHOW: Sir, the last line of questions that I asked actually related to the test carried out by BOSA to the partially engaged couplers for the purpose of the Commission, in relation to which my instruction is that the test was carried out by BOSA without the request of the Buildings Department, and the Buildings Department was only invited on the day of the testing to send</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14	<ul> <li>" when a representative gauge length assembly comprising reinforcement of the diameter, grade and profile to be used, and a coupler of the precise type to be used, is tested in tension the permanent elongation after loading to 0.6 [yield strength] should not exceed 0.1 millimetre; and</li> <li> the coupled bar assembly tensile strength should exceed 287.5 newtons per millimetre squared for grade 250, and 483 newtons per millimetre squared for grade 460."</li> <li>So you confirm it's actually a requirement under the 2004 Concrete Code?</li> <li>A. For couplers, yes.</li> <li>Q. And this requirement actually applies to both ductile</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15	<ul> <li>BOSA were not requested to do this or that BOSA failed to do it. There's quite a difference, because BOSA is not a party, and that would be a criticism of BOSA if we use the suggestion "failed". But if they were not asked to do it by way of later testing, that's a different matter.</li> <li>MR CHOW: Sir, the last line of questions that I asked actually related to the test carried out by BOSA to the partially engaged couplers for the purpose of the Commission, in relation to which my instruction is that the test was carried out by BOSA without the request of the Buildings Department, and the Buildings Department was only invited on the day of the testing to send someone to witness the test.</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	<ul> <li>" when a representative gauge length assembly comprising reinforcement of the diameter, grade and profile to be used, and a coupler of the precise type to be used, is tested in tension the permanent elongation after loading to 0.6 [yield strength] should not exceed 0.1 millimetre; and</li> <li> the coupled bar assembly tensile strength should exceed 287.5 newtons per millimetre squared for grade 250, and 483 newtons per millimetre squared for grade 460."</li> <li>So you confirm it's actually a requirement under the 2004 Concrete Code?</li> <li>A. For couplers, yes.</li> <li>Q. And this requirement actually applies to both ductile and non-ductile couplers; correct?</li> <li>A. I think in 2004 they may not consider ductile coupler at that time.</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	<ul> <li>BOSA were not requested to do this or that BOSA failed to do it. There's quite a difference, because BOSA is not a party, and that would be a criticism of BOSA if we use the suggestion "failed". But if they were not asked to do it by way of later testing, that's a different matter.</li> <li>MR CHOW: Sir, the last line of questions that I asked actually related to the test carried out by BOSA to the partially engaged couplers for the purpose of the Commission, in relation to which my instruction is that the test was carried out by BOSA without the request of the Buildings Department, and the Buildings Department was only invited on the day of the testing to send someone to witness the test.</li> <li>It is not clear whether the test performed by BOSA was originally requested by MTR or not. That is something beyond my knowledge or the government's</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	<ul> <li>" when a representative gauge length assembly comprising reinforcement of the diameter, grade and profile to be used, and a coupler of the precise type to be used, is tested in tension the permanent elongation after loading to 0.6 [yield strength] should not exceed 0.1 millimetre; and</li> <li> the coupled bar assembly tensile strength should exceed 287.5 newtons per millimetre squared for grade 250, and 483 newtons per millimetre squared for grade 460."</li> <li>So you confirm it's actually a requirement under the 2004 Concrete Code?</li> <li>A. For couplers, yes.</li> <li>Q. And this requirement actually applies to both ductile and non-ductile couplers; correct?</li> <li>A. I think in 2004 they may not consider ductile coupler at that time.</li> <li>Q. Okay. But the acceptance letter from the Buildings</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	<ul> <li>BOSA were not requested to do this or that BOSA failed to do it. There's quite a difference, because BOSA is not a party, and that would be a criticism of BOSA if we use the suggestion "failed". But if they were not asked to do it by way of later testing, that's a different matter.</li> <li>MR CHOW: Sir, the last line of questions that I asked actually related to the test carried out by BOSA to the partially engaged couplers for the purpose of the Commission, in relation to which my instruction is that the test was carried out by BOSA without the request of the Buildings Department, and the Buildings Department was only invited on the day of the testing to send someone to witness the test.</li> <li>It is not clear whether the test performed by BOSA was originally requested by MTR or not. That is something beyond my knowledge or the government's knowledge.</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	<ul> <li>" when a representative gauge length assembly comprising reinforcement of the diameter, grade and profile to be used, and a coupler of the precise type to be used, is tested in tension the permanent elongation after loading to 0.6 [yield strength] should not exceed 0.1 millimetre; and</li> <li> the coupled bar assembly tensile strength should exceed 287.5 newtons per millimetre squared for grade 250, and 483 newtons per millimetre squared for grade 460."</li> <li>So you confirm it's actually a requirement under the 2004 Concrete Code?</li> <li>A. For couplers, yes.</li> <li>Q. And this requirement actually applies to both ductile and non-ductile couplers; correct?</li> <li>A. I think in 2004 they may not consider ductile coupler at that time.</li> <li>Q. Okay. But the acceptance letter from the Buildings Department also sets out testing requirement for</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	<ul> <li>BOSA were not requested to do this or that BOSA failed to do it. There's quite a difference, because BOSA is not a party, and that would be a criticism of BOSA if we use the suggestion "failed". But if they were not asked to do it by way of later testing, that's a different matter.</li> <li>MR CHOW: Sir, the last line of questions that I asked actually related to the test carried out by BOSA to the partially engaged couplers for the purpose of the Commission, in relation to which my instruction is that the test was carried out by BOSA without the request of the Buildings Department, and the Buildings Department was only invited on the day of the testing to send someone to witness the test.</li> <li>It is not clear whether the test performed by BOSA was originally requested by MTR or not. That is something beyond my knowledge or the government's knowledge.</li> <li>CHAIRMAN: All right. That puts it into context.</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	<ul> <li>" when a representative gauge length assembly comprising reinforcement of the diameter, grade and profile to be used, and a coupler of the precise type to be used, is tested in tension the permanent elongation after loading to 0.6 [yield strength] should not exceed 0.1 millimetre; and <ul> <li> the coupled bar assembly tensile strength</li> <li>should exceed 287.5 newtons per millimetre squared for grade 250, and 483 newtons per millimetre squared for grade 460."</li> <li>So you confirm it's actually a requirement under the 2004 Concrete Code?</li> </ul> </li> <li>A. For couplers, yes.</li> <li>Q. And this requirement actually applies to both ductile and non-ductile couplers; correct?</li> <li>A. I think in 2004 they may not consider ductile coupler at that time.</li> <li>Q. Okay. But the acceptance letter from the Buildings Department also sets out testing requirement for non-ductile couplers. Can I ask you to go back to the</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	<ul> <li>BOSA were not requested to do this or that BOSA failed to do it. There's quite a difference, because BOSA is not a party, and that would be a criticism of BOSA if we use the suggestion "failed". But if they were not asked to do it by way of later testing, that's a different matter.</li> <li>MR CHOW: Sir, the last line of questions that I asked actually related to the test carried out by BOSA to the partially engaged couplers for the purpose of the Commission, in relation to which my instruction is that the test was carried out by BOSA without the request of the Buildings Department, and the Buildings Department was only invited on the day of the testing to send someone to witness the test.</li> <li>It is not clear whether the test performed by BOSA was originally requested by MTR or not. That is something beyond my knowledge or the government's knowledge.</li> <li>CHAIRMAN: All right. That puts it into context. MR CHOW: Yes.</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	<ul> <li>" when a representative gauge length assembly comprising reinforcement of the diameter, grade and profile to be used, and a coupler of the precise type to be used, is tested in tension the permanent elongation after loading to 0.6 [yield strength] should not exceed 0.1 millimetre; and</li> <li> the coupled bar assembly tensile strength should exceed 287.5 newtons per millimetre squared for grade 250, and 483 newtons per millimetre squared for grade 460."</li> <li>So you confirm it's actually a requirement under the 2004 Concrete Code?</li> <li>A. For couplers, yes.</li> <li>Q. And this requirement actually applies to both ductile and non-ductile couplers; correct?</li> <li>A. I think in 2004 they may not consider ductile coupler at that time.</li> <li>Q. Okay. But the acceptance letter from the Buildings Department also sets out testing requirement for non-ductile couplers. Can I ask you to go back to the acceptance letter, bundle H9, page 3934. This is the</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	<ul> <li>BOSA were not requested to do this or that BOSA failed to do it. There's quite a difference, because BOSA is not a party, and that would be a criticism of BOSA if we use the suggestion "failed". But if they were not asked to do it by way of later testing, that's a different matter.</li> <li>MR CHOW: Sir, the last line of questions that I asked actually related to the test carried out by BOSA to the partially engaged couplers for the purpose of the Commission, in relation to which my instruction is that the test was carried out by BOSA without the request of the Buildings Department, and the Buildings Department was only invited on the day of the testing to send someone to witness the test.</li> <li>It is not clear whether the test performed by BOSA was originally requested by MTR or not. That is something beyond my knowledge or the government's knowledge.</li> <li>CHAIRMAN: All right. That puts it into context.</li> <li>MR PENNICOTT: Sir, there was certainly no failure. It may</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>" when a representative gauge length assembly comprising reinforcement of the diameter, grade and profile to be used, and a coupler of the precise type to be used, is tested in tension the permanent elongation after loading to 0.6 [yield strength] should not exceed 0.1 millimetre; and <ul> <li> the coupled bar assembly tensile strength</li> <li>should exceed 287.5 newtons per millimetre squared for grade 250, and 483 newtons per millimetre squared for grade 460."</li> <li>So you confirm it's actually a requirement under the 2004 Concrete Code?</li> </ul> </li> <li>A. For couplers, yes.</li> <li>Q. And this requirement actually applies to both ductile and non-ductile couplers; correct?</li> <li>A. I think in 2004 they may not consider ductile coupler at that time.</li> <li>Q. Okay. But the acceptance letter from the Buildings Department also sets out testing requirement for non-ductile couplers. Can I ask you to go back to the acceptance letter, bundle H9, page 3934. This is the same acceptance letter that we have just looked at, it's</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>BOSA were not requested to do this or that BOSA failed to do it. There's quite a difference, because BOSA is not a party, and that would be a criticism of BOSA if we use the suggestion "failed". But if they were not asked to do it by way of later testing, that's a different matter.</li> <li>MR CHOW: Sir, the last line of questions that I asked actually related to the test carried out by BOSA to the partially engaged couplers for the purpose of the Commission, in relation to which my instruction is that the test was carried out by BOSA without the request of the Buildings Department, and the Buildings Department was only invited on the day of the testing to send someone to witness the test.</li> <li>It is not clear whether the test performed by BOSA was originally requested by MTR or not. That is something beyond my knowledge or the government's knowledge.</li> <li>CHAIRMAN: All right. That puts it into context.</li> <li>MR PENNICOTT: Sir, there was certainly no failure. It may be I'm in a very similar situation to Mr Chow. I'm</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	<ul> <li>" when a representative gauge length assembly comprising reinforcement of the diameter, grade and profile to be used, and a coupler of the precise type to be used, is tested in tension the permanent elongation after loading to 0.6 [yield strength] should not exceed 0.1 millimetre; and <ul> <li> the coupled bar assembly tensile strength</li> <li>should exceed 287.5 newtons per millimetre squared for grade 250, and 483 newtons per millimetre squared for grade 460."</li> <li>So you confirm it's actually a requirement under the 2004 Concrete Code?</li> </ul> </li> <li>A. For couplers, yes.</li> <li>Q. And this requirement actually applies to both ductile and non-ductile couplers; correct?</li> <li>A. I think in 2004 they may not consider ductile coupler at that time.</li> <li>Q. Okay. But the acceptance letter from the Buildings Department also sets out testing requirement for non-ductile couplers. Can I ask you to go back to the acceptance letter, bundle H9, page 3934. This is the same acceptance letter that we have just looked at, it's just that this is another page under the section for</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	<ul> <li>BOSA were not requested to do this or that BOSA failed to do it. There's quite a difference, because BOSA is not a party, and that would be a criticism of BOSA if we use the suggestion "failed". But if they were not asked to do it by way of later testing, that's a different matter.</li> <li>MR CHOW: Sir, the last line of questions that I asked actually related to the test carried out by BOSA to the partially engaged couplers for the purpose of the Commission, in relation to which my instruction is that the test was carried out by BOSA without the request of the Buildings Department, and the Buildings Department was only invited on the day of the testing to send someone to witness the test.</li> <li>It is not clear whether the test performed by BOSA was originally requested by MTR or not. That is something beyond my knowledge or the government's knowledge.</li> <li>CHAIRMAN: All right. That puts it into context.</li> <li>MR CHOW: Yes.</li> <li>MR PENNICOTT: Sir, there was certainly no failure. It may be I'm in a very similar situation to Mr Chow. I'm still struggling a little bit to help the Commission in</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>" when a representative gauge length assembly comprising reinforcement of the diameter, grade and profile to be used, and a coupler of the precise type to be used, is tested in tension the permanent elongation after loading to 0.6 [yield strength] should not exceed 0.1 millimetre; and <ul> <li> the coupled bar assembly tensile strength</li> <li>should exceed 287.5 newtons per millimetre squared for grade 250, and 483 newtons per millimetre squared for grade 460."</li> <li>So you confirm it's actually a requirement under the 2004 Concrete Code?</li> </ul> </li> <li>A. For couplers, yes.</li> <li>Q. And this requirement actually applies to both ductile and non-ductile couplers; correct?</li> <li>A. I think in 2004 they may not consider ductile coupler at that time.</li> <li>Q. Okay. But the acceptance letter from the Buildings Department also sets out testing requirement for non-ductile couplers. Can I ask you to go back to the acceptance letter, bundle H9, page 3934. This is the same acceptance letter that we have just looked at, it's</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>BOSA were not requested to do this or that BOSA failed to do it. There's quite a difference, because BOSA is not a party, and that would be a criticism of BOSA if we use the suggestion "failed". But if they were not asked to do it by way of later testing, that's a different matter.</li> <li>MR CHOW: Sir, the last line of questions that I asked actually related to the test carried out by BOSA to the partially engaged couplers for the purpose of the Commission, in relation to which my instruction is that the test was carried out by BOSA without the request of the Buildings Department, and the Buildings Department was only invited on the day of the testing to send someone to witness the test.</li> <li>It is not clear whether the test performed by BOSA was originally requested by MTR or not. That is something beyond my knowledge or the government's knowledge.</li> <li>CHAIRMAN: All right. That puts it into context.</li> <li>MR PENNICOTT: Sir, there was certainly no failure. It may be I'm in a very similar situation to Mr Chow. I'm</li> </ul>

	Page 61		Page 63
1	failure, which is quite possible, I'm not convinced it	1	this kind of change has to inform the Buildings
2	was something initiated by the Commission itself, and if	2	Department and get its acceptance before the
3	that is correct then I'm still a little bit, as I say,	3	implementation of the changes.
4	factually unclear as to precisely the provenance and how	4	The issue now is what is the proper classification
5	all that came about in the first place.	5	of the station box structure. The expert instructed by
6	CHAIRMAN: I accept that.	6	Leighton
7	MR PENNICOTT: So I certainly don't think one can categorise	7	CHAIRMAN: Sorry, I am interrupting you again; I do
8	it as a failure. Clearly they either did it of their	8	apologise. This is a classification question, is it
9	own initiative or somebody asked them to do it. I don't	9	not, that may differ from one jurisdiction to another,
10	think it was the Commission and it doesn't sound as	10	so that in jurisdiction A I may be wrong here; please
11	though it was the government, so the number of potential	11	tell me if I am. In jurisdiction A they may say this
12	requesters are limited.	12	type of working classifies as a foundation whereas in
13	CHAIRMAN: Good. I'm sure you understand my position	13	jurisdiction B it may, depending on certain things,
14	though	14	classify as superstructure. I'm just wondering,
15	MR PENNICOTT: Yes.	15	therefore, if the professor, with due acknowledgement of
16	CHAIRMAN: that obviously if BOSA is criticised in some	16	all his skills, is actually in a position to determine
17	way, it would be quite wrong for them, not being	17	a classification in Hong Kong of a particular form of
18	parties, to just pick it up somewhere or other in the	18	building.
19	media at some later stage, without being given	19	MR PENNICOTT: Also, sir, there's a rather broader question
20	an opportunity to reply.	20	that has arisen on a number of occasions already, as to
21	MR PENNICOTT: Of course, sir.	21	whether this is actually an issue which concerns the
22	MR CHOW: Sir, can I also add this: from my recollection,	22	Commission at all in any event.
23	Mr Glover's report also mentioned about the tests as	23	CHAIRMAN: Because I think we made it quite clear earlier
24	something commissioned by MTRC. That is where I got	24	on, we were not being pulled into any aspects related to
25	that impression. Perhaps we can clarify with Mr Glover	25	the sort of thing that arises in civil litigation. You
	Page 62		Page 64
1	Page 62 later on.	1	Page 64 know, you have built to this or built to that and
1 2	-	1 2	-
	later on.		know, you have built to this or built to that and
2	later on. As Mr Pennicott said, at the moment it is not clear	2	know, you have built to this or built to that and somebody has to determine what it is in law. So I'm
2 3	later on. As Mr Pennicott said, at the moment it is not clear to the government as to who was the one who initiated	2 3	know, you have built to this or built to that and somebody has to determine what it is in law. So I'm a bit concerned as to whether we should really be
2 3 4	later on. As Mr Pennicott said, at the moment it is not clear to the government as to who was the one who initiated this test, but definitely not the government.	2 3 4	<ul><li>know, you have built to this or built to that and somebody has to determine what it is in law. So I'm a bit concerned as to whether we should really be enticed into this area.</li><li>MR CHOW: Sir, may I try to assist further on this point? The reason why I need to ask this question actually</li></ul>
2 3 4 5	later on. As Mr Pennicott said, at the moment it is not clear to the government as to who was the one who initiated this test, but definitely not the government. Prof Yeung, I have one last topic I would like to	2 3 4 5	know, you have built to this or built to that and somebody has to determine what it is in law. So I'm a bit concerned as to whether we should really be enticed into this area. MR CHOW: Sir, may I try to assist further on this point?
2 3 4 5 6	later on. As Mr Pennicott said, at the moment it is not clear to the government as to who was the one who initiated this test, but definitely not the government. Prof Yeung, I have one last topic I would like to explore with you. You know, when I heard about your credentials, I noticed that you are a specialist in geotechnical engineering.	2 3 4 5 6	<ul><li>know, you have built to this or built to that and somebody has to determine what it is in law. So I'm a bit concerned as to whether we should really be enticed into this area.</li><li>MR CHOW: Sir, may I try to assist further on this point? The reason why I need to ask this question actually relates to one of the issues I believe that the Commission would be interested in. That is whether</li></ul>
2 3 4 5 6 7	later on. As Mr Pennicott said, at the moment it is not clear to the government as to who was the one who initiated this test, but definitely not the government. Prof Yeung, I have one last topic I would like to explore with you. You know, when I heard about your credentials, I noticed that you are a specialist in	2 3 4 5 6 7	<ul><li>know, you have built to this or built to that and somebody has to determine what it is in law. So I'm a bit concerned as to whether we should really be enticed into this area.</li><li>MR CHOW: Sir, may I try to assist further on this point? The reason why I need to ask this question actually relates to one of the issues I believe that the Commission would be interested in. That is whether prior consultation with the Buildings Department before</li></ul>
2 3 4 5 6 7 8	<ul> <li>later on.</li> <li>As Mr Pennicott said, at the moment it is not clear to the government as to who was the one who initiated this test, but definitely not the government.</li> <li>Prof Yeung, I have one last topic I would like to explore with you. You know, when I heard about your credentials, I noticed that you are a specialist in geotechnical engineering.</li> <li>A. Correct.</li> <li>Q. One of the issues so far that has given rise is how we</li> </ul>	2 3 4 5 6 7 8	<ul><li>know, you have built to this or built to that and somebody has to determine what it is in law. So I'm a bit concerned as to whether we should really be enticed into this area.</li><li>MR CHOW: Sir, may I try to assist further on this point? The reason why I need to ask this question actually relates to one of the issues I believe that the Commission would be interested in. That is whether prior consultation with the Buildings Department before the implementation of the changes is required.</li></ul>
2 3 4 5 6 7 8 9 10 11	<ul> <li>later on.</li> <li>As Mr Pennicott said, at the moment it is not clear to the government as to who was the one who initiated this test, but definitely not the government.</li> <li>Prof Yeung, I have one last topic I would like to explore with you. You know, when I heard about your credentials, I noticed that you are a specialist in geotechnical engineering.</li> <li>A. Correct.</li> <li>Q. One of the issues so far that has given rise is how we should classify the station box structure, comprising</li> </ul>	2 3 4 5 6 7 8 9 10 11	<ul> <li>know, you have built to this or built to that and somebody has to determine what it is in law. So I'm a bit concerned as to whether we should really be enticed into this area.</li> <li>MR CHOW: Sir, may I try to assist further on this point? The reason why I need to ask this question actually relates to one of the issues I believe that the Commission would be interested in. That is whether prior consultation with the Buildings Department before the implementation of the changes is required. Given the experts also discuss about the implication</li> </ul>
2 3 4 5 6 7 8 9 10 11 12	<ul> <li>later on.</li> <li>As Mr Pennicott said, at the moment it is not clear to the government as to who was the one who initiated this test, but definitely not the government.</li> <li>Prof Yeung, I have one last topic I would like to explore with you. You know, when I heard about your credentials, I noticed that you are a specialist in geotechnical engineering.</li> <li>A. Correct.</li> <li>Q. One of the issues so far that has given rise is how we should classify the station box structure, comprising the platform slab and the diaphragm wall.</li> </ul>	2 3 4 5 6 7 8 9 10	know, you have built to this or built to that and somebody has to determine what it is in law. So I'm a bit concerned as to whether we should really be enticed into this area. MR CHOW: Sir, may I try to assist further on this point? The reason why I need to ask this question actually relates to one of the issues I believe that the Commission would be interested in. That is whether prior consultation with the Buildings Department before the implementation of the changes is required. Given the experts also discuss about the implication of a practice note, PNAP ADM-19
2 3 4 5 6 7 8 9 10 11 12 13	<ul> <li>later on.</li> <li>As Mr Pennicott said, at the moment it is not clear to the government as to who was the one who initiated this test, but definitely not the government.</li> <li>Prof Yeung, I have one last topic I would like to explore with you. You know, when I heard about your credentials, I noticed that you are a specialist in geotechnical engineering.</li> <li>A. Correct.</li> <li>Q. One of the issues so far that has given rise is how we should classify the station box structure, comprising the platform slab and the diaphragm wall.</li> <li>The position of the government or some of the</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13	<ul> <li>know, you have built to this or built to that and somebody has to determine what it is in law. So I'm a bit concerned as to whether we should really be enticed into this area.</li> <li>MR CHOW: Sir, may I try to assist further on this point? The reason why I need to ask this question actually relates to one of the issues I believe that the Commission would be interested in. That is whether prior consultation with the Buildings Department before the implementation of the changes is required. Given the experts also discuss about the implication of a practice note, PNAP ADM-19</li> <li>CHAIRMAN: I appreciate all of that. That's why we are</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14	<ul> <li>later on.</li> <li>As Mr Pennicott said, at the moment it is not clear to the government as to who was the one who initiated this test, but definitely not the government.</li> <li>Prof Yeung, I have one last topic I would like to explore with you. You know, when I heard about your credentials, I noticed that you are a specialist in geotechnical engineering.</li> <li>A. Correct.</li> <li>Q. One of the issues so far that has given rise is how we should classify the station box structure, comprising the platform slab and the diaphragm wall.</li> <li>The position of the government or some of the factual witnesses for example, Mr Humphrey Ho of the</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14	<ul> <li>know, you have built to this or built to that and somebody has to determine what it is in law. So I'm a bit concerned as to whether we should really be enticed into this area.</li> <li>MR CHOW: Sir, may I try to assist further on this point? The reason why I need to ask this question actually relates to one of the issues I believe that the Commission would be interested in. That is whether prior consultation with the Buildings Department before the implementation of the changes is required. Given the experts also discuss about the implication of a practice note, PNAP ADM-19</li> <li>CHAIRMAN: I appreciate all of that. That's why we are aware of the fact that this issue has been dealt with.</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15	<ul> <li>later on.</li> <li>As Mr Pennicott said, at the moment it is not clear to the government as to who was the one who initiated this test, but definitely not the government.</li> <li>Prof Yeung, I have one last topic I would like to explore with you. You know, when I heard about your credentials, I noticed that you are a specialist in geotechnical engineering.</li> <li>A. Correct.</li> <li>Q. One of the issues so far that has given rise is how we should classify the station box structure, comprising the platform slab and the diaphragm wall.</li> <li>The position of the government or some of the factual witnesses for example, Mr Humphrey Ho of the Buildings Department considers the diaphragm wall</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15	<ul> <li>know, you have built to this or built to that and somebody has to determine what it is in law. So I'm a bit concerned as to whether we should really be enticed into this area.</li> <li>MR CHOW: Sir, may I try to assist further on this point? The reason why I need to ask this question actually relates to one of the issues I believe that the Commission would be interested in. That is whether prior consultation with the Buildings Department before the implementation of the changes is required. Given the experts also discuss about the implication of a practice note, PNAP ADM-19</li> <li>CHAIRMAN: I appreciate all of that. That's why we are aware of the fact that this issue has been dealt with. I don't see it falling into our terms of reference.</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	<ul> <li>later on.</li> <li>As Mr Pennicott said, at the moment it is not clear to the government as to who was the one who initiated this test, but definitely not the government.</li> <li>Prof Yeung, I have one last topic I would like to explore with you. You know, when I heard about your credentials, I noticed that you are a specialist in geotechnical engineering.</li> <li>A. Correct.</li> <li>Q. One of the issues so far that has given rise is how we should classify the station box structure, comprising the platform slab and the diaphragm wall.</li> <li>The position of the government or some of the factual witnesses for example, Mr Humphrey Ho of the Buildings Department considers the diaphragm wall forming part of the station structure, it should be</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	<ul> <li>know, you have built to this or built to that and somebody has to determine what it is in law. So I'm a bit concerned as to whether we should really be enticed into this area.</li> <li>MR CHOW: Sir, may I try to assist further on this point? The reason why I need to ask this question actually relates to one of the issues I believe that the Commission would be interested in. That is whether prior consultation with the Buildings Department before the implementation of the changes is required. Given the experts also discuss about the implication of a practice note, PNAP ADM-19</li> <li>CHAIRMAN: I appreciate all of that. That's why we are aware of the fact that this issue has been dealt with. I don't see it falling into our terms of reference. I can certainly see a situation arising as to as-built</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	<ul> <li>later on.</li> <li>As Mr Pennicott said, at the moment it is not clear to the government as to who was the one who initiated this test, but definitely not the government.</li> <li>Prof Yeung, I have one last topic I would like to explore with you. You know, when I heard about your credentials, I noticed that you are a specialist in geotechnical engineering.</li> <li>A. Correct.</li> <li>Q. One of the issues so far that has given rise is how we should classify the station box structure, comprising the platform slab and the diaphragm wall.</li> <li>The position of the government or some of the factual witnesses for example, Mr Humphrey Ho of the Buildings Department considers the diaphragm wall forming part of the station structure, it should be considered as foundation; right? We also have evidence</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	<ul> <li>know, you have built to this or built to that and somebody has to determine what it is in law. So I'm a bit concerned as to whether we should really be enticed into this area.</li> <li>MR CHOW: Sir, may I try to assist further on this point? The reason why I need to ask this question actually relates to one of the issues I believe that the Commission would be interested in. That is whether prior consultation with the Buildings Department before the implementation of the changes is required. Given the experts also discuss about the implication of a practice note, PNAP ADM-19</li> <li>CHAIRMAN: I appreciate all of that. That's why we are aware of the fact that this issue has been dealt with. I don't see it falling into our terms of reference. I can certainly see a situation arising as to as-built drawings. I can certainly see the argument being there</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	<ul> <li>later on.</li> <li>As Mr Pennicott said, at the moment it is not clear to the government as to who was the one who initiated this test, but definitely not the government.</li> <li>Prof Yeung, I have one last topic I would like to explore with you. You know, when I heard about your credentials, I noticed that you are a specialist in geotechnical engineering.</li> <li>A. Correct.</li> <li>Q. One of the issues so far that has given rise is how we should classify the station box structure, comprising the platform slab and the diaphragm wall.</li> <li>The position of the government or some of the factual witnesses for example, Mr Humphrey Ho of the Buildings Department considers the diaphragm wall forming part of the station structure, it should be considered as foundation; right? We also have evidence from an Atkins engineer, for example Mr Sung, who</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	<ul> <li>know, you have built to this or built to that and somebody has to determine what it is in law. So I'm a bit concerned as to whether we should really be enticed into this area.</li> <li>MR CHOW: Sir, may I try to assist further on this point? The reason why I need to ask this question actually relates to one of the issues I believe that the Commission would be interested in. That is whether prior consultation with the Buildings Department before the implementation of the changes is required. Given the experts also discuss about the implication of a practice note, PNAP ADM-19</li> <li>CHAIRMAN: I appreciate all of that. That's why we are aware of the fact that this issue has been dealt with. I don't see it falling into our terms of reference. I can certainly see a situation arising as to as-built drawings. I can certainly see the argument being there should have been earlier consultation. And then the</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	<ul> <li>later on.</li> <li>As Mr Pennicott said, at the moment it is not clear to the government as to who was the one who initiated this test, but definitely not the government.</li> <li>Prof Yeung, I have one last topic I would like to explore with you. You know, when I heard about your credentials, I noticed that you are a specialist in geotechnical engineering.</li> <li>A. Correct.</li> <li>Q. One of the issues so far that has given rise is how we should classify the station box structure, comprising the platform slab and the diaphragm wall.</li> <li>The position of the government or some of the factual witnesses for example, Mr Humphrey Ho of the Buildings Department considers the diaphragm wall forming part of the station structure, it should be considered as foundation; right? We also have evidence from an Atkins engineer, for example Mr Sung, who confirmed that to him the change made to the top of the</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	<ul> <li>know, you have built to this or built to that and somebody has to determine what it is in law. So I'm a bit concerned as to whether we should really be enticed into this area.</li> <li>MR CHOW: Sir, may I try to assist further on this point? The reason why I need to ask this question actually relates to one of the issues I believe that the Commission would be interested in. That is whether prior consultation with the Buildings Department before the implementation of the changes is required. Given the experts also discuss about the implication of a practice note, PNAP ADM-19</li> <li>CHAIRMAN: I appreciate all of that. That's why we are aware of the fact that this issue has been dealt with. I don't see it falling into our terms of reference. I can certainly see a situation arising as to as-built drawings. I can certainly see the argument being there should have been earlier consultation. And then the question is whether it was required or not. But as to</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	<ul> <li>later on.</li> <li>As Mr Pennicott said, at the moment it is not clear to the government as to who was the one who initiated this test, but definitely not the government.</li> <li>Prof Yeung, I have one last topic I would like to explore with you. You know, when I heard about your credentials, I noticed that you are a specialist in geotechnical engineering.</li> <li>A. Correct.</li> <li>Q. One of the issues so far that has given rise is how we should classify the station box structure, comprising the platform slab and the diaphragm wall.</li> <li>The position of the government or some of the factual witnesses for example, Mr Humphrey Ho of the Buildings Department considers the diaphragm wall forming part of the station structure, it should be considered as foundation; right? We also have evidence from an Atkins engineer, for example Mr Sung, who confirmed that to him the change made to the</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	<ul> <li>know, you have built to this or built to that and somebody has to determine what it is in law. So I'm a bit concerned as to whether we should really be enticed into this area.</li> <li>MR CHOW: Sir, may I try to assist further on this point? The reason why I need to ask this question actually relates to one of the issues I believe that the Commission would be interested in. That is whether prior consultation with the Buildings Department before the implementation of the changes is required. Given the experts also discuss about the implication of a practice note, PNAP ADM-19</li> <li>CHAIRMAN: I appreciate all of that. That's why we are aware of the fact that this issue has been dealt with. I don't see it falling into our terms of reference. I can certainly see a situation arising as to as-built drawings. I can certainly see the argument being there should have been earlier consultation. And then the question is whether it was required or not. But as to whether it was required or not, that seems to us at the</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	<ul> <li>later on.</li> <li>As Mr Pennicott said, at the moment it is not clear to the government as to who was the one who initiated this test, but definitely not the government.</li> <li>Prof Yeung, I have one last topic I would like to explore with you. You know, when I heard about your credentials, I noticed that you are a specialist in geotechnical engineering.</li> <li>A. Correct.</li> <li>Q. One of the issues so far that has given rise is how we should classify the station box structure, comprising the platform slab and the diaphragm wall.</li> <li>The position of the government or some of the factual witnesses for example, Mr Humphrey Ho of the Buildings Department considers the diaphragm wall forming part of the station structure, it should be considered as foundation; right? We also have evidence from an Atkins engineer, for example Mr Sung, who confirmed that to him the change made to the foundation, and he also advised the Commission that</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	<ul> <li>know, you have built to this or built to that and somebody has to determine what it is in law. So I'm a bit concerned as to whether we should really be enticed into this area.</li> <li>MR CHOW: Sir, may I try to assist further on this point? The reason why I need to ask this question actually relates to one of the issues I believe that the Commission would be interested in. That is whether prior consultation with the Buildings Department before the implementation of the changes is required. Given the experts also discuss about the implication of a practice note, PNAP ADM-19</li> <li>CHAIRMAN: I appreciate all of that. That's why we are aware of the fact that this issue has been dealt with. I don't see it falling into our terms of reference. I can certainly see a situation arising as to as-built drawings. I can certainly see the argument being there should have been earlier consultation. And then the question is whether it was required or not. But as to whether it was required or not, that seems to us at the moment, subject to your representations in a week or so,</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>later on.</li> <li>As Mr Pennicott said, at the moment it is not clear to the government as to who was the one who initiated this test, but definitely not the government.</li> <li>Prof Yeung, I have one last topic I would like to explore with you. You know, when I heard about your credentials, I noticed that you are a specialist in geotechnical engineering.</li> <li>A. Correct.</li> <li>Q. One of the issues so far that has given rise is how we should classify the station box structure, comprising the platform slab and the diaphragm wall.</li> <li>The position of the government or some of the factual witnesses for example, Mr Humphrey Ho of the Buildings Department considers the diaphragm wall forming part of the station structure, it should be considered as foundation; right? We also have evidence from an Atkins engineer, for example Mr Sung, who confirmed that to him the change made to the top of the eastern diaphragm wall is a change made to the point of the government on the prior consultation has to be done with BD before the</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>know, you have built to this or built to that and somebody has to determine what it is in law. So I'm a bit concerned as to whether we should really be enticed into this area.</li> <li>MR CHOW: Sir, may I try to assist further on this point? The reason why I need to ask this question actually relates to one of the issues I believe that the Commission would be interested in. That is whether prior consultation with the Buildings Department before the implementation of the changes is required. Given the experts also discuss about the implication of a practice note, PNAP ADM-19</li> <li>CHAIRMAN: I appreciate all of that. That's why we are aware of the fact that this issue has been dealt with. I don't see it falling into our terms of reference. I can certainly see a situation arising as to as-built drawings. I can certainly see the argument being there should have been earlier consultation. And then the question is whether it was required or not. But as to whether it was required or not, that seems to us at the moment, subject to your representations in a week or so, not to be an issue for us.</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	<ul> <li>later on.</li> <li>As Mr Pennicott said, at the moment it is not clear to the government as to who was the one who initiated this test, but definitely not the government.</li> <li>Prof Yeung, I have one last topic I would like to explore with you. You know, when I heard about your credentials, I noticed that you are a specialist in geotechnical engineering.</li> <li>A. Correct.</li> <li>Q. One of the issues so far that has given rise is how we should classify the station box structure, comprising the platform slab and the diaphragm wall.</li> <li>The position of the government or some of the factual witnesses for example, Mr Humphrey Ho of the Buildings Department considers the diaphragm wall forming part of the station structure, it should be considered as foundation; right? We also have evidence from an Atkins engineer, for example Mr Sung, who confirmed that to him the change made to the top of the eastern diaphragm wall is a change made to the foundation, and he also advised the Commission that prior consultation has to be done with BD before the implementation of the change.</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	<ul> <li>know, you have built to this or built to that and somebody has to determine what it is in law. So I'm a bit concerned as to whether we should really be enticed into this area.</li> <li>MR CHOW: Sir, may I try to assist further on this point? The reason why I need to ask this question actually relates to one of the issues I believe that the Commission would be interested in. That is whether prior consultation with the Buildings Department before the implementation of the changes is required. Given the experts also discuss about the implication of a practice note, PNAP ADM-19</li> <li>CHAIRMAN: I appreciate all of that. That's why we are aware of the fact that this issue has been dealt with. I don't see it falling into our terms of reference. I can certainly see a situation arising as to as-built drawings. I can certainly see the argument being there should have been earlier consultation. And then the question is whether it was required or not. But as to whether it was required or not, that seems to us at the moment, subject to your representations in a week or so, not to be an issue for us.</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>later on.</li> <li>As Mr Pennicott said, at the moment it is not clear to the government as to who was the one who initiated this test, but definitely not the government.</li> <li>Prof Yeung, I have one last topic I would like to explore with you. You know, when I heard about your credentials, I noticed that you are a specialist in geotechnical engineering.</li> <li>A. Correct.</li> <li>Q. One of the issues so far that has given rise is how we should classify the station box structure, comprising the platform slab and the diaphragm wall.</li> <li>The position of the government or some of the factual witnesses for example, Mr Humphrey Ho of the Buildings Department considers the diaphragm wall forming part of the station structure, it should be considered as foundation; right? We also have evidence from an Atkins engineer, for example Mr Sung, who confirmed that to him the change made to the top of the eastern diaphragm wall is a change made to the point of the government on the prior consultation has to be done with BD before the</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>know, you have built to this or built to that and somebody has to determine what it is in law. So I'm a bit concerned as to whether we should really be enticed into this area.</li> <li>MR CHOW: Sir, may I try to assist further on this point? The reason why I need to ask this question actually relates to one of the issues I believe that the Commission would be interested in. That is whether prior consultation with the Buildings Department before the implementation of the changes is required. Given the experts also discuss about the implication of a practice note, PNAP ADM-19</li> <li>CHAIRMAN: I appreciate all of that. That's why we are aware of the fact that this issue has been dealt with. I don't see it falling into our terms of reference. I can certainly see a situation arising as to as-built drawings. I can certainly see the argument being there should have been earlier consultation. And then the question is whether it was required or not. But as to whether it was required or not, that seems to us at the moment, subject to your representations in a week or so, not to be an issue for us.</li> </ul>

	Page 65		Page 67
1	is we stick to our terms of reference and only to our	1	foundation, et cetera.
2	terms of reference	2	So it is actually in relation to this particular
3	MR CHOW: Very well.	3	area that this issue has arisen.
4	CHAIRMAN: and we don't get enticed into other areas; all	4	I have also checked the transcript regarding this
5	right?	5	Monday. In fact when Prof Au was giving evidence,
6	MR CHOW: In that case, I have no more questions. Thank	6	Mr Shieh also referred Mr Au to a particular passage in
7	you.	7	Mr Southward's report regarding this classification in
8	CHAIRMAN: Thank you.	8	relation to the structure.
9	MR CHOW: Thank you, Prof Yeung.	9	CHAIRMAN: You are right.
10	CHAIRMAN: Sorry, Mr Pennicott, as counsel to the tribunal	10	MR SHIEH: That's because the government asked Prof Au
11	does that roughly accord with your approach?	11	a question along those lines and that's what prompted me
12	MR PENNICOTT: It does, sir, yes.	12	to ask him that question.
13	MR SO: Sir, I have some re-examination. I'm entirely in	13	The whole thing about foundation came about because
14	your hands as to whether you want me to do it now.	14	the government witnesses made a point that whether or
15	CHAIRMAN: It's now nearly 12 o'clock, so we will allow for	15	not consultation is needed or not needed may turn on the
16	tea or coffee now.	16	interpretation of that particular practice note, which
17	MR SO: Thank you.	17	then turns on whether or not the D-wall counts as part
18	CHAIRMAN: Quarter of an hour.	18	of the foundation.
19	(11.54 am)	19	CHAIRMAN: That's right.
20	(A short adjournment)	20	MR SHIEH: Which is the origin of all this.
21	(12.17 pm)	21	CHAIRMAN: Sorry to interrupt. I'll let you continue in
22	MR KHAW: Mr Chairman and Mr Commissioner, just on the last	22	a second. What has concerned the Commission is this.
23	point that was discussed between Mr Chow and the	23	We appreciate the issue is one of when this decision was
24	Commission regarding the terms of reference before the	24	made or before it was implemented, should there have
25	morning break I heard what the Commission said and	25	been representations made to the Buildings Department.
	Page 66		Page 68
1	I heard what Mr Pennicott said. I don't want to argue	1	One can look at that more holistically by saying one
2	this point with anybody but it's just that I have a duty	2	needs to build up a culture of cooperation and close
3	to point out that this may have a direct bearing on the	3	liaison; it becomes a joint endeavour in these things.
4	scope of the closing submissions that our team has been	4	Or one can look at it, perhaps and I'm just giving
5	working on.	5	examples at the moment from a much more restrictive
6	CHAIRMAN: Yes.	6	legal perspective, which then becomes a case of saying:
7	MR KHAW: During the break, I had a look at Mr Pennicott's	7	in order to determine whether this was a design change,
8	second opening address. In fact if I can very briefly	8	as opposed to not a design change, one therefore has to
9	refer to one of his sentences which in fact had been	9	determine whether what was being changed was
10	formulated as primary topics of enquiry, one of the	10	a foundation as opposed to a superstructure. It's then
11	question which has been formulated is this:	11	required for the Commission to make a legal
12	"In relation to the connection between the east	12	determination of what, under existing regulations in
13	diaphragm wall and the EWL slab and, in particular, the	13	Hong Kong, constitutes a foundation in respect of the
14	reinforcement steel arrangement in respect thereof,	14	diaphragm walls, et cetera, et cetera.
15	separately in relation to area A, area HKC, area B,	15	That becomes a peculiar and particular legal issue,
16	area C1, area C2 and area C3"	16	and I don't know that we are there may be occasions
17	Under his (v) it says:	17	when it is necessary to do so, and we would be very
18	"Insofar as the as-built situation differs from the	18	happy to be educated on this, but that's our major
19	original design/specification, what reporting to the	19	concern.
20	government ought to have been taken place, if any, when	20	Then, of course, what are we going to do is
21	and by whom?"	21	somebody going to appeal that on the basis that actually
22	I believe it is in this context that parties have	22	we've got it wrong, it's not a foundation, it's
	_		
23	put forward various arguments regarding the	23	a superstructure? It becomes a peculiar legal issue
	_		a superstructure? It becomes a peculiar legal issue that we want to try to avoid. Do you see what I mean? MR KHAW: (Nodded head).

1	Page 69		Page 71
1	MR SHIEH: In fact it resonates, from Leighton's	1	doubt Mr Shieh can confirm this you will recall that
2	perspective, with one observation which came from the	2	on 27 November Mr Shieh and his team put in I think
3	Commission at a certain juncture where the Commission	3	it's somewhere in the bundle; I'm not sure
4	actually observed that the Commission is well aware of	4	a submission on the design change issue, which as
5	certain actions taken by the government in respect of	5	I understood it was indeed an attempt, by Leighton at
6	Leighton prior to the commencement of the Inquiry, but	6	least, to take the Commission away from deciding these
7	the Commission is not going to enter into	7	issues.
8	a determination of the civil aspects of any matters	8	Certainly since then, I'm bound to say I've been
9	which may transpire between Leighton and the government		trying to row the Leighton boat on that particular
10	There may be all kinds of legal disputes subsequently	10	point, that the Commission shouldn't get involved in
11	arising.	11	deciding these rather complex issues which, as you've
12	CHAIRMAN: Yes, of course. Sorry, Mr Khaw, I'll let you	12	said, sir, are rather more relevant perhaps to
12	stand in a second. We are aware that these are the	12	commercial litigation or arbitration or however it may
14	issues, and we've allowed some debate on the issue,	14	be resolved in the future, if it needs to be.
14	because unless we understand the issue we can't know,	14	CHAIRMAN: Yes.
16	for example and this is off the top of my head	16	MR PENNICOTT: Sir, that's really how I have been
10	whether something should come forward from this	17	approaching it since all the evidence has emerged about
17	Commission suggesting more cooperative manoeuvres or	17	the construction of the provisions of the Ordinance and
18 19		18	the contractual documents.
	steps in future between the Buildings Department and various contractors and the like. So we have to know	20	CHAIRMAN: Yes.
20			
21	something about it.	21	MR SHIEH: That is indeed our position. May I echo what the
22	But we don't want to be taken so far into the jaws	22	Chairman has said? It is one thing to say on a high
23	of it that we get chewed up in a legal debate which then	23	level of generality at the very beginning, "Let's
24	becomes a legal decision which should really come from	24	enquire whether or not anyone should be made known about
25	a court of the classic kind as opposed to a Commission	25	it, et cetera, at an earlier stage." But if, as things
	Page 70		Page 72
1	of Inquiry.	1	transpired, the finer points of detail are no longer
2	Mr Khaw, you may want to answer that.	2	whether something should have been sent we know
1			-
3	MR PENNICOTT: Can I just make some observations as well,	3	something had been sent but whether or not, on a fine
4	very briefly?	3 4	something had been sent but whether or not, on a fine legal construction, that amounted to a proper form of
	very briefly? Obviously, what was said in the opening submissions	3	something had been sent but whether or not, on a fine legal construction, that amounted to a proper form of statutory application or consultation, that is
4 5 6	very briefly? Obviously, what was said in the opening submissions has been accurately read out by Mr Khaw and I have no	3 4	something had been sent but whether or not, on a fine legal construction, that amounted to a proper form of statutory application or consultation, that is a completely different kettle of fish and which we had
4 5 6 7	very briefly? Obviously, what was said in the opening submissions has been accurately read out by Mr Khaw and I have no difficulty with that. But what we have here is	3 4 5	something had been sent but whether or not, on a fine legal construction, that amounted to a proper form of statutory application or consultation, that is a completely different kettle of fish and which we had suggested the Commission should stay away from.
4 5 6 7 8	very briefly? Obviously, what was said in the opening submissions has been accurately read out by Mr Khaw and I have no difficulty with that. But what we have here is a dynamic process, and I am bound to say that when	3 4 5 6	something had been sent but whether or not, on a fine legal construction, that amounted to a proper form of statutory application or consultation, that is a completely different kettle of fish and which we had suggested the Commission should stay away from. If what the government wants is some assurance that
4 5 6 7 8 9	very briefly? Obviously, what was said in the opening submissions has been accurately read out by Mr Khaw and I have no difficulty with that. But what we have here is a dynamic process, and I am bound to say that when I wrote that and I take full responsibility for it,	3 4 5 6 7	something had been sent but whether or not, on a fine legal construction, that amounted to a proper form of statutory application or consultation, that is a completely different kettle of fish and which we had suggested the Commission should stay away from. If what the government wants is some assurance that this is not what the terms of reference require and not
4 5 6 7 8 9 10	very briefly? Obviously, what was said in the opening submissions has been accurately read out by Mr Khaw and I have no difficulty with that. But what we have here is a dynamic process, and I am bound to say that when I wrote that and I take full responsibility for it, of course I have to say I was completely unaware of	3 4 5 6 7 8	something had been sent but whether or not, on a fine legal construction, that amounted to a proper form of statutory application or consultation, that is a completely different kettle of fish and which we had suggested the Commission should stay away from. If what the government wants is some assurance that this is not what the terms of reference require and not what the Commission is going to get into, I hope and
4 5 6 7 8 9 10 11	very briefly? Obviously, what was said in the opening submissions has been accurately read out by Mr Khaw and I have no difficulty with that. But what we have here is a dynamic process, and I am bound to say that when I wrote that and I take full responsibility for it, of course I have to say I was completely unaware of where all this was going to lead. I had no idea	3 4 5 6 7 8 9 10 11	something had been sent but whether or not, on a fine legal construction, that amounted to a proper form of statutory application or consultation, that is a completely different kettle of fish and which we had suggested the Commission should stay away from. If what the government wants is some assurance that this is not what the terms of reference require and not what the Commission is going to get into, I hope and I think the government has its answer.
4 5 7 8 9 10 11 12	very briefly? Obviously, what was said in the opening submissions has been accurately read out by Mr Khaw and I have no difficulty with that. But what we have here is a dynamic process, and I am bound to say that when I wrote that and I take full responsibility for it, of course I have to say I was completely unaware of where all this was going to lead. I had no idea of course that all of this ultimately might hinge on the	3 4 5 6 7 8 9 10 11 12	something had been sent but whether or not, on a fine legal construction, that amounted to a proper form of statutory application or consultation, that is a completely different kettle of fish and which we had suggested the Commission should stay away from. If what the government wants is some assurance that this is not what the terms of reference require and not what the Commission is going to get into, I hope and I think the government has its answer. But if what the government now wants is to
4 5 6 7 8 9 10 11 12 13	very briefly? Obviously, what was said in the opening submissions has been accurately read out by Mr Khaw and I have no difficulty with that. But what we have here is a dynamic process, and I am bound to say that when I wrote that and I take full responsibility for it, of course I have to say I was completely unaware of where all this was going to lead. I had no idea of course that all of this ultimately might hinge on the question of whether or not this was a foundation or not	3 4 5 6 7 8 9 10 11 12 13	something had been sent but whether or not, on a fine legal construction, that amounted to a proper form of statutory application or consultation, that is a completely different kettle of fish and which we had suggested the Commission should stay away from. If what the government wants is some assurance that this is not what the terms of reference require and not what the Commission is going to get into, I hope and I think the government has its answer. But if what the government now wants is to positively press for it, then I would respectfully
4 5 6 7 8 9 10 11 12 13 14	very briefly? Obviously, what was said in the opening submissions has been accurately read out by Mr Khaw and I have no difficulty with that. But what we have here is a dynamic process, and I am bound to say that when I wrote that and I take full responsibility for it, of course I have to say I was completely unaware of where all this was going to lead. I had no idea of course that all of this ultimately might hinge on the question of whether or not this was a foundation or not a foundation and all of that.	3 4 5 6 7 8 9 10 11 12 13 14	something had been sent but whether or not, on a fine legal construction, that amounted to a proper form of statutory application or consultation, that is a completely different kettle of fish and which we had suggested the Commission should stay away from. If what the government wants is some assurance that this is not what the terms of reference require and not what the Commission is going to get into, I hope and I think the government has its answer. But if what the government now wants is to positively press for it, then I would respectfully suggest some underlying agenda which is unknown to us.
4 5 6 7 8 9 10 11 12 13 14 15	very briefly? Obviously, what was said in the opening submissions has been accurately read out by Mr Khaw and I have no difficulty with that. But what we have here is a dynamic process, and I am bound to say that when I wrote that and I take full responsibility for it, of course I have to say I was completely unaware of where all this was going to lead. I had no idea of course that all of this ultimately might hinge on the question of whether or not this was a foundation or not a foundation and all of that. I had more in mind at the time that this was	3 4 5 6 7 8 9 10 11 12 13 14 15	something had been sent but whether or not, on a fine legal construction, that amounted to a proper form of statutory application or consultation, that is a completely different kettle of fish and which we had suggested the Commission should stay away from. If what the government wants is some assurance that this is not what the terms of reference require and not what the Commission is going to get into, I hope and I think the government has its answer. But if what the government now wants is to positively press for it, then I would respectfully suggest some underlying agenda which is unknown to us. In other words, if they want assurance, I suspect they
4 5 6 7 8 9 10 11 12 13 14 15 16	very briefly? Obviously, what was said in the opening submissions has been accurately read out by Mr Khaw and I have no difficulty with that. But what we have here is a dynamic process, and I am bound to say that when I wrote that and I take full responsibility for it, of course I have to say I was completely unaware of where all this was going to lead. I had no idea of course that all of this ultimately might hinge on the question of whether or not this was a foundation or not a foundation and all of that. I had more in mind at the time that this was actually going into a potential project management issue	3 4 5 6 7 8 9 10 11 12 13 14	something had been sent but whether or not, on a fine legal construction, that amounted to a proper form of statutory application or consultation, that is a completely different kettle of fish and which we had suggested the Commission should stay away from. If what the government wants is some assurance that this is not what the terms of reference require and not what the Commission is going to get into, I hope and I think the government has its answer. But if what the government now wants is to positively press for it, then I would respectfully suggest some underlying agenda which is unknown to us. In other words, if they want assurance, I suspect they would have got their assurance by now, but if they go
4 5 6 7 8 9 10 11 12 13 14 15 16 17	very briefly? Obviously, what was said in the opening submissions has been accurately read out by Mr Khaw and I have no difficulty with that. But what we have here is a dynamic process, and I am bound to say that when I wrote that and I take full responsibility for it, of course I have to say I was completely unaware of where all this was going to lead. I had no idea of course that all of this ultimately might hinge on the question of whether or not this was a foundation or not a foundation and all of that. I had more in mind at the time that this was actually going into a potential project management issue as to how the MTR and Leighton on the one hand should	3 4 5 6 7 8 9 10 11 12 13 14 15	something had been sent but whether or not, on a fine legal construction, that amounted to a proper form of statutory application or consultation, that is a completely different kettle of fish and which we had suggested the Commission should stay away from. If what the government wants is some assurance that this is not what the terms of reference require and not what the Commission is going to get into, I hope and I think the government has its answer. But if what the government now wants is to positively press for it, then I would respectfully suggest some underlying agenda which is unknown to us. In other words, if they want assurance, I suspect they would have got their assurance by now, but if they go any further, then I hear what they say.
4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	very briefly? Obviously, what was said in the opening submissions has been accurately read out by Mr Khaw and I have no difficulty with that. But what we have here is a dynamic process, and I am bound to say that when I wrote that and I take full responsibility for it, of course I have to say I was completely unaware of where all this was going to lead. I had no idea of course that all of this ultimately might hinge on the question of whether or not this was a foundation or not a foundation and all of that. I had more in mind at the time that this was actually going into a potential project management issue as to how the MTR and Leighton on the one hand should have communicated with the government, was there	3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	something had been sent but whether or not, on a fine legal construction, that amounted to a proper form of statutory application or consultation, that is a completely different kettle of fish and which we had suggested the Commission should stay away from. If what the government wants is some assurance that this is not what the terms of reference require and not what the Commission is going to get into, I hope and I think the government has its answer. But if what the government now wants is to positively press for it, then I would respectfully suggest some underlying agenda which is unknown to us. In other words, if they want assurance, I suspect they would have got their assurance by now, but if they go any further, then I hear what they say. MR KHAW: Certainly no hidden agenda whatsoever. I just
4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	very briefly? Obviously, what was said in the opening submissions has been accurately read out by Mr Khaw and I have no difficulty with that. But what we have here is a dynamic process, and I am bound to say that when I wrote that and I take full responsibility for it, of course I have to say I was completely unaware of where all this was going to lead. I had no idea of course that all of this ultimately might hinge on the question of whether or not this was a foundation or not a foundation and all of that. I had more in mind at the time that this was actually going into a potential project management issue as to how the MTR and Leighton on the one hand should have communicated with the government, was there a breakdown? It was more seen as a project management	3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	something had been sent but whether or not, on a fine legal construction, that amounted to a proper form of statutory application or consultation, that is a completely different kettle of fish and which we had suggested the Commission should stay away from. If what the government wants is some assurance that this is not what the terms of reference require and not what the Commission is going to get into, I hope and I think the government has its answer. But if what the government now wants is to positively press for it, then I would respectfully suggest some underlying agenda which is unknown to us. In other words, if they want assurance, I suspect they would have got their assurance by now, but if they go any further, then I hear what they say. MR KHAW: Certainly no hidden agenda whatsoever. I just want to make myself clear, Mr Chairman and
4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	very briefly? Obviously, what was said in the opening submissions has been accurately read out by Mr Khaw and I have no difficulty with that. But what we have here is a dynamic process, and I am bound to say that when I wrote that and I take full responsibility for it, of course I have to say I was completely unaware of where all this was going to lead. I had no idea of course that all of this ultimately might hinge on the question of whether or not this was a foundation or not a foundation and all of that. I had more in mind at the time that this was actually going into a potential project management issue as to how the MTR and Leighton on the one hand should have communicated with the government, was there a breakdown? It was more seen as a project management issue than a technical issue, if you like, that it seems	3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	<ul> <li>something had been sent but whether or not, on a fine legal construction, that amounted to a proper form of statutory application or consultation, that is</li> <li>a completely different kettle of fish and which we had suggested the Commission should stay away from. If what the government wants is some assurance that this is not what the terms of reference require and not what the Commission is going to get into, I hope and I think the government has its answer. But if what the government now wants is to positively press for it, then I would respectfully suggest some underlying agenda which is unknown to us. In other words, if they want assurance, I suspect they would have got their assurance by now, but if they go any further, then I hear what they say.</li> <li>MR KHAW: Certainly no hidden agenda whatsoever. I just want to make myself clear, Mr Chairman and Mr Commissioner. My point is simply this. I'm not</li> </ul>
4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	very briefly? Obviously, what was said in the opening submissions has been accurately read out by Mr Khaw and I have no difficulty with that. But what we have here is a dynamic process, and I am bound to say that when I wrote that and I take full responsibility for it, of course I have to say I was completely unaware of where all this was going to lead. I had no idea of course that all of this ultimately might hinge on the question of whether or not this was a foundation or not a foundation and all of that. I had more in mind at the time that this was actually going into a potential project management issue as to how the MTR and Leighton on the one hand should have communicated with the government, was there a breakdown? It was more seen as a project management issue than a technical issue, if you like, that it seems to have turned into.	3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	<ul> <li>something had been sent but whether or not, on a fine legal construction, that amounted to a proper form of statutory application or consultation, that is</li> <li>a completely different kettle of fish and which we had suggested the Commission should stay away from.</li> <li>If what the government wants is some assurance that this is not what the terms of reference require and not what the Commission is going to get into, I hope and I think the government has its answer.</li> <li>But if what the government now wants is to positively press for it, then I would respectfully suggest some underlying agenda which is unknown to us. In other words, if they want assurance, I suspect they would have got their assurance by now, but if they go any further, then I hear what they say.</li> <li>MR KHAW: Certainly no hidden agenda whatsoever. I just want to make myself clear, Mr Chairman and Mr Commissioner. My point is simply this. I'm not trying to encourage anyone in fact to really labour this</li> </ul>
4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>very briefly?</li> <li>Obviously, what was said in the opening submissions has been accurately read out by Mr Khaw and I have no difficulty with that. But what we have here is a dynamic process, and I am bound to say that when I wrote that and I take full responsibility for it, of course I have to say I was completely unaware of where all this was going to lead. I had no idea of course that all of this ultimately might hinge on the question of whether or not this was a foundation or not a foundation and all of that.</li> <li>I had more in mind at the time that this was actually going into a potential project management issue as to how the MTR and Leighton on the one hand should have communicated with the government, was there a breakdown? It was more seen as a project management issue than a technical issue, if you like, that it seems to have turned into.</li> <li>So, in defence of myself, if I can say so,</li> </ul>	3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	<ul> <li>something had been sent but whether or not, on a fine legal construction, that amounted to a proper form of statutory application or consultation, that is</li> <li>a completely different kettle of fish and which we had suggested the Commission should stay away from.</li> <li>If what the government wants is some assurance that this is not what the terms of reference require and not what the Commission is going to get into, I hope and I think the government has its answer.</li> <li>But if what the government now wants is to positively press for it, then I would respectfully suggest some underlying agenda which is unknown to us. In other words, if they want assurance, I suspect they would have got their assurance by now, but if they go any further, then I hear what they say.</li> <li>MR KHAW: Certainly no hidden agenda whatsoever. I just want to make myself clear, Mr Chairman and Mr Commissioner. My point is simply this. I'm not trying to encourage anyone in fact to really labour this point. This is certainly not my intention. I only</li> </ul>
4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	<ul> <li>very briefly?</li> <li>Obviously, what was said in the opening submissions has been accurately read out by Mr Khaw and I have no difficulty with that. But what we have here is a dynamic process, and I am bound to say that when I wrote that and I take full responsibility for it, of course I have to say I was completely unaware of where all this was going to lead. I had no idea of course that all of this ultimately might hinge on the question of whether or not this was a foundation or not a foundation and all of that.</li> <li>I had more in mind at the time that this was actually going into a potential project management issue as to how the MTR and Leighton on the one hand should have communicated with the government, was there a breakdown? It was more seen as a project management issue than a technical issue, if you like, that it seems to have turned into.</li> <li>So, in defence of myself, if I can say so, I honestly didn't understand the technicalities that</li> </ul>	3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	<ul> <li>something had been sent but whether or not, on a fine legal construction, that amounted to a proper form of statutory application or consultation, that is</li> <li>a completely different kettle of fish and which we had suggested the Commission should stay away from.</li> <li>If what the government wants is some assurance that this is not what the terms of reference require and not what the Commission is going to get into, I hope and I think the government has its answer.</li> <li>But if what the government now wants is to positively press for it, then I would respectfully suggest some underlying agenda which is unknown to us. In other words, if they want assurance, I suspect they would have got their assurance by now, but if they go any further, then I hear what they say.</li> <li>MR KHAW: Certainly no hidden agenda whatsoever. I just want to make myself clear, Mr Chairman and Mr Commissioner. My point is simply this. I'm not trying to encourage anyone in fact to really labour this</li> </ul>
4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>very briefly?</li> <li>Obviously, what was said in the opening submissions has been accurately read out by Mr Khaw and I have no difficulty with that. But what we have here is a dynamic process, and I am bound to say that when I wrote that and I take full responsibility for it, of course I have to say I was completely unaware of where all this was going to lead. I had no idea of course that all of this ultimately might hinge on the question of whether or not this was a foundation or not a foundation and all of that.</li> <li>I had more in mind at the time that this was actually going into a potential project management issue as to how the MTR and Leighton on the one hand should have communicated with the government, was there a breakdown? It was more seen as a project management issue than a technical issue, if you like, that it seems to have turned into.</li> <li>So, in defence of myself, if I can say so,</li> </ul>	3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>something had been sent but whether or not, on a fine legal construction, that amounted to a proper form of statutory application or consultation, that is</li> <li>a completely different kettle of fish and which we had suggested the Commission should stay away from.</li> <li>If what the government wants is some assurance that this is not what the terms of reference require and not what the Commission is going to get into, I hope and I think the government has its answer.</li> <li>But if what the government now wants is to positively press for it, then I would respectfully suggest some underlying agenda which is unknown to us. In other words, if they want assurance, I suspect they would have got their assurance by now, but if they go any further, then I hear what they say.</li> <li>MR KHAW: Certainly no hidden agenda whatsoever. I just want to make myself clear, Mr Chairman and Mr Commissioner. My point is simply this. I'm not trying to encourage anyone in fact to really labour this point. This is certainly not my intention. I only</li> </ul>

1	Page 73		Page 75
	government's stance that we need to have	1	CHAIRMAN: Good. Can I also just say I appreciate that
1	an interpretation on this PNAP no. 19. In fact we never	2	parties have in the past and will continue to do so,
2	•		* *
3	raised it in the first place. It is Leighton who tried	3	that they will look to what may have been said for counsel for the Commission at the outset. That's quite
4	to convince the Commission that they did not need to	4	
5	report this change to the Buildings Department, ie they	5	proper. There's no criticism at all. However, unlike
6	rely on this practice note to say it's not necessary.	6	litigation of the classic kind, where the chess pieces
7	That is why this interpretation of the practice note	7	are set up ready to be moved that's why whenever you
8	came into being. It was never the government's case	8	take a civil case to court, it takes you so long,
9	that this was relevant.	9	because the pleadings have to be prepared with
10	But since Leighton has raised this point, we have to	10	a Commission of Inquiry which commences within a much
11	meet this case by doing an interpretation on the	11	more limited scope of time, the chess pieces make their
12	practice note in relation to this narrow part regarding	12	own way onto the stage, bit by bit. It's a much more
13	the classification of the structure.	13	fluid, a much more progressive process. It's
14	Of course, if it is now Mr Shieh's case that	14	an inquiry, and inquiries you have to follow your nose
15	Leighton is not going to run this argument, that "This	15	in many respects.
16	is a superstructure, not a foundation; we are not going	16	Good. So what Mr Pennicott's nose tells him at one
17	to rely on the interpretation of this PNAP no. 19", I'm	17	time, the combined olfactory wisdom of everybody may say
18	perfectly fine with that and we don't need to actually	18	shouldn't influence us at a later stage.
19	deal with this particular argument.	19	Good. Thank you very much.
20	But when we look at it, they actually have chosen to	20	MR SO: In that case, I wonder if Mr Chow would
21	raise this point again in their expert report.	21	CHAIRMAN: Yes, I was just waiting. I think Mr Chow was
22	I believe they still find it necessary to do so. That	22	having a brief final discussion with Mr Khaw.
23	is why, just as a matter of prudence, we would like to	23	MR CHOW: Prof Yeung, just before the break, I was going to
24	clarify this point, because if they are going to run	24	ask you you recall about the classification of the
25	this point and they are going to rely on the	25	station box structure; right? You recall that?
	Page 74		Page 76
	aloggification of the attracture and if Mr Charry is now		
1	classification of the structure, and if Mr Chow is now	1	A. I think we were talking about the diaphragm wall in
1 2	not given a chance to ask Prof Yeung this question, we	1 2	<ul> <li>A. I think we were talking about the diaphragm wall in particular.</li> </ul>
	not given a chance to ask Prof Yeung this question, we		
2	not given a chance to ask Prof Yeung this question, we may not have a complete picture regarding this narrow	2	particular.
2 3 4	not given a chance to ask Prof Yeung this question, we may not have a complete picture regarding this narrow point on classification. That is my only concern.	2 3	particular. Q. Yes. What I was going to say is that according to Mr Southward's expert report, having made reference to
2 3 4 5	not given a chance to ask Prof Yeung this question, we may not have a complete picture regarding this narrow point on classification. That is my only concern. CHAIRMAN: I think you can accept from us we have	2 3 4	particular. Q. Yes. What I was going to say is that according to Mr Southward's expert report, having made reference to a foundation analysis and design textbook, Mr Southward
2 3 4 5 6	not given a chance to ask Prof Yeung this question, we may not have a complete picture regarding this narrow point on classification. That is my only concern. CHAIRMAN: I think you can accept from us we have discussed this matter, so this is not	2 3 4 5	particular. Q. Yes. What I was going to say is that according to Mr Southward's expert report, having made reference to a foundation analysis and design textbook, Mr Southward takes the view that the station box in question should
2 3 4 5 6 7	<ul><li>not given a chance to ask Prof Yeung this question, we may not have a complete picture regarding this narrow point on classification. That is my only concern.</li><li>CHAIRMAN: I think you can accept from us we have discussed this matter, so this is not an off-the-shoulder answer to you; far from it, we've</li></ul>	2 3 4 5 6 7	<ul><li>particular.</li><li>Q. Yes. What I was going to say is that according to Mr Southward's expert report, having made reference to a foundation analysis and design textbook, Mr Southward takes the view that the station box in question should be treated as a superstructure. Do you agree?</li></ul>
2 3 4 5 6 7 8	not given a chance to ask Prof Yeung this question, we may not have a complete picture regarding this narrow point on classification. That is my only concern. CHAIRMAN: I think you can accept from us we have discussed this matter, so this is not an off-the-shoulder answer to you; far from it, we've discussed it on more than one occasion and we are of	2 3 4 5 6 7 8	<ul><li>particular.</li><li>Q. Yes. What I was going to say is that according to Mr Southward's expert report, having made reference to a foundation analysis and design textbook, Mr Southward takes the view that the station box in question should be treated as a superstructure. Do you agree?</li><li>A. I think that's not in his report. I think he's saying,</li></ul>
2 3 4 5 6 7 8 9	<ul> <li>not given a chance to ask Prof Yeung this question, we may not have a complete picture regarding this narrow point on classification. That is my only concern.</li> <li>CHAIRMAN: I think you can accept from us we have discussed this matter, so this is not an off-the-shoulder answer to you; far from it, we've discussed it on more than one occasion and we are of the view that it is not for this Commission to make</li> </ul>	2 3 4 5 6 7 8 9	<ul><li>particular.</li><li>Q. Yes. What I was going to say is that according to Mr Southward's expert report, having made reference to a foundation analysis and design textbook, Mr Southward takes the view that the station box in question should be treated as a superstructure. Do you agree?</li><li>A. I think that's not in his report. I think he's saying, if my recollection is correct, the diaphragm wall below</li></ul>
2 3 4 5 6 7 8 9 10	<ul> <li>not given a chance to ask Prof Yeung this question, we may not have a complete picture regarding this narrow point on classification. That is my only concern.</li> <li>CHAIRMAN: I think you can accept from us we have discussed this matter, so this is not an off-the-shoulder answer to you; far from it, we've discussed it on more than one occasion and we are of the view that it is not for this Commission to make a legal decision in this instance, which it would be, as</li> </ul>	2 3 4 5 6 7 8 9 10	<ul><li>particular.</li><li>Q. Yes. What I was going to say is that according to Mr Southward's expert report, having made reference to a foundation analysis and design textbook, Mr Southward takes the view that the station box in question should be treated as a superstructure. Do you agree?</li><li>A. I think that's not in his report. I think he's saying, if my recollection is correct, the diaphragm wall below the EWL slab is a foundation, but then above the EWL</li></ul>
2 3 4 5 6 7 8 9 10 11	<ul> <li>not given a chance to ask Prof Yeung this question, we may not have a complete picture regarding this narrow point on classification. That is my only concern.</li> <li>CHAIRMAN: I think you can accept from us we have discussed this matter, so this is not an off-the-shoulder answer to you; far from it, we've discussed it on more than one occasion and we are of the view that it is not for this Commission to make a legal decision in this instance, which it would be, as to whether the diaphragm walls in this particular</li> </ul>	2 3 4 5 6 7 8 9 10 11	<ul><li>particular.</li><li>Q. Yes. What I was going to say is that according to Mr Southward's expert report, having made reference to a foundation analysis and design textbook, Mr Southward takes the view that the station box in question should be treated as a superstructure. Do you agree?</li><li>A. I think that's not in his report. I think he's saying, if my recollection is correct, the diaphragm wall below the EWL slab is a foundation, but then above the EWL slab is not. I think that's what he said in his report.</li></ul>
2 3 4 5 6 7 8 9 10 11 12	<ul> <li>not given a chance to ask Prof Yeung this question, we may not have a complete picture regarding this narrow point on classification. That is my only concern.</li> <li>CHAIRMAN: I think you can accept from us we have discussed this matter, so this is not an off-the-shoulder answer to you; far from it, we've discussed it on more than one occasion and we are of the view that it is not for this Commission to make a legal decision in this instance, which it would be, as to whether the diaphragm walls in this particular structure constitute foundations in accordance with the</li> </ul>	2 3 4 5 6 7 8 9 10 11 12	<ul><li>particular.</li><li>Q. Yes. What I was going to say is that according to Mr Southward's expert report, having made reference to a foundation analysis and design textbook, Mr Southward takes the view that the station box in question should be treated as a superstructure. Do you agree?</li><li>A. I think that's not in his report. I think he's saying, if my recollection is correct, the diaphragm wall below the EWL slab is a foundation, but then above the EWL slab is not. I think that's what he said in his report. Correct me if I'm wrong.</li></ul>
2 3 4 5 6 7 8 9 10 11 12 13	<ul> <li>not given a chance to ask Prof Yeung this question, we may not have a complete picture regarding this narrow point on classification. That is my only concern.</li> <li>CHAIRMAN: I think you can accept from us we have discussed this matter, so this is not an off-the-shoulder answer to you; far from it, we've discussed it on more than one occasion and we are of the view that it is not for this Commission to make a legal decision in this instance, which it would be, as to whether the diaphragm walls in this particular structure constitute foundations in accordance with the prevailing regulations, statutes, bylaws, et cetera,</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13	<ul> <li>particular.</li> <li>Q. Yes. What I was going to say is that according to Mr Southward's expert report, having made reference to a foundation analysis and design textbook, Mr Southward takes the view that the station box in question should be treated as a superstructure. Do you agree?</li> <li>A. I think that's not in his report. I think he's saying, if my recollection is correct, the diaphragm wall below the EWL slab is a foundation, but then above the EWL slab is not. I think that's what he said in his report. Correct me if I'm wrong.</li> <li>Q. Yes. Perhaps it's easier for me to refer you to</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14	<ul> <li>not given a chance to ask Prof Yeung this question, we may not have a complete picture regarding this narrow point on classification. That is my only concern.</li> <li>CHAIRMAN: I think you can accept from us we have discussed this matter, so this is not an off-the-shoulder answer to you; far from it, we've discussed it on more than one occasion and we are of the view that it is not for this Commission to make a legal decision in this instance, which it would be, as to whether the diaphragm walls in this particular structure constitute foundations in accordance with the prevailing regulations, statutes, bylaws, et cetera, that prevail in Hong Kong.</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14	<ul> <li>particular.</li> <li>Q. Yes. What I was going to say is that according to Mr Southward's expert report, having made reference to a foundation analysis and design textbook, Mr Southward takes the view that the station box in question should be treated as a superstructure. Do you agree?</li> <li>A. I think that's not in his report. I think he's saying, if my recollection is correct, the diaphragm wall below the EWL slab is a foundation, but then above the EWL slab is not. I think that's what he said in his report. Correct me if I'm wrong.</li> <li>Q. Yes. Perhaps it's easier for me to refer you to a particular part of his report, section 14.2, page 40</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15	<ul> <li>not given a chance to ask Prof Yeung this question, we may not have a complete picture regarding this narrow point on classification. That is my only concern.</li> <li>CHAIRMAN: I think you can accept from us we have discussed this matter, so this is not an off-the-shoulder answer to you; far from it, we've discussed it on more than one occasion and we are of the view that it is not for this Commission to make a legal decision in this instance, which it would be, as to whether the diaphragm walls in this particular structure constitute foundations in accordance with the prevailing regulations, statutes, bylaws, et cetera, that prevail in Hong Kong.</li> <li>So, that said, it's clearly a very important issue</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15	<ul> <li>particular.</li> <li>Q. Yes. What I was going to say is that according to Mr Southward's expert report, having made reference to a foundation analysis and design textbook, Mr Southward takes the view that the station box in question should be treated as a superstructure. Do you agree?</li> <li>A. I think that's not in his report. I think he's saying, if my recollection is correct, the diaphragm wall below the EWL slab is a foundation, but then above the EWL slab is not. I think that's what he said in his report. Correct me if I'm wrong.</li> <li>Q. Yes. Perhaps it's easier for me to refer you to a particular part of his report, section 14.2, page 40 of Mr Southward's report.</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	<ul> <li>not given a chance to ask Prof Yeung this question, we may not have a complete picture regarding this narrow point on classification. That is my only concern.</li> <li>CHAIRMAN: I think you can accept from us we have discussed this matter, so this is not an off-the-shoulder answer to you; far from it, we've discussed it on more than one occasion and we are of the view that it is not for this Commission to make a legal decision in this instance, which it would be, as to whether the diaphragm walls in this particular structure constitute foundations in accordance with the prevailing regulations, statutes, bylaws, et cetera, that prevail in Hong Kong.</li> <li>So, that said, it's clearly a very important issue because it sets the scene and contains within its</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	<ul> <li>particular.</li> <li>Q. Yes. What I was going to say is that according to Mr Southward's expert report, having made reference to a foundation analysis and design textbook, Mr Southward takes the view that the station box in question should be treated as a superstructure. Do you agree?</li> <li>A. I think that's not in his report. I think he's saying, if my recollection is correct, the diaphragm wall below the EWL slab is a foundation, but then above the EWL slab is not. I think that's what he said in his report. Correct me if I'm wrong.</li> <li>Q. Yes. Perhaps it's easier for me to refer you to a particular part of his report, section 14.2, page 40 of Mr Southward's report.</li> <li>A. I think you are referring to page 41, internal page</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	<ul> <li>not given a chance to ask Prof Yeung this question, we may not have a complete picture regarding this narrow point on classification. That is my only concern.</li> <li>CHAIRMAN: I think you can accept from us we have discussed this matter, so this is not an off-the-shoulder answer to you; far from it, we've discussed it on more than one occasion and we are of the view that it is not for this Commission to make a legal decision in this instance, which it would be, as to whether the diaphragm walls in this particular structure constitute foundations in accordance with the prevailing regulations, statutes, bylaws, et cetera, that prevail in Hong Kong.</li> <li>So, that said, it's clearly a very important issue because it sets the scene and contains within its parameters the reason for a lot of dynamic happenings</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	<ul> <li>particular.</li> <li>Q. Yes. What I was going to say is that according to Mr Southward's expert report, having made reference to a foundation analysis and design textbook, Mr Southward takes the view that the station box in question should be treated as a superstructure. Do you agree?</li> <li>A. I think that's not in his report. I think he's saying, if my recollection is correct, the diaphragm wall below the EWL slab is a foundation, but then above the EWL slab is not. I think that's what he said in his report. Correct me if I'm wrong.</li> <li>Q. Yes. Perhaps it's easier for me to refer you to a particular part of his report, section 14.2, page 40 of Mr Southward's report.</li> <li>A. I think you are referring to page 41, internal page number.</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	<ul> <li>not given a chance to ask Prof Yeung this question, we may not have a complete picture regarding this narrow point on classification. That is my only concern.</li> <li>CHAIRMAN: I think you can accept from us we have discussed this matter, so this is not an off-the-shoulder answer to you; far from it, we've discussed it on more than one occasion and we are of the view that it is not for this Commission to make a legal decision in this instance, which it would be, as to whether the diaphragm walls in this particular structure constitute foundations in accordance with the prevailing regulations, statutes, bylaws, et cetera, that prevail in Hong Kong.</li> <li>So, that said, it's clearly a very important issue because it sets the scene and contains within its parameters the reason for a lot of dynamic happenings that have taken up the time. So we will expect from</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	<ul> <li>particular.</li> <li>Q. Yes. What I was going to say is that according to Mr Southward's expert report, having made reference to a foundation analysis and design textbook, Mr Southward takes the view that the station box in question should be treated as a superstructure. Do you agree?</li> <li>A. I think that's not in his report. I think he's saying, if my recollection is correct, the diaphragm wall below the EWL slab is a foundation, but then above the EWL slab is not. I think that's what he said in his report. Correct me if I'm wrong.</li> <li>Q. Yes. Perhaps it's easier for me to refer you to a particular part of his report, section 14.2, page 40 of Mr Southward's report.</li> <li>A. I think you are referring to page 41, internal page number.</li> <li>Q. Page 41 is the figure, the figure 13 referred to by</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	<ul> <li>not given a chance to ask Prof Yeung this question, we may not have a complete picture regarding this narrow point on classification. That is my only concern.</li> <li>CHAIRMAN: I think you can accept from us we have discussed this matter, so this is not <ul> <li>an off-the-shoulder answer to you; far from it, we've</li> <li>discussed it on more than one occasion and we are of the view that it is not for this Commission to make</li> <li>a legal decision in this instance, which it would be, as to whether the diaphragm walls in this particular structure constitute foundations in accordance with the prevailing regulations, statutes, bylaws, et cetera, that prevail in Hong Kong.</li> <li>So, that said, it's clearly a very important issue because it sets the scene and contains within its parameters the reason for a lot of dynamic happenings that have taken up the time. So we will expect from parties who believe it's relevant to their case that the</li> </ul> </li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	<ul> <li>particular.</li> <li>Q. Yes. What I was going to say is that according to Mr Southward's expert report, having made reference to a foundation analysis and design textbook, Mr Southward takes the view that the station box in question should be treated as a superstructure. Do you agree?</li> <li>A. I think that's not in his report. I think he's saying, if my recollection is correct, the diaphragm wall below the EWL slab is a foundation, but then above the EWL slab is not. I think that's what he said in his report. Correct me if I'm wrong.</li> <li>Q. Yes. Perhaps it's easier for me to refer you to a particular part of his report, section 14.2, page 40 of Mr Southward's report.</li> <li>A. I think you are referring to page 41, internal page number.</li> <li>Q. Page 41 is the figure, the figure 13 referred to by Mr Southward on page 40. In page 40, under</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	<ul> <li>not given a chance to ask Prof Yeung this question, we may not have a complete picture regarding this narrow point on classification. That is my only concern.</li> <li>CHAIRMAN: I think you can accept from us we have discussed this matter, so this is not an off-the-shoulder answer to you; far from it, we've discussed it on more than one occasion and we are of the view that it is not for this Commission to make a legal decision in this instance, which it would be, as to whether the diaphragm walls in this particular structure constitute foundations in accordance with the prevailing regulations, statutes, bylaws, et cetera, that prevail in Hong Kong.</li> <li>So, that said, it's clearly a very important issue because it sets the scene and contains within its parameters the reason for a lot of dynamic happenings that have taken up the time. So we will expect from parties who believe it's relevant to their case that the issues should be there, but we will not, at the end of</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	<ul> <li>particular.</li> <li>Q. Yes. What I was going to say is that according to Mr Southward's expert report, having made reference to a foundation analysis and design textbook, Mr Southward takes the view that the station box in question should be treated as a superstructure. Do you agree?</li> <li>A. I think that's not in his report. I think he's saying, if my recollection is correct, the diaphragm wall below the EWL slab is a foundation, but then above the EWL slab is not. I think that's what he said in his report. Correct me if I'm wrong.</li> <li>Q. Yes. Perhaps it's easier for me to refer you to a particular part of his report, section 14.2, page 40 of Mr Southward's report.</li> <li>A. I think you are referring to page 41, internal page number.</li> <li>Q. Page 41 is the figure, the figure 13 referred to by Mr Southward on page 40. In page 40, under section 14.2</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	<ul> <li>not given a chance to ask Prof Yeung this question, we may not have a complete picture regarding this narrow point on classification. That is my only concern.</li> <li>CHAIRMAN: I think you can accept from us we have discussed this matter, so this is not an off-the-shoulder answer to you; far from it, we've discussed it on more than one occasion and we are of the view that it is not for this Commission to make a legal decision in this instance, which it would be, as to whether the diaphragm walls in this particular structure constitute foundations in accordance with the prevailing regulations, statutes, bylaws, et cetera, that prevail in Hong Kong.</li> <li>So, that said, it's clearly a very important issue because it sets the scene and contains within its parameters the reason for a lot of dynamic happenings that have taken up the time. So we will expect from parties who believe it's relevant to their case that the issues should be there, but we will not, at the end of the day, make a decision on that limited legal point of</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	<ul> <li>particular.</li> <li>Q. Yes. What I was going to say is that according to Mr Southward's expert report, having made reference to a foundation analysis and design textbook, Mr Southward takes the view that the station box in question should be treated as a superstructure. Do you agree?</li> <li>A. I think that's not in his report. I think he's saying, if my recollection is correct, the diaphragm wall below the EWL slab is a foundation, but then above the EWL slab is not. I think that's what he said in his report. Correct me if I'm wrong.</li> <li>Q. Yes. Perhaps it's easier for me to refer you to a particular part of his report, section 14.2, page 40 of Mr Southward's report.</li> <li>A. I think you are referring to page 41, internal page number.</li> <li>Q. Page 41 is the figure, the figure 13 referred to by Mr Southward on page 40. In page 40, under section 14.2</li> <li>A. Yes.</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>not given a chance to ask Prof Yeung this question, we may not have a complete picture regarding this narrow point on classification. That is my only concern.</li> <li>CHAIRMAN: I think you can accept from us we have discussed this matter, so this is not</li> <li>an off-the-shoulder answer to you; far from it, we've discussed it on more than one occasion and we are of the view that it is not for this Commission to make</li> <li>a legal decision in this instance, which it would be, as to whether the diaphragm walls in this particular structure constitute foundations in accordance with the prevailing regulations, statutes, bylaws, et cetera, that prevail in Hong Kong.</li> <li>So, that said, it's clearly a very important issue because it sets the scene and contains within its parameters the reason for a lot of dynamic happenings that have taken up the time. So we will expect from parties who believe it's relevant to their case that the issues should be there, but we will not, at the end of the day, make a decision on that limited legal point of whether the diaphragm walls in this structure constitute</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>particular.</li> <li>Q. Yes. What I was going to say is that according to Mr Southward's expert report, having made reference to a foundation analysis and design textbook, Mr Southward takes the view that the station box in question should be treated as a superstructure. Do you agree?</li> <li>A. I think that's not in his report. I think he's saying, if my recollection is correct, the diaphragm wall below the EWL slab is a foundation, but then above the EWL slab is not. I think that's what he said in his report. Correct me if I'm wrong.</li> <li>Q. Yes. Perhaps it's easier for me to refer you to a particular part of his report, section 14.2, page 40 of Mr Southward's report.</li> <li>A. I think you are referring to page 41, internal page number.</li> <li>Q. Page 41 is the figure, the figure 13 referred to by Mr Southward on page 40. In page 40, under section 14.2</li> <li>A. Yes.</li> <li>Q Mr Southward refers to a foundation analysis and</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	<ul> <li>not given a chance to ask Prof Yeung this question, we may not have a complete picture regarding this narrow point on classification. That is my only concern.</li> <li>CHAIRMAN: I think you can accept from us we have discussed this matter, so this is not <ul> <li>an off-the-shoulder answer to you; far from it, we've</li> <li>discussed it on more than one occasion and we are of the view that it is not for this Commission to make</li> <li>a legal decision in this instance, which it would be, as to whether the diaphragm walls in this particular</li> <li>structure constitute foundations in accordance with the prevailing regulations, statutes, bylaws, et cetera, that prevail in Hong Kong.</li> <li>So, that said, it's clearly a very important issue</li> <li>because it sets the scene and contains within its</li> <li>parameters the reason for a lot of dynamic happenings</li> <li>that have taken up the time. So we will expect from parties who believe it's relevant to their case that the issues should be there, but we will not, at the end of the day, make a decision on that limited legal point of whether the diaphragm walls in this structure constitute foundations in accordance with the law of Hong Kong.</li> </ul> </li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	<ul> <li>particular.</li> <li>Q. Yes. What I was going to say is that according to Mr Southward's expert report, having made reference to a foundation analysis and design textbook, Mr Southward takes the view that the station box in question should be treated as a superstructure. Do you agree?</li> <li>A. I think that's not in his report. I think he's saying, if my recollection is correct, the diaphragm wall below the EWL slab is a foundation, but then above the EWL slab is not. I think that's what he said in his report. Correct me if I'm wrong.</li> <li>Q. Yes. Perhaps it's easier for me to refer you to a particular part of his report, section 14.2, page 40 of Mr Southward's report.</li> <li>A. I think you are referring to page 41, internal page number.</li> <li>Q. Page 41 is the figure, the figure 13 referred to by Mr Southward on page 40. In page 40, under section 14.2</li> <li>A. Yes.</li> <li>Q Mr Southward refers to a foundation analysis and design textbook, and in particular he refers to</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>not given a chance to ask Prof Yeung this question, we may not have a complete picture regarding this narrow point on classification. That is my only concern.</li> <li>CHAIRMAN: I think you can accept from us we have discussed this matter, so this is not</li> <li>an off-the-shoulder answer to you; far from it, we've discussed it on more than one occasion and we are of the view that it is not for this Commission to make</li> <li>a legal decision in this instance, which it would be, as to whether the diaphragm walls in this particular structure constitute foundations in accordance with the prevailing regulations, statutes, bylaws, et cetera, that prevail in Hong Kong.</li> <li>So, that said, it's clearly a very important issue because it sets the scene and contains within its parameters the reason for a lot of dynamic happenings that have taken up the time. So we will expect from parties who believe it's relevant to their case that the issues should be there, but we will not, at the end of the day, make a decision on that limited legal point of whether the diaphragm walls in this structure constitute</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>particular.</li> <li>Q. Yes. What I was going to say is that according to Mr Southward's expert report, having made reference to a foundation analysis and design textbook, Mr Southward takes the view that the station box in question should be treated as a superstructure. Do you agree?</li> <li>A. I think that's not in his report. I think he's saying, if my recollection is correct, the diaphragm wall below the EWL slab is a foundation, but then above the EWL slab is not. I think that's what he said in his report. Correct me if I'm wrong.</li> <li>Q. Yes. Perhaps it's easier for me to refer you to a particular part of his report, section 14.2, page 40 of Mr Southward's report.</li> <li>A. I think you are referring to page 41, internal page number.</li> <li>Q. Page 41 is the figure, the figure 13 referred to by Mr Southward on page 40. In page 40, under section 14.2</li> <li>A. Yes.</li> <li>Q Mr Southward refers to a foundation analysis and</li> </ul>

	Page 77		Page 79
1	which transmits to, and into, the underlying soil or	1	going to often find areas where highly respected experts
2	rock the loads supported by the foundation and its	2	may agree on definition, or may disagree on definition?
3	self-weight."	3	A. Not frequently.
4	Then he goes on to refer to the Code of Practice for	4	CHAIRMAN: No, but when you've got an in-depth investigation
5	Foundations 2017, which provides:	5	of this kind, you may find that happening?
6	"Foundation. That part of a building, building	6	A. I have seldom see for one structural member get two
7	works, structure or street in direct contact with and	7	definitions, because diaphragm wall is one single entity
8	transmitting loads to the ground.'	8	and it was actually built in one piece.
9	The term diaphragm wall is explained by the	9	CHAIRMAN: Okay. Fine. Thank you very much.
10	Buildings Department in the same publication as follows:	10	MR SO: Thank you, sir.
11	'A diaphragm wall may be used as a temporary lateral	11	Professor, I have two topics that I wish to discuss
12	support wall for deep excavation or the permanent wall	12	with you. The first one is arising out of a discussion
13	of a basement, or it may be designed for both temporary	13	you had between yourself and Prof Hansford this morning
14	and permanent uses. It may also be used to support	14	about the engagement length and embedment length issue.
15	vertical loads."	15	Prof Yeung, I heard that you told us in your answers
16	Then Mr Southward continues to say:	16	to Prof Hansford that the current tests could only
17	"In the context of the SCL1112 station box	17	measure the engagement length but not the embedment
18	structure"	18	length
19	Now, the station box structure is the one that you	19	A. No, it's the other way around.
20	were just pointing out to us, figure 13, turn over the	20	Q. The other way around. Only the embedment length but not
21	page, it's the part comprising the ground, EWL slab, the	21	the engagement length. Can you tell us why this is so?
22	purple NSL slab and the section of diaphragm wall in	22	A. The technique we are using is actually sending
23	between the two slabs, as the station box structure.	23	an ultrasound wave into the bar. And then when the wave
24	In the penultimate paragraph, Mr Southward	24	hits the end of the bar, it gets reflected back, and
25	concluded:	25	then by measuring the length of time it takes, we know
	Page 78		Page 80
1	"This element of the overall structure should be	1	where the end of the bar is. That's why we call it
2	termed the superstructure."	2	embedment length.
3	Do you see that?	3	In between are all the threads and the threads are
4	A. Yes.	4	engaged to the coupler. So this thread doesn't tell us
5	Q. Do you agree with his conclusion?	5	how many threads are engaged. So we are trying to make
6	A. No, I don't.	6	a deduction now is: if we know where the end of the bar
7	Q. How would you classify this part of the station box	_	
8	Q. How would you classify this part of the station box	7	is and try to make that to deduce how many threads
	structure?	7 8	is and try to make that to deduce how many threads are within that section.
9			-
9 10	structure?	8	are within that section.
	structure? A. If you look at the structure itself, the weight or the	8 9	are within that section. COMMISSIONER HANSFORD: Forgive me, because I'm quite keen
10	structure? A. If you look at the structure itself, the weight or the load on the EWL slab will be transmitted to that part of	8 9 10	are within that section. COMMISSIONER HANSFORD: Forgive me, because I'm quite keen to understand this point.
10 11	structure? A. If you look at the structure itself, the weight or the load on the EWL slab will be transmitted to that part of the diaphragm wall, and through that diaphragm wall it	8 9 10 11	are within that section. COMMISSIONER HANSFORD: Forgive me, because I'm quite keen to understand this point. MR SO: Sure.
10 11 12	structure? A. If you look at the structure itself, the weight or the load on the EWL slab will be transmitted to that part of the diaphragm wall, and through that diaphragm wall it will transmit the load to the ground. So if you look at	8 9 10 11 12	are within that section. COMMISSIONER HANSFORD: Forgive me, because I'm quite keen to understand this point. MR SO: Sure. COMMISSIONER HANSFORD: So in your view the difference
10 11 12 13	structure? A. If you look at the structure itself, the weight or the load on the EWL slab will be transmitted to that part of the diaphragm wall, and through that diaphragm wall it will transmit the load to the ground. So if you look at all the definitions, that remains a foundation.	8 9 10 11 12 13	are within that section. COMMISSIONER HANSFORD: Forgive me, because I'm quite keen to understand this point. MR SO: Sure. COMMISSIONER HANSFORD: So in your view the difference between the embedment length and the engagement length
10 11 12 13 14	structure? A. If you look at the structure itself, the weight or the load on the EWL slab will be transmitted to that part of the diaphragm wall, and through that diaphragm wall it will transmit the load to the ground. So if you look at all the definitions, that remains a foundation. The second thing is you also see from the figure,	8 9 10 11 12 13 14	<ul><li>are within that section.</li><li>COMMISSIONER HANSFORD: Forgive me, because I'm quite keen to understand this point.</li><li>MR SO: Sure.</li><li>COMMISSIONER HANSFORD: So in your view the difference between the embedment length and the engagement length is the chamfer; is that correct?</li></ul>
10 11 12 13 14 15	structure? A. If you look at the structure itself, the weight or the load on the EWL slab will be transmitted to that part of the diaphragm wall, and through that diaphragm wall it will transmit the load to the ground. So if you look at all the definitions, that remains a foundation. The second thing is you also see from the figure, you see the ground level. So that part, the whole box,	8 9 10 11 12 13 14 15	<ul> <li>are within that section.</li> <li>COMMISSIONER HANSFORD: Forgive me, because I'm quite keen to understand this point.</li> <li>MR SO: Sure.</li> <li>COMMISSIONER HANSFORD: So in your view the difference between the embedment length and the engagement length is the chamfer; is that correct?</li> <li>A. In this case, yes.</li> </ul>
10 11 12 13 14 15 16	<ul><li>structure?</li><li>A. If you look at the structure itself, the weight or the load on the EWL slab will be transmitted to that part of the diaphragm wall, and through that diaphragm wall it will transmit the load to the ground. So if you look at all the definitions, that remains a foundation. The second thing is you also see from the figure, you see the ground level. So that part, the whole box, is underground, so it cannot be called "superstructure".</li></ul>	8 9 10 11 12 13 14 15 16	<ul> <li>are within that section.</li> <li>COMMISSIONER HANSFORD: Forgive me, because I'm quite keer to understand this point.</li> <li>MR SO: Sure.</li> <li>COMMISSIONER HANSFORD: So in your view the difference between the embedment length and the engagement length is the chamfer; is that correct?</li> <li>A. In this case, yes.</li> <li>COMMISSIONER HANSFORD: And the chamfer, I think we said</li> </ul>
10 11 12 13 14 15 16 17	<ul> <li>structure?</li> <li>A. If you look at the structure itself, the weight or the load on the EWL slab will be transmitted to that part of the diaphragm wall, and through that diaphragm wall it will transmit the load to the ground. So if you look at all the definitions, that remains a foundation.</li> <li>The second thing is you also see from the figure, you see the ground level. So that part, the whole box, is underground, so it cannot be called "superstructure".</li> <li>Q. So how would you describe it, foundation or substructure</li> </ul>	8 9 10 11 12 13 14 15 16 17	<ul> <li>are within that section.</li> <li>COMMISSIONER HANSFORD: Forgive me, because I'm quite keen to understand this point.</li> <li>MR SO: Sure.</li> <li>COMMISSIONER HANSFORD: So in your view the difference between the embedment length and the engagement length is the chamfer; is that correct?</li> <li>A. In this case, yes.</li> <li>COMMISSIONER HANSFORD: And the chamfer, I think we said yesterday, was a maximum of 2 millimetres?</li> </ul>
10 11 12 13 14 15 16 17 18	<ul> <li>structure?</li> <li>A. If you look at the structure itself, the weight or the load on the EWL slab will be transmitted to that part of the diaphragm wall, and through that diaphragm wall it will transmit the load to the ground. So if you look at all the definitions, that remains a foundation. The second thing is you also see from the figure, you see the ground level. So that part, the whole box, is underground, so it cannot be called "superstructure". Q. So how would you describe it, foundation or substructure or whatever, something else?</li></ul>	8 9 10 11 12 13 14 15 16 17 18	<ul> <li>are within that section.</li> <li>COMMISSIONER HANSFORD: Forgive me, because I'm quite keer to understand this point.</li> <li>MR SO: Sure.</li> <li>COMMISSIONER HANSFORD: So in your view the difference between the embedment length and the engagement length is the chamfer; is that correct?</li> <li>A. In this case, yes.</li> <li>COMMISSIONER HANSFORD: And the chamfer, I think we said yesterday, was a maximum of 2 millimetres?</li> <li>A. Correct.</li> </ul>
10 11 12 13 14 15 16 17 18 19	<ul> <li>structure?</li> <li>A. If you look at the structure itself, the weight or the load on the EWL slab will be transmitted to that part of the diaphragm wall, and through that diaphragm wall it will transmit the load to the ground. So if you look at all the definitions, that remains a foundation. The second thing is you also see from the figure, you see the ground level. So that part, the whole box, is underground, so it cannot be called "superstructure".</li> <li>Q. So how would you describe it, foundation or substructure or whatever, something else?</li> <li>A. I will call this a foundation.</li> </ul>	8 9 10 11 12 13 14 15 16 17 18 19	<ul> <li>are within that section.</li> <li>COMMISSIONER HANSFORD: Forgive me, because I'm quite keer to understand this point.</li> <li>MR SO: Sure.</li> <li>COMMISSIONER HANSFORD: So in your view the difference between the embedment length and the engagement length is the chamfer; is that correct?</li> <li>A. In this case, yes.</li> <li>COMMISSIONER HANSFORD: And the chamfer, I think we said yesterday, was a maximum of 2 millimetres?</li> <li>A. Correct.</li> <li>COMMISSIONER HANSFORD: So therefore, in your view, the</li> </ul>
10 11 12 13 14 15 16 17 18 19 20	<ul> <li>structure?</li> <li>A. If you look at the structure itself, the weight or the load on the EWL slab will be transmitted to that part of the diaphragm wall, and through that diaphragm wall it will transmit the load to the ground. So if you look at all the definitions, that remains a foundation. The second thing is you also see from the figure, you see the ground level. So that part, the whole box, is underground, so it cannot be called "superstructure".</li> <li>Q. So how would you describe it, foundation or substructure or whatever, something else?</li> <li>A. I will call this a foundation.</li> </ul>	8 9 10 11 12 13 14 15 16 17 18 19 20	<ul> <li>are within that section.</li> <li>COMMISSIONER HANSFORD: Forgive me, because I'm quite keer to understand this point.</li> <li>MR SO: Sure.</li> <li>COMMISSIONER HANSFORD: So in your view the difference between the embedment length and the engagement length is the chamfer; is that correct?</li> <li>A. In this case, yes.</li> <li>COMMISSIONER HANSFORD: And the chamfer, I think we said yesterday, was a maximum of 2 millimetres?</li> <li>A. Correct.</li> <li>COMMISSIONER HANSFORD: So therefore, in your view, the engagement is 2 millimetres short of the embedment</li> </ul>
10 11 12 13 14 15 16 17 18 19 20 21	<ul> <li>structure?</li> <li>A. If you look at the structure itself, the weight or the load on the EWL slab will be transmitted to that part of the diaphragm wall, and through that diaphragm wall it will transmit the load to the ground. So if you look at all the definitions, that remains a foundation. The second thing is you also see from the figure, you see the ground level. So that part, the whole box, is underground, so it cannot be called "superstructure". Q. So how would you describe it, foundation or substructure or whatever, something else? A. I will call this a foundation. MR CHOW: Thank you, Prof Yeung. I have no more questions Re-examination by MR SO</li></ul>	8 9 10 11 12 13 14 15 16 17 18 19 20 21	<ul> <li>are within that section.</li> <li>COMMISSIONER HANSFORD: Forgive me, because I'm quite keer to understand this point.</li> <li>MR SO: Sure.</li> <li>COMMISSIONER HANSFORD: So in your view the difference between the embedment length and the engagement length is the chamfer; is that correct?</li> <li>A. In this case, yes.</li> <li>COMMISSIONER HANSFORD: And the chamfer, I think we said yesterday, was a maximum of 2 millimetres?</li> <li>A. Correct.</li> <li>COMMISSIONER HANSFORD: So therefore, in your view, the engagement is 2 millimetres short of the embedment length?</li> </ul>
10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>structure?</li> <li>A. If you look at the structure itself, the weight or the load on the EWL slab will be transmitted to that part of the diaphragm wall, and through that diaphragm wall it will transmit the load to the ground. So if you look at all the definitions, that remains a foundation. The second thing is you also see from the figure, you see the ground level. So that part, the whole box, is underground, so it cannot be called "superstructure".</li> <li>Q. So how would you describe it, foundation or substructure or whatever, something else?</li> <li>A. I will call this a foundation.</li> <li>MR CHOW: Thank you, Prof Yeung. I have no more questions. Re-examination by MR SO</li> <li>MR SO: Prof Yeung, I have two topics</li> </ul>	8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>are within that section.</li> <li>COMMISSIONER HANSFORD: Forgive me, because I'm quite keer to understand this point.</li> <li>MR SO: Sure.</li> <li>COMMISSIONER HANSFORD: So in your view the difference between the embedment length and the engagement length is the chamfer; is that correct?</li> <li>A. In this case, yes.</li> <li>COMMISSIONER HANSFORD: And the chamfer, I think we said yesterday, was a maximum of 2 millimetres?</li> <li>A. Correct.</li> <li>COMMISSIONER HANSFORD: So therefore, in your view, the engagement is 2 millimetres short of the embedment length?</li> <li>A. At most.</li> </ul>

	Page 81		Page 83
1	helped to resolve that matter.	1	sentence you have told us so if the parent bar is
2	I will move to the second topic I wish to discuss	2	48mm, so by a simple calculation we would know the
3	with you. The second topic is arising out of your	3	remaining bar would be 40mm only into the coupler?
4	discussion with the learned Chairman this morning.	4	A. Correct.
5	There was a lot of debate between yourself with other	5	Q. So if it takes up to 48mm in the other bar, then it will
6	counsel as to the definition of "butt-to-butt" and the	6	be at most two pitches; is that what you are trying to
7	stipulation where BOSA said there would be a tolerance	7	say?
8	of maximum up to two threads.	8	A. That is if both bars are at the maximum tolerance.
9	A. Yes.	9	Q. Thank you very much.
10	Q. I remember this morning when you were trying to explain	10	I would like to bring you to page OU135. I believe
11	the mechanism, you want to give us some examples and the	11	this is the up-to-date opening-up result.
12	details of that.	12	MR PENNICOTT: The very latest is 338.
13	A. Mm-hmm.	12	MR SO: I heard it was 338. I'm not sure which is the most
14	Q. I understand that the secretary has kindly prepared	13	updated one.
14	a pen next to yourself. Can you try to help us		MR PENNICOTT: 338.
16		15	
	demonstrate graphically why butt-to-butt would be	16	MR SO: Thank you. This is the 15 January opening-up
17 18	equivalent to what you have told us to be the two-thread tolerance?	17	result. Can I bring you to the last page of it.
		18	A. So this is 352 then.
19	A. Okay.	19	MR PENNICOTT: The last page.
20	COMMISSIONER HANSFORD: I think you will need the microphon		MR SO: Yes. Thank you.
21	with you.	21	In my examination-in-chief, and of course it was
22	A. Let me draw it first.	22	also cross-examined by Mr Pennicott on this topic,
23	COMMISSIONER HANSFORD: Okay.	23	regarding the opening-up results, you were asked by
24	A. (Drawing on the whiteboard) So what I draw here is on	24	Mr Pennicott and also by Mr Paul Shieh, if the standard
25	the top will be the type A bar. The type A bar was	25	was changed, then the opening-up results would be
	Page 82		Page 84
1	designed to be the threaded section, by design it's	1	different in terms of the failure rate.
2	44mm. In real-life construction or manufacturing,	2	Do you remember that exchange you had with
3	there's no way we can make it exactly 44 all the time.	3	Mr Pennicott yesterday?
4	That's why, in engineering, we have something we call	4	A. I think we are talking about the acceptance criteria.
5	the tolerance. And by the design of BOSA, BOSA make the	5	Q. Exactly. So, with your after your oral synopsis and
6	tolerance, they make sure that the threaded length is	6	with your criteria that you have proposed to this
7	always greater than 44. Their tolerance didn't allow	7	Commission, can you tell us what is the percentage of
8	anything to be less than 44. Then this tolerance, they	8	the failure rate, if using your standard?
9	allow it to be the maximum would be 4mm.	9	A. So that means we start to count all the numbers here?
10	So that threaded section will be from 44 to 48, in	10	Q. I think we have the total numbers at the end. There are
11	reality. Then the coupler itself will be 88mm.	11	altogether 75.
12	So what it shows on that picture is if the two bar	12	A. 75, okay. Can it come down a little bit?
13	that we try to put in, both the parent bar and the	13	Q. Maybe you can be given a hard copy. I think that would
14	continuation bar, if they are both 44, so both will get	14	be more convenient for you to count.
15	in and they butt-to-butt, 44 plus 44 equal to 88. On	15	A. The hard copy is extremely small.
16	the other hand now, we may get a situation now is: both	16	Q. I see.
17	bars reach their maximum tolerance, that becomes the	17	A. Okay, good.
18	figure on the right-most, that becomes 48 plus 48. And	18	Okay, go up.
19	also the installation procedure, we say the coupler	19	Okay, move.
20	needs to go into the end first, so that the parent bar	20	Move up. Okay.
21	will take up already 48. As the coupler is only	21	I got 45 that are less than 40. So 45 divided by 75
22	88 millimetres long, so the continuation bar, when it	22	is 60 per cent.
23	comes in, it can only go in for 40, and that's exactly	23	Q. The last question I have for you, in light of that: in
23	why you get two threads sticking out from that side.	23	your expert opinion, and in your expert opinion in
/4		_ <del></del> _	jour expert opinion, and in your expert opinion in
24 25	MR SO: Just following from what you have told us, the last	25	referring to the terms of reference of this Commission

21 (Pages 81 to 84)

	Page 85		Page 87
1	of Inquiry, it's your expert opinion that the structural	1	handed to you I think in October.
2	integrity is now compromised, not compromised, or you	2	However, and as will be apparent from the last
3	have doubt?	3	answer that Prof Yeung gave, safety now seems to be
4	A. We see 60 per cent of the couplers not installed	4	determined by reference to the opening-up, one would
5	properly in the sample, so by statistics that means, in	5	have thought perhaps exclusively by reference to the
6	the population, you may get a little bit more or less,	6	opening-up, and in particular the arbitrary, we would
7	depending on the margin of error in the sampling. But	7	say, pass or fail measurement of 37 millimetres which
8	with 60 per cent not construct according to the drawing,	8	the government has imposed upon MTR; secondly, the issue
9	and before I can have a chance to do a very detailed	9	of engagement or embedment, and very recently whether
10	analysis on the existing conditions, the best I would	10	rebars will butt-to-butt.
11	say is I have doubt on the structural integrity of the	11	We are very concerned about this because none of
12	structure.	12	these matters were investigated in the factual evidence.
13	MR SO: Thank you very much. I have no further questions.	13	For example, there was evidence that BOSA gave
14	CHAIRMAN: Good. Any questions arising from that? Because	14	instruction courses to the workers. It wasn't
15	that sort of came out at the end.	15	investigated whether there was any direction that it
16	Professor, thank you very much indeed. I think we	16	ought to be butt-to-butt or whatever. But we are very
17	kept you somewhat longer than intended. But thank you	17	concerned as to whether it's going to be suggested in
18	for all your help. It's been of great value. Thank you	18	some way that MTR Leightons must speak for
19	very much indeed.	19	themselves are responsible for the way the case on
20	WITNESS: Thank you.	20	safety or lack of safety is now being put, whether it's
21	(The witness was released)	21	going to be suggested that instead of satisfying
22	MR PENNICOTT: Sir, I see it's about 1.50, is it?	22	ourselves that there was a maximum of two threads
23	CHAIRMAN: It is, yes.	23	showing, we should have had some sort of x-ray machine
24	MR PENNICOTT: Mr Southward is the next expert to give	24	and we should have been looking for embedment or
25	evidence. Can I suggest perhaps we break for lunch now	25	engagement. We don't know whether it's going to be
	Page 86		Page 88
			1 age 86
1	and come back a bit earlier?	1	suggested against us. And it's not entirely
1 2	CHAIRMAN: Yes.	1 2	suggested against us. And it's not entirely CHAIRMAN: Sorry, suggested that you should have had some
2 3	CHAIRMAN: Yes. MR PENNICOTT: Perhaps come back at 2.05 or something of	2 3	suggested against us. And it's not entirely CHAIRMAN: Sorry, suggested that you should have had some sort of technology available to you at the time that the
2 3 4	CHAIRMAN: Yes. MR PENNICOTT: Perhaps come back at 2.05 or something of that nature?	2 3 4	suggested against us. And it's not entirely CHAIRMAN: Sorry, suggested that you should have had some sort of technology available to you at the time that the couplers were coupled?
2 3 4 5	<ul><li>CHAIRMAN: Yes.</li><li>MR PENNICOTT: Perhaps come back at 2.05 or something of that nature?</li><li>CHAIRMAN: That sounds good. So we will adjourn now until</li></ul>	2 3 4 5	suggested against us. And it's not entirely CHAIRMAN: Sorry, suggested that you should have had some sort of technology available to you at the time that the couplers were coupled? MR BOULDING: Exactly, whether our inspectors or supervisors
2 3 4 5 6	<ul><li>CHAIRMAN: Yes.</li><li>MR PENNICOTT: Perhaps come back at 2.05 or something of that nature?</li><li>CHAIRMAN: That sounds good. So we will adjourn now until 2.05. Thank you.</li></ul>	2 3 4 5 6	<ul> <li>suggested against us. And it's not entirely</li> <li>CHAIRMAN: Sorry, suggested that you should have had some sort of technology available to you at the time that the couplers were coupled?</li> <li>MR BOULDING: Exactly, whether our inspectors or supervisors should have been watching out for butt-to-butt, and if</li> </ul>
2 3 4 5 6 7	<ul><li>CHAIRMAN: Yes.</li><li>MR PENNICOTT: Perhaps come back at 2.05 or something of that nature?</li><li>CHAIRMAN: That sounds good. So we will adjourn now until 2.05. Thank you.</li><li>(12.53 pm)</li></ul>	2 3 4 5 6 7	<ul> <li>suggested against us. And it's not entirely</li> <li>CHAIRMAN: Sorry, suggested that you should have had some sort of technology available to you at the time that the couplers were coupled?</li> <li>MR BOULDING: Exactly, whether our inspectors or supervisors should have been watching out for butt-to-butt, and if so how, and so on and so forth.</li> </ul>
2 3 4 5 6 7 8	<ul> <li>CHAIRMAN: Yes.</li> <li>MR PENNICOTT: Perhaps come back at 2.05 or something of that nature?</li> <li>CHAIRMAN: That sounds good. So we will adjourn now until 2.05. Thank you.</li> <li>(12.53 pm)         (The luncheon adjournment)</li> </ul>	2 3 4 5 6 7 8	<ul> <li>suggested against us. And it's not entirely</li> <li>CHAIRMAN: Sorry, suggested that you should have had some sort of technology available to you at the time that the couplers were coupled?</li> <li>MR BOULDING: Exactly, whether our inspectors or supervisors should have been watching out for butt-to-butt, and if so how, and so on and so forth.</li> <li>So I don't know what the answer is but I did feel it</li> </ul>
2 3 4 5 6 7 8 9	<ul> <li>CHAIRMAN: Yes.</li> <li>MR PENNICOTT: Perhaps come back at 2.05 or something of that nature?</li> <li>CHAIRMAN: That sounds good. So we will adjourn now until 2.05. Thank you.</li> <li>(12.53 pm)</li></ul>	2 3 4 5 6 7 8 9	<ul> <li>suggested against us. And it's not entirely</li> <li>CHAIRMAN: Sorry, suggested that you should have had some sort of technology available to you at the time that the couplers were coupled?</li> <li>MR BOULDING: Exactly, whether our inspectors or supervisors should have been watching out for butt-to-butt, and if so how, and so on and so forth.</li> <li>So I don't know what the answer is but I did feel it appropriate just to put down a maker at this stage</li> </ul>
2 3 4 5 6 7 8 9 10	<ul> <li>CHAIRMAN: Yes.</li> <li>MR PENNICOTT: Perhaps come back at 2.05 or something of that nature?</li> <li>CHAIRMAN: That sounds good. So we will adjourn now until 2.05. Thank you.</li> <li>(12.53 pm)         (The luncheon adjournment)</li> <li>(2.14 pm)</li> <li>MR BOULDING: Sir, before Mr Southward is called, I wonder</li> </ul>	2 3 4 5 6 7 8 9 10	<ul> <li>suggested against us. And it's not entirely</li> <li>CHAIRMAN: Sorry, suggested that you should have had some sort of technology available to you at the time that the couplers were coupled?</li> <li>MR BOULDING: Exactly, whether our inspectors or supervisors should have been watching out for butt-to-butt, and if so how, and so on and so forth.</li> <li>So I don't know what the answer is but I did feel it appropriate just to put down a maker at this stage because we do seem to be moving quite a considerable way</li> </ul>
2 3 4 5 6 7 8 9 10 11	<ul> <li>CHAIRMAN: Yes.</li> <li>MR PENNICOTT: Perhaps come back at 2.05 or something of that nature?</li> <li>CHAIRMAN: That sounds good. So we will adjourn now until 2.05. Thank you.</li> <li>(12.53 pm)         <ul> <li>(The luncheon adjournment)</li> </ul> </li> <li>(2.14 pm)</li> <li>MR BOULDING: Sir, before Mr Southward is called, I wonder if I can make one or two observations on behalf of MTR</li> </ul>	2 3 4 5 6 7 8 9 10 11	<ul> <li>suggested against us. And it's not entirely</li> <li>CHAIRMAN: Sorry, suggested that you should have had some sort of technology available to you at the time that the couplers were coupled?</li> <li>MR BOULDING: Exactly, whether our inspectors or supervisors should have been watching out for butt-to-butt, and if so how, and so on and so forth.</li> <li>So I don't know what the answer is but I did feel it appropriate just to put down a maker at this stage because we do seem to be moving quite a considerable way from where we started.</li> </ul>
2 3 4 5 6 7 8 9 10 11 12	<ul> <li>CHAIRMAN: Yes.</li> <li>MR PENNICOTT: Perhaps come back at 2.05 or something of that nature?</li> <li>CHAIRMAN: That sounds good. So we will adjourn now until 2.05. Thank you.</li> <li>(12.53 pm)</li></ul>	2 3 4 5 6 7 8 9 10 11 12	<ul> <li>suggested against us. And it's not entirely</li> <li>CHAIRMAN: Sorry, suggested that you should have had some sort of technology available to you at the time that the couplers were coupled?</li> <li>MR BOULDING: Exactly, whether our inspectors or supervisors should have been watching out for butt-to-butt, and if so how, and so on and so forth.</li> <li>So I don't know what the answer is but I did feel it appropriate just to put down a maker at this stage because we do seem to be moving quite a considerable way from where we started.</li> <li>CHAIRMAN: Yes. It's one of the dangers of an inquiry of</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13	<ul> <li>CHAIRMAN: Yes.</li> <li>MR PENNICOTT: Perhaps come back at 2.05 or something of that nature?</li> <li>CHAIRMAN: That sounds good. So we will adjourn now until 2.05. Thank you.</li> <li>(12.53 pm)         <ul> <li>(The luncheon adjournment)</li> </ul> </li> <li>(2.14 pm)</li> <li>MR BOULDING: Sir, before Mr Southward is called, I wonder if I can make one or two observations on behalf of MTR as to quite where we are going now. It seems a long time ago but when the Commission of</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13	<ul> <li>suggested against us. And it's not entirely</li> <li>CHAIRMAN: Sorry, suggested that you should have had some sort of technology available to you at the time that the couplers were coupled?</li> <li>MR BOULDING: Exactly, whether our inspectors or supervisors should have been watching out for butt-to-butt, and if so how, and so on and so forth.</li> <li>So I don't know what the answer is but I did feel it appropriate just to put down a maker at this stage because we do seem to be moving quite a considerable way from where we started.</li> <li>CHAIRMAN: Yes. It's one of the dangers of an inquiry of this kind. I confess to having considerable sympathy</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14	<ul> <li>CHAIRMAN: Yes.</li> <li>MR PENNICOTT: Perhaps come back at 2.05 or something of that nature?</li> <li>CHAIRMAN: That sounds good. So we will adjourn now until 2.05. Thank you.</li> <li>(12.53 pm)         <ul> <li>(The luncheon adjournment)</li> </ul> </li> <li>(2.14 pm)</li> <li>MR BOULDING: Sir, before Mr Southward is called, I wonder if I can make one or two observations on behalf of MTR as to quite where we are going now.         <ul> <li>It seems a long time ago but when the Commission of Inquiry started, perhaps the two most important matters</li> </ul> </li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14	<ul> <li>suggested against us. And it's not entirely</li> <li>CHAIRMAN: Sorry, suggested that you should have had some sort of technology available to you at the time that the couplers were coupled?</li> <li>MR BOULDING: Exactly, whether our inspectors or supervisors should have been watching out for butt-to-butt, and if so how, and so on and so forth.</li> <li>So I don't know what the answer is but I did feel it appropriate just to put down a maker at this stage because we do seem to be moving quite a considerable way from where we started.</li> <li>CHAIRMAN: Yes. It's one of the dangers of an inquiry of this kind. I confess to having considerable sympathy because both Prof Hansford and myself have been</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15	<ul> <li>CHAIRMAN: Yes.</li> <li>MR PENNICOTT: Perhaps come back at 2.05 or something of that nature?</li> <li>CHAIRMAN: That sounds good. So we will adjourn now until 2.05. Thank you.</li> <li>(12.53 pm)         <ul> <li>(The luncheon adjournment)</li> </ul> </li> <li>(2.14 pm)</li> <li>MR BOULDING: Sir, before Mr Southward is called, I wonder if I can make one or two observations on behalf of MTR as to quite where we are going now.         <ul> <li>It seems a long time ago but when the Commission of Inquiry started, perhaps the two most important matters to enquire into was firstly the issue of the cut rebar</li> </ul> </li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15	<ul> <li>suggested against us. And it's not entirely</li> <li>CHAIRMAN: Sorry, suggested that you should have had some sort of technology available to you at the time that the couplers were coupled?</li> <li>MR BOULDING: Exactly, whether our inspectors or supervisors should have been watching out for butt-to-butt, and if so how, and so on and so forth.</li> <li>So I don't know what the answer is but I did feel it appropriate just to put down a maker at this stage because we do seem to be moving quite a considerable way from where we started.</li> <li>CHAIRMAN: Yes. It's one of the dangers of an inquiry of this kind. I confess to having considerable sympathy because both Prof Hansford and myself have been burrowing away behind our closed doors, looking for</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	<ul> <li>CHAIRMAN: Yes.</li> <li>MR PENNICOTT: Perhaps come back at 2.05 or something of that nature?</li> <li>CHAIRMAN: That sounds good. So we will adjourn now until 2.05. Thank you.</li> <li>(12.53 pm)         <ul> <li>(The luncheon adjournment)</li> </ul> </li> <li>(2.14 pm)</li> <li>MR BOULDING: Sir, before Mr Southward is called, I wonder if I can make one or two observations on behalf of MTR as to quite where we are going now.         <ul> <li>It seems a long time ago but when the Commission of Inquiry started, perhaps the two most important matters to enquire into was firstly the issue of the cut rebar and secondly the connection detail, and you will recall</li> </ul></li></ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	<ul> <li>suggested against us. And it's not entirely</li> <li>CHAIRMAN: Sorry, suggested that you should have had some sort of technology available to you at the time that the couplers were coupled?</li> <li>MR BOULDING: Exactly, whether our inspectors or supervisors should have been watching out for butt-to-butt, and if so how, and so on and so forth.</li> <li>So I don't know what the answer is but I did feel it appropriate just to put down a maker at this stage because we do seem to be moving quite a considerable way from where we started.</li> <li>CHAIRMAN: Yes. It's one of the dangers of an inquiry of this kind. I confess to having considerable sympathy because both Prof Hansford and myself have been burrowing away behind our closed doors, looking for example to BOSA's evidence, and going back to some of</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	<ul> <li>CHAIRMAN: Yes.</li> <li>MR PENNICOTT: Perhaps come back at 2.05 or something of that nature?</li> <li>CHAIRMAN: That sounds good. So we will adjourn now until 2.05. Thank you.</li> <li>(12.53 pm)         <ul> <li>(The luncheon adjournment)</li> </ul> </li> <li>(2.14 pm)</li> <li>MR BOULDING: Sir, before Mr Southward is called, I wonder if I can make one or two observations on behalf of MTR as to quite where we are going now.         <ul> <li>It seems a long time ago but when the Commission of Inquiry started, perhaps the two most important matters to enquire into was firstly the issue of the cut rebar and secondly the connection detail, and you will recall that that was the focus of the evidence over a number of</li> </ul></li></ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	<ul> <li>suggested against us. And it's not entirely</li> <li>CHAIRMAN: Sorry, suggested that you should have had some sort of technology available to you at the time that the couplers were coupled?</li> <li>MR BOULDING: Exactly, whether our inspectors or supervisors should have been watching out for butt-to-butt, and if so how, and so on and so forth.</li> <li>So I don't know what the answer is but I did feel it appropriate just to put down a maker at this stage because we do seem to be moving quite a considerable way from where we started.</li> <li>CHAIRMAN: Yes. It's one of the dangers of an inquiry of this kind. I confess to having considerable sympathy because both Prof Hansford and myself have been burrowing away behind our closed doors, looking for example to BOSA's evidence, and going back to some of the original employees and things like that, to find out</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	<ul> <li>CHAIRMAN: Yes.</li> <li>MR PENNICOTT: Perhaps come back at 2.05 or something of that nature?</li> <li>CHAIRMAN: That sounds good. So we will adjourn now until 2.05. Thank you.</li> <li>(12.53 pm)         <ul> <li>(The luncheon adjournment)</li> </ul> </li> <li>(2.14 pm)</li> <li>MR BOULDING: Sir, before Mr Southward is called, I wonder if I can make one or two observations on behalf of MTR as to quite where we are going now.         <ul> <li>It seems a long time ago but when the Commission of Inquiry started, perhaps the two most important matters to enquire into was firstly the issue of the cut rebar and secondly the connection detail, and you will recall that that was the focus of the evidence over a number of weeks, and of course it was against those two matters</li> </ul></li></ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	<ul> <li>suggested against us. And it's not entirely</li> <li>CHAIRMAN: Sorry, suggested that you should have had some sort of technology available to you at the time that the couplers were coupled?</li> <li>MR BOULDING: Exactly, whether our inspectors or supervisors should have been watching out for butt-to-butt, and if so how, and so on and so forth.</li> <li>So I don't know what the answer is but I did feel it appropriate just to put down a maker at this stage because we do seem to be moving quite a considerable way from where we started.</li> <li>CHAIRMAN: Yes. It's one of the dangers of an inquiry of this kind. I confess to having considerable sympathy because both Prof Hansford and myself have been burrowing away behind our closed doors, looking for example to BOSA's evidence, and going back to some of the original employees and things like that, to find out did anything arise about these issues, and at the moment</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	<ul> <li>CHAIRMAN: Yes.</li> <li>MR PENNICOTT: Perhaps come back at 2.05 or something of that nature?</li> <li>CHAIRMAN: That sounds good. So we will adjourn now until 2.05. Thank you.</li> <li>(12.53 pm)         <ul> <li>(The luncheon adjournment)</li> </ul> </li> <li>(2.14 pm)</li> <li>MR BOULDING: Sir, before Mr Southward is called, I wonder if I can make one or two observations on behalf of MTR as to quite where we are going now.         <ul> <li>It seems a long time ago but when the Commission of Inquiry started, perhaps the two most important matters to enquire into was firstly the issue of the cut rebar and secondly the connection detail, and you will recall that that was the focus of the evidence over a number of weeks, and of course it was against those two matters primarily, if not exclusively, that issues of safety</li> </ul></li></ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	<ul> <li>suggested against us. And it's not entirely</li> <li>CHAIRMAN: Sorry, suggested that you should have had some sort of technology available to you at the time that the couplers were coupled?</li> <li>MR BOULDING: Exactly, whether our inspectors or supervisors should have been watching out for butt-to-butt, and if so how, and so on and so forth.</li> <li>So I don't know what the answer is but I did feel it appropriate just to put down a maker at this stage because we do seem to be moving quite a considerable way from where we started.</li> <li>CHAIRMAN: Yes. It's one of the dangers of an inquiry of this kind. I confess to having considerable sympathy because both Prof Hansford and myself have been burrowing away behind our closed doors, looking for example to BOSA's evidence, and going back to some of the original employees and things like that, to find out did anything arise about these issues, and at the moment it seems not.</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	<ul> <li>CHAIRMAN: Yes.</li> <li>MR PENNICOTT: Perhaps come back at 2.05 or something of that nature?</li> <li>CHAIRMAN: That sounds good. So we will adjourn now until 2.05. Thank you.</li> <li>(12.53 pm)         <ul> <li>(The luncheon adjournment)</li> </ul> </li> <li>(2.14 pm)</li> <li>MR BOULDING: Sir, before Mr Southward is called, I wonder if I can make one or two observations on behalf of MTR as to quite where we are going now.</li> <li>It seems a long time ago but when the Commission of Inquiry started, perhaps the two most important matters to enquire into was firstly the issue of the cut rebar and secondly the connection detail, and you will recall that that was the focus of the evidence over a number of weeks, and of course it was against those two matters primarily, if not exclusively, that issues of safety were to be considered.</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	<ul> <li>suggested against us. And it's not entirely</li> <li>CHAIRMAN: Sorry, suggested that you should have had some sort of technology available to you at the time that the couplers were coupled?</li> <li>MR BOULDING: Exactly, whether our inspectors or supervisors should have been watching out for butt-to-butt, and if so how, and so on and so forth.</li> <li>So I don't know what the answer is but I did feel it appropriate just to put down a maker at this stage because we do seem to be moving quite a considerable way from where we started.</li> <li>CHAIRMAN: Yes. It's one of the dangers of an inquiry of this kind. I confess to having considerable sympathy because both Prof Hansford and myself have been burrowing away behind our closed doors, looking for example to BOSA's evidence, and going back to some of the original employees and things like that, to find out did anything arise about these issues, and at the moment it seems not.</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	<ul> <li>CHAIRMAN: Yes.</li> <li>MR PENNICOTT: Perhaps come back at 2.05 or something of that nature?</li> <li>CHAIRMAN: That sounds good. So we will adjourn now until 2.05. Thank you.</li> <li>(12.53 pm)         <ul> <li>(The luncheon adjournment)</li> </ul> </li> <li>(2.14 pm)</li> <li>MR BOULDING: Sir, before Mr Southward is called, I wonder if I can make one or two observations on behalf of MTR as to quite where we are going now.         <ul> <li>It seems a long time ago but when the Commission of Inquiry started, perhaps the two most important matters to enquire into was firstly the issue of the cut rebar and secondly the connection detail, and you will recall that that was the focus of the evidence over a number of weeks, and of course it was against those two matters primarily, if not exclusively, that issues of safety were to be considered.         <ul> <li>But we have now moved on to the opening-up phase</li> </ul> </li> </ul></li></ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	<ul> <li>suggested against us. And it's not entirely</li> <li>CHAIRMAN: Sorry, suggested that you should have had some sort of technology available to you at the time that the couplers were coupled?</li> <li>MR BOULDING: Exactly, whether our inspectors or supervisors should have been watching out for butt-to-butt, and if so how, and so on and so forth.</li> <li>So I don't know what the answer is but I did feel it appropriate just to put down a maker at this stage because we do seem to be moving quite a considerable way from where we started.</li> <li>CHAIRMAN: Yes. It's one of the dangers of an inquiry of this kind. I confess to having considerable sympathy because both Prof Hansford and myself have been burrowing away behind our closed doors, looking for example to BOSA's evidence, and going back to some of the original employees and things like that, to find out did anything arise about these issues, and at the moment it seems not.</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	<ul> <li>CHAIRMAN: Yes.</li> <li>MR PENNICOTT: Perhaps come back at 2.05 or something of that nature?</li> <li>CHAIRMAN: That sounds good. So we will adjourn now until 2.05. Thank you.</li> <li>(12.53 pm)         <ul> <li>(The luncheon adjournment)</li> </ul> </li> <li>(2.14 pm)</li> <li>MR BOULDING: Sir, before Mr Southward is called, I wonder if I can make one or two observations on behalf of MTR as to quite where we are going now.         <ul> <li>It seems a long time ago but when the Commission of Inquiry started, perhaps the two most important matters to enquire into was firstly the issue of the cut rebar and secondly the connection detail, and you will recall that that was the focus of the evidence over a number of weeks, and of course it was against those two matters primarily, if not exclusively, that issues of safety were to be considered.         <ul> <li>But we have now moved on to the opening-up phase which, as I understand it, was directed initially at</li> </ul> </li> </ul></li></ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	<ul> <li>suggested against us. And it's not entirely</li> <li>CHAIRMAN: Sorry, suggested that you should have had some sort of technology available to you at the time that the couplers were coupled?</li> <li>MR BOULDING: Exactly, whether our inspectors or supervisors should have been watching out for butt-to-butt, and if so how, and so on and so forth.</li> <li>So I don't know what the answer is but I did feel it appropriate just to put down a maker at this stage because we do seem to be moving quite a considerable way from where we started.</li> <li>CHAIRMAN: Yes. It's one of the dangers of an inquiry of this kind. I confess to having considerable sympathy because both Prof Hansford and myself have been burrowing away behind our closed doors, looking for example to BOSA's evidence, and going back to some of the original employees and things like that, to find out did anything arise about these issues, and at the moment it seems not.</li> <li>MR BOULDING: As you will have heard this morning, you heard me refer to Mr Wong's evidence, and he was looking for</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>CHAIRMAN: Yes.</li> <li>MR PENNICOTT: Perhaps come back at 2.05 or something of that nature?</li> <li>CHAIRMAN: That sounds good. So we will adjourn now until 2.05. Thank you.</li> <li>(12.53 pm)         <ul> <li>(The luncheon adjournment)</li> </ul> </li> <li>(2.14 pm)</li> <li>MR BOULDING: Sir, before Mr Southward is called, I wonder if I can make one or two observations on behalf of MTR as to quite where we are going now.         <ul> <li>It seems a long time ago but when the Commission of Inquiry started, perhaps the two most important matters to enquire into was firstly the issue of the cut rebar and secondly the connection detail, and you will recall that that was the focus of the evidence over a number of weeks, and of course it was against those two matters primarily, if not exclusively, that issues of safety were to be considered.         <ul> <li>But we have now moved on to the opening-up phase</li> </ul> </li> </ul></li></ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>suggested against us. And it's not entirely</li> <li>CHAIRMAN: Sorry, suggested that you should have had some sort of technology available to you at the time that the couplers were coupled?</li> <li>MR BOULDING: Exactly, whether our inspectors or supervisors should have been watching out for butt-to-butt, and if so how, and so on and so forth.</li> <li>So I don't know what the answer is but I did feel it appropriate just to put down a maker at this stage because we do seem to be moving quite a considerable way from where we started.</li> <li>CHAIRMAN: Yes. It's one of the dangers of an inquiry of this kind. I confess to having considerable sympathy because both Prof Hansford and myself have been burrowing away behind our closed doors, looking for example to BOSA's evidence, and going back to some of the original employees and things like that, to find out did anything arise about these issues, and at the moment it seems not.</li> <li>MR BOULDING: As you will have heard this morning, you heard me refer to Mr Wong's evidence, and he was looking for the 2 millimetres.</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	<ul> <li>CHAIRMAN: Yes.</li> <li>MR PENNICOTT: Perhaps come back at 2.05 or something of that nature?</li> <li>CHAIRMAN: That sounds good. So we will adjourn now until 2.05. Thank you.</li> <li>(12.53 pm)         <ul> <li>(The luncheon adjournment)</li> </ul> </li> <li>(2.14 pm)</li> <li>MR BOULDING: Sir, before Mr Southward is called, I wonder if I can make one or two observations on behalf of MTR as to quite where we are going now.         <ul> <li>It seems a long time ago but when the Commission of Inquiry started, perhaps the two most important matters to enquire into was firstly the issue of the cut rebar and secondly the connection detail, and you will recall that that was the focus of the evidence over a number of weeks, and of course it was against those two matters primarily, if not exclusively, that issues of safety were to be considered.         <ul> <li>But we have now moved on to the opening-up phase which, as I understand it, was directed initially at establishing the extent of the cut bars and secondly</li> </ul> </li> </ul></li></ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	<ul> <li>suggested against us. And it's not entirely</li> <li>CHAIRMAN: Sorry, suggested that you should have had some sort of technology available to you at the time that the couplers were coupled?</li> <li>MR BOULDING: Exactly, whether our inspectors or supervisors should have been watching out for butt-to-butt, and if so how, and so on and so forth.</li> <li>So I don't know what the answer is but I did feel it appropriate just to put down a maker at this stage because we do seem to be moving quite a considerable way from where we started.</li> <li>CHAIRMAN: Yes. It's one of the dangers of an inquiry of this kind. I confess to having considerable sympathy because both Prof Hansford and myself have been burrowing away behind our closed doors, looking for example to BOSA's evidence, and going back to some of the original employees and things like that, to find out did anything arise about these issues, and at the moment it seems not.</li> <li>MR BOULDING: As you will have heard this morning, you heard me refer to Mr Wong's evidence, and he was looking for the 2 millimetres.</li> <li>COMMISSIONER HANSFORD: Two threads.</li> </ul>

	Page 89		Page 91
1	recommendation and he agreed with me.	1	terms of reference; it may throw up matters outside of
2	That seems to me to be a test that we ought to have	2	the allegation of cutting of threads, which ironically
3	been looking for. If we found the two threads,	2	was the only thing Mr Poon alleged at the very outset
4	a maximum of two threads, job done. Now it appears to	4	which gave rise to media enquiry, and I would add it's
5	be progressing somewhat from that, and I don't know	5	somewhat ironic that Mr Poon and China Tech, and the
6	what's going to be suggested at the end of the day, so	6	experts engaged by China Tech now see fit to have
7	far as we're concerned, and of course so far as Leighton	7	a roving enquiry on matters outside of the allegations
8	is concerned because Mr Paul Shieh is obviously very	8	originally made. These are all matters we will make in
9	competent and will be looking after their interests, but	9	due course.
10	I don't know whether it's going to be suggested that	10	But in order to assist the Commission, because the
11	Leightons were somehow in breach of contract through	11	Commission when it asked for the experts' evidence to be
12	failing to achieve butt-to-butt on every single coupler.	12	reduced into a kind of synopsis, the Commission did ask
13	CHAIRMAN: Well, butt-to-butt is brand new to us.	13	for the experts to comment on opening-up,
14	MR BOULDING: And to me.	14	understandably, and the experts will be commenting on
15	CHAIRMAN: Look, this is a danger we run. We have had in		that.
16	progress, and still have in progress, a collateral	16	But it is not to be taken as somehow Leighton
17	exercise, namely one of opening up, conducted	17	accepting that somehow we are to be taken as being fully
18	essentially independently of the Inquiry, and that	18	equipped or prepared to deal with a hitherto
19	collateral exercise is being judged and assessed	19	unarticulated cause for concern, namely bars, albeit not
20	independently. So what we have to do, I think, is just	20	cut, for whatever reason, now having been detected to be
21	try to stay abreast of that, and if we have to recall	21	not possessing the arbitrarily imposed 40 millimetres
22	a number of witnesses, even if, with the greatest of	22	engaged or embedded length.
23	respect, it means calling them after normal working	23	As the discussion we have seen so far, we have all
24	hours or something like that, just so we can clarify	24	been trying to "interpret" in lawyerly fashion what BOSA
25	some matters, then I think we may have to do so. That's	25	has written back then and maybe a couple of weeks ago.
	Page 90		Page 92
1	just off the top of my head.	1	That is unsatisfactory. All I can say is we will do our
2	MR BOULDING: Of course.	2	best to assist by commenting on the issues of opening-up
3	CHAIRMAN: But we share your concerns, Mr Boulding.	3	but with an eye to ultimately addressing the issues
4		5	
	MR SHIEH. May I simply add that Mr Chairman had his tingers	4	
5	MR SHIEH: May I simply add that Mr Chairman had his fingers on the nub of the matter, namely that we actually have		raised by the terms of reference, which actually are
5 6	on the nub of the matter, namely that we actually have	5	raised by the terms of reference, which actually are referable back to allegations made way back in May, as
6	on the nub of the matter, namely that we actually have two parallel processes going on. As perhaps of	5 6	raised by the terms of reference, which actually are referable back to allegations made way back in May, as publicised by the media.
6 7	on the nub of the matter, namely that we actually have two parallel processes going on. As perhaps of a political knee-jerk reaction or whatever may be the	5 6 7	raised by the terms of reference, which actually are referable back to allegations made way back in May, as publicised by the media. MR SO: Mr Chairman, if I may respond.
6 7 8	on the nub of the matter, namely that we actually have two parallel processes going on. As perhaps of a political knee-jerk reaction or whatever may be the reason, the administration appointed a Commission of	5 6	<ul><li>raised by the terms of reference, which actually are</li><li>referable back to allegations made way back in May, as</li><li>publicised by the media.</li><li>MR SO: Mr Chairman, if I may respond.</li><li>CHAIRMAN: Yes.</li></ul>
6 7 8 9	on the nub of the matter, namely that we actually have two parallel processes going on. As perhaps of a political knee-jerk reaction or whatever may be the reason, the administration appointed a Commission of Inquiry, and then as things went by, someone came up	5 6 7 8 9	<ul><li>raised by the terms of reference, which actually are</li><li>referable back to allegations made way back in May, as</li><li>publicised by the media.</li><li>MR SO: Mr Chairman, if I may respond.</li><li>CHAIRMAN: Yes.</li><li>MR SO: I have two points to address. First is in regards</li></ul>
6 7 8	on the nub of the matter, namely that we actually have two parallel processes going on. As perhaps of a political knee-jerk reaction or whatever may be the reason, the administration appointed a Commission of Inquiry, and then as things went by, someone came up with an idea of some experts getting their heads	5 6 7 8 9 10	<ul><li>raised by the terms of reference, which actually are</li><li>referable back to allegations made way back in May, as</li><li>publicised by the media.</li><li>MR SO: Mr Chairman, if I may respond.</li><li>CHAIRMAN: Yes.</li><li>MR SO: I have two points to address. First is in regards</li><li>to Mr Boulding's observation as per whether there would</li></ul>
6 7 8 9 10	on the nub of the matter, namely that we actually have two parallel processes going on. As perhaps of a political knee-jerk reaction or whatever may be the reason, the administration appointed a Commission of Inquiry, and then as things went by, someone came up with an idea of some experts getting their heads together and then an opening-up exercise going on, when	5 6 7 8 9 10 11	<ul> <li>raised by the terms of reference, which actually are</li> <li>referable back to allegations made way back in May, as</li> <li>publicised by the media.</li> <li>MR SO: Mr Chairman, if I may respond.</li> <li>CHAIRMAN: Yes.</li> <li>MR SO: I have two points to address. First is in regards</li> <li>to Mr Boulding's observation as per whether there would</li> <li>be allegations on the part of in particular China</li> </ul>
6 7 8 9 10 11	on the nub of the matter, namely that we actually have two parallel processes going on. As perhaps of a political knee-jerk reaction or whatever may be the reason, the administration appointed a Commission of Inquiry, and then as things went by, someone came up with an idea of some experts getting their heads	5 6 7 8 9 10 11 12	<ul> <li>raised by the terms of reference, which actually are</li> <li>referable back to allegations made way back in May, as</li> <li>publicised by the media.</li> <li>MR SO: Mr Chairman, if I may respond.</li> <li>CHAIRMAN: Yes.</li> <li>MR SO: I have two points to address. First is in regards</li> <li>to Mr Boulding's observation as per whether there would</li> <li>be allegations on the part of in particular China</li> <li>Technology as to whether there are failures in</li> </ul>
6 7 8 9 10 11 12	on the nub of the matter, namely that we actually have two parallel processes going on. As perhaps of a political knee-jerk reaction or whatever may be the reason, the administration appointed a Commission of Inquiry, and then as things went by, someone came up with an idea of some experts getting their heads together and then an opening-up exercise going on, when the Commission of Inquiry was actually deep into its	5 6 7 8 9 10 11	<ul> <li>raised by the terms of reference, which actually are</li> <li>referable back to allegations made way back in May, as</li> <li>publicised by the media.</li> <li>MR SO: Mr Chairman, if I may respond.</li> <li>CHAIRMAN: Yes.</li> <li>MR SO: I have two points to address. First is in regards</li> <li>to Mr Boulding's observation as per whether there would</li> <li>be allegations on the part of in particular China</li> <li>Technology as to whether there are failures in</li> <li>supervisory plan.</li> </ul>
6 7 8 9 10 11 12 13	on the nub of the matter, namely that we actually have two parallel processes going on. As perhaps of a political knee-jerk reaction or whatever may be the reason, the administration appointed a Commission of Inquiry, and then as things went by, someone came up with an idea of some experts getting their heads together and then an opening-up exercise going on, when the Commission of Inquiry was actually deep into its hearings. One of the points we may make in our closing	5 6 7 8 9 10 11 12 13	<ul> <li>raised by the terms of reference, which actually are</li> <li>referable back to allegations made way back in May, as</li> <li>publicised by the media.</li> <li>MR SO: Mr Chairman, if I may respond.</li> <li>CHAIRMAN: Yes.</li> <li>MR SO: I have two points to address. First is in regards</li> <li>to Mr Boulding's observation as per whether there would</li> <li>be allegations on the part of in particular China</li> <li>Technology as to whether there are failures in</li> <li>supervisory plan.</li> <li>As far as I'm concerned, I'm not trying to make</li> </ul>
6 7 8 9 10 11 12 13 14	on the nub of the matter, namely that we actually have two parallel processes going on. As perhaps of a political knee-jerk reaction or whatever may be the reason, the administration appointed a Commission of Inquiry, and then as things went by, someone came up with an idea of some experts getting their heads together and then an opening-up exercise going on, when the Commission of Inquiry was actually deep into its hearings.	5 6 7 8 9 10 11 12 13 14	<ul> <li>raised by the terms of reference, which actually are</li> <li>referable back to allegations made way back in May, as</li> <li>publicised by the media.</li> <li>MR SO: Mr Chairman, if I may respond.</li> <li>CHAIRMAN: Yes.</li> <li>MR SO: I have two points to address. First is in regards</li> <li>to Mr Boulding's observation as per whether there would</li> <li>be allegations on the part of in particular China</li> <li>Technology as to whether there are failures in</li> <li>supervisory plan.</li> <li>As far as I'm concerned, I'm not trying to make</li> <li>submission or giving evidence from the bar table, but</li> </ul>
6 7 8 9 10 11 12 13 14 15	on the nub of the matter, namely that we actually have two parallel processes going on. As perhaps of a political knee-jerk reaction or whatever may be the reason, the administration appointed a Commission of Inquiry, and then as things went by, someone came up with an idea of some experts getting their heads together and then an opening-up exercise going on, when the Commission of Inquiry was actually deep into its hearings. One of the points we may make in our closing submission is that usually, in prior Commissions of	5 6 7 8 9 10 11 12 13 14 15	<ul> <li>raised by the terms of reference, which actually are</li> <li>referable back to allegations made way back in May, as</li> <li>publicised by the media.</li> <li>MR SO: Mr Chairman, if I may respond.</li> <li>CHAIRMAN: Yes.</li> <li>MR SO: I have two points to address. First is in regards</li> <li>to Mr Boulding's observation as per whether there would</li> <li>be allegations on the part of in particular China</li> <li>Technology as to whether there are failures in</li> <li>supervisory plan.</li> <li>As far as I'm concerned, I'm not trying to make</li> </ul>
6 7 8 9 10 11 12 13 14 15 16	on the nub of the matter, namely that we actually have two parallel processes going on. As perhaps of a political knee-jerk reaction or whatever may be the reason, the administration appointed a Commission of Inquiry, and then as things went by, someone came up with an idea of some experts getting their heads together and then an opening-up exercise going on, when the Commission of Inquiry was actually deep into its hearings. One of the points we may make in our closing submission is that usually, in prior Commissions of Inquiries in the past few years, one has an undisputed	5 6 7 8 9 10 11 12 13 14 15 16	<ul> <li>raised by the terms of reference, which actually are</li> <li>referable back to allegations made way back in May, as</li> <li>publicised by the media.</li> <li>MR SO: Mr Chairman, if I may respond.</li> <li>CHAIRMAN: Yes.</li> <li>MR SO: I have two points to address. First is in regards</li> <li>to Mr Boulding's observation as per whether there would</li> <li>be allegations on the part of in particular China</li> <li>Technology as to whether there are failures in</li> <li>supervisory plan.</li> <li>As far as I'm concerned, I'm not trying to make</li> <li>submission or giving evidence from the bar table, but</li> <li>insofar as we read the evidence of Prof Yeung and read</li> </ul>
6 7 8 9 10 11 12 13 14 15 16 17	on the nub of the matter, namely that we actually have two parallel processes going on. As perhaps of a political knee-jerk reaction or whatever may be the reason, the administration appointed a Commission of Inquiry, and then as things went by, someone came up with an idea of some experts getting their heads together and then an opening-up exercise going on, when the Commission of Inquiry was actually deep into its hearings. One of the points we may make in our closing submission is that usually, in prior Commissions of Inquiries in the past few years, one has an undisputed incident or catastrophe, such as a ship collision or	5 6 7 8 9 10 11 12 13 14 15 16 17	<ul> <li>raised by the terms of reference, which actually are</li> <li>referable back to allegations made way back in May, as</li> <li>publicised by the media.</li> <li>MR SO: Mr Chairman, if I may respond.</li> <li>CHAIRMAN: Yes.</li> <li>MR SO: I have two points to address. First is in regards</li> <li>to Mr Boulding's observation as per whether there would</li> <li>be allegations on the part of in particular China</li> <li>Technology as to whether there are failures in</li> <li>supervisory plan.</li> <li>As far as I'm concerned, I'm not trying to make</li> <li>submission or giving evidence from the bar table, but</li> <li>insofar as we read the evidence of Prof Yeung and read</li> <li>the evidence of Mr Paulino Lim from BOSA in collective</li> </ul>
6 7 8 9 10 11 12 13 14 15 16 17 18	on the nub of the matter, namely that we actually have two parallel processes going on. As perhaps of a political knee-jerk reaction or whatever may be the reason, the administration appointed a Commission of Inquiry, and then as things went by, someone came up with an idea of some experts getting their heads together and then an opening-up exercise going on, when the Commission of Inquiry was actually deep into its hearings. One of the points we may make in our closing submission is that usually, in prior Commissions of Inquiries in the past few years, one has an undisputed incident or catastrophe, such as a ship collision or lead found in drinking water, where nobody is seriously	5 6 7 8 9 10 11 12 13 14 15 16 17 18	<ul> <li>raised by the terms of reference, which actually are</li> <li>referable back to allegations made way back in May, as</li> <li>publicised by the media.</li> <li>MR SO: Mr Chairman, if I may respond.</li> <li>CHAIRMAN: Yes.</li> <li>MR SO: I have two points to address. First is in regards</li> <li>to Mr Boulding's observation as per whether there would</li> <li>be allegations on the part of in particular China</li> <li>Technology as to whether there are failures in</li> <li>supervisory plan.</li> <li>As far as I'm concerned, I'm not trying to make</li> <li>submission or giving evidence from the bar table, but</li> <li>insofar as we read the evidence of Prof Yeung and read</li> <li>the evidence of Mr Paulino Lim from BOSA in collective</li> <li>terms, it seems that the butt-to-butt requirement would</li> </ul>
6 7 8 9 10 11 12 13 14 15 16 17 18 19	on the nub of the matter, namely that we actually have two parallel processes going on. As perhaps of a political knee-jerk reaction or whatever may be the reason, the administration appointed a Commission of Inquiry, and then as things went by, someone came up with an idea of some experts getting their heads together and then an opening-up exercise going on, when the Commission of Inquiry was actually deep into its hearings. One of the points we may make in our closing submission is that usually, in prior Commissions of Inquiries in the past few years, one has an undisputed incident or catastrophe, such as a ship collision or lead found in drinking water, where nobody is seriously disputing what actually happened, so people can	5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	<ul> <li>raised by the terms of reference, which actually are</li> <li>referable back to allegations made way back in May, as</li> <li>publicised by the media.</li> <li>MR SO: Mr Chairman, if I may respond.</li> <li>CHAIRMAN: Yes.</li> <li>MR SO: I have two points to address. First is in regards</li> <li>to Mr Boulding's observation as per whether there would</li> <li>be allegations on the part of in particular China</li> <li>Technology as to whether there are failures in</li> <li>supervisory plan.</li> <li>As far as I'm concerned, I'm not trying to make</li> <li>submission or giving evidence from the bar table, but</li> <li>insofar as we read the evidence of Prof Yeung and read</li> <li>the evidence of Mr Paulino Lim from BOSA in collective</li> <li>terms, it seems that the butt-to-butt requirement would</li> <li>effectively be satisfied if the requirement of BOSA that</li> <li>no more than two threads are being exposed. So, in</li> </ul>
6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	on the nub of the matter, namely that we actually have two parallel processes going on. As perhaps of a political knee-jerk reaction or whatever may be the reason, the administration appointed a Commission of Inquiry, and then as things went by, someone came up with an idea of some experts getting their heads together and then an opening-up exercise going on, when the Commission of Inquiry was actually deep into its hearings. One of the points we may make in our closing submission is that usually, in prior Commissions of Inquiries in the past few years, one has an undisputed incident or catastrophe, such as a ship collision or lead found in drinking water, where nobody is seriously disputing what actually happened, so people can meaningfully find out why it happened, with no one	5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	<ul> <li>raised by the terms of reference, which actually are</li> <li>referable back to allegations made way back in May, as</li> <li>publicised by the media.</li> <li>MR SO: Mr Chairman, if I may respond.</li> <li>CHAIRMAN: Yes.</li> <li>MR SO: I have two points to address. First is in regards</li> <li>to Mr Boulding's observation as per whether there would</li> <li>be allegations on the part of in particular China</li> <li>Technology as to whether there are failures in</li> <li>supervisory plan.</li> <li>As far as I'm concerned, I'm not trying to make</li> <li>submission or giving evidence from the bar table, but</li> <li>insofar as we read the evidence of Prof Yeung and read</li> <li>the evidence of Mr Paulino Lim from BOSA in collective</li> <li>terms, it seems that the butt-to-butt requirement would</li> </ul>
6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	on the nub of the matter, namely that we actually have two parallel processes going on. As perhaps of a political knee-jerk reaction or whatever may be the reason, the administration appointed a Commission of Inquiry, and then as things went by, someone came up with an idea of some experts getting their heads together and then an opening-up exercise going on, when the Commission of Inquiry was actually deep into its hearings. One of the points we may make in our closing submission is that usually, in prior Commissions of Inquiries in the past few years, one has an undisputed incident or catastrophe, such as a ship collision or lead found in drinking water, where nobody is seriously disputing what actually happened, so people can meaningfully find out why it happened, with no one having any particular axe to grind; whereas now we are	5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	<ul> <li>raised by the terms of reference, which actually are</li> <li>referable back to allegations made way back in May, as</li> <li>publicised by the media.</li> <li>MR SO: Mr Chairman, if I may respond.</li> <li>CHAIRMAN: Yes.</li> <li>MR SO: I have two points to address. First is in regards</li> <li>to Mr Boulding's observation as per whether there would</li> <li>be allegations on the part of in particular China</li> <li>Technology as to whether there are failures in</li> <li>supervisory plan.</li> <li>As far as I'm concerned, I'm not trying to make</li> <li>submission or giving evidence from the bar table, but</li> <li>insofar as we read the evidence of Prof Yeung and read</li> <li>the evidence of Mr Paulino Lim from BOSA in collective</li> <li>terms, it seems that the butt-to-butt requirement would</li> <li>effectively be satisfied if the requirement of BOSA that</li> <li>no more than two threads are being exposed. So, in</li> </ul>
6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	on the nub of the matter, namely that we actually have two parallel processes going on. As perhaps of a political knee-jerk reaction or whatever may be the reason, the administration appointed a Commission of Inquiry, and then as things went by, someone came up with an idea of some experts getting their heads together and then an opening-up exercise going on, when the Commission of Inquiry was actually deep into its hearings. One of the points we may make in our closing submission is that usually, in prior Commissions of Inquiries in the past few years, one has an undisputed incident or catastrophe, such as a ship collision or lead found in drinking water, where nobody is seriously disputing what actually happened, so people can meaningfully find out why it happened, with no one having any particular axe to grind; whereas now we are obviously having a rather different animal.	5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	raised by the terms of reference, which actually are referable back to allegations made way back in May, as publicised by the media. MR SO: Mr Chairman, if I may respond. CHAIRMAN: Yes. MR SO: I have two points to address. First is in regards to Mr Boulding's observation as per whether there would be allegations on the part of in particular China Technology as to whether there are failures in supervisory plan. As far as I'm concerned, I'm not trying to make submission or giving evidence from the bar table, but insofar as we read the evidence of Prof Yeung and read the evidence of Mr Paulino Lim from BOSA in collective terms, it seems that the butt-to-butt requirement would effectively be satisfied if the requirement of BOSA that no more than two threads are being exposed. So, in effect, the supervision would have been done without the need of, say, what Mr Boulding is suggesting, x-ray

Works	at the Hung Hom Station Extension under the Shatin to Central Link Project		Day 4
	Page 93		Page 95
1	evidence.	1	Inquiry; that is the opening-up exercise and that has
2	But insofar as the second point I wish to address,	2	raised new issues.
3	regarding whether we are shifting focus on the terms of	3	I think for us to say, "Sorry, it's not really part
4	reference, I wish to quote a small bit of transcript.	4	of our terms of reference as we saw them originally" is
5	If I may be so bold as to invite the Commission to look	5	not acceptable. The fact of the matter is the public
6	at Day 8 of the transcript, page 97, at lines 8 to 18.	6	expects us to consider all matters that are relevant to
7	This is the cross-examination of Mr Pennicott, counsel	7	safety of the structures within the terms of reference,
8	for the Commission, against Mr Jason Poon.	8	and if it means that we have to spend a bit more time
9	There Mr Poon deliberately made clear that:	9	calling back some witnesses or looking at new aspects of
10	"For T40 table, above that T40 table, it's clear,	10	evidence in order to satisfy ourselves, then that we
11	external thread tolerance is 4mm, right, and metric	11	will have to do. I think the public would quite rightly
12	thread per pitch, that means for every thread, every	12	believe that they had been severely let down by this
13	circle of thread, the distance is 40.5 metric times	13	Commission if we were to deal with cut rebars and
14	4 millimetres. That means this table already tells	14	despite the public concern say nothing about the
15	you this is the table approved by BD, it's telling	15	opening-up issues that have arisen.
16	you that in the other paper of BOSA, to say that we	16	So I think I make myself quite clear there.
17	could leave out two or three threads and that's already	17	If it means we have to burn the midnight oil, then
18	outside the tolerance limit, if the tolerance limit is	18	we will have to do that, or if it means that because the
19	just one thread or no more than one thread, the pitch,	19	matter becomes one of central importance to this Inquiry
20	crest to crest, that is."	20	and we ourselves are not able properly to submit our
21	Now, of course the terminology adopted by Mr Poon is	21	report to the Chief Executive until we are better
22	"crest to crest". As for now, we are mentioning a new	22	informed on this issue of opening-up, then we will have
23	term, "butt-to-butt". But I must say, this term or this	23	to inform the Chief Executive of that fact. We are not
24	allegation made by China Technology is in no way out of	24	going to be found wanting in our desire to give to the
25	the blue, neither are involved parties being ambushed.	25	public a full report because the report is due in in
	Page 94		Page 96
1	This is clearly being revealed in the course of the	1	a week's time when we could easily put it in in three
2	evidence that this Commission has heard. Therefore,	2	weeks' time, for example. Quite clearly, the public
3	I would, in my most respectful submission, say the	3	will want they are happy to wait an extra two weeks
4	Commission will not taken by surprise that there is such	4	and get a proper report.
5	an allegation that threads are now not fully engaged or	5	That's our view on that.
6	fully threaded into the couplers. That evidence is	6	That said, we share the concerns that this has
7	clear there and I leave the evidence there until we make	7	arisen so late in the day and we will make sure that we
8	further submissions in our closing. Thank you.	8	can properly deal with it so that everybody, all the
9	MR BOULDING: Sir, I will just observe that when the phrase	9	parties that appear here, are given a full and fair
10	"crest to crest" is being used, it's being used in the	10	hearing. That includes the government and includes MTR
11	context of the thread and the pitch. It's not being	11	and Leighton, as well as the sub-contractors.
12	used in the sense of butt-to-butt.	12	So we will proceed on that basis. It may well be,
13	CHAIRMAN: Yes. Thank you.	13	of course and let me say this emphatically that
14	The position as I see it and I don't have the	14	while we have given absolute weight and will consider
15	terms of reference directly in front of me is	15	most anxiously the reports of the two experts who have
16	essentially and primarily that we have to conduct	16	already given evidence before the Commission, there are
17	an inquiry in order to be satisfied that the structures	17	three more experts still to give evidence, and it's our
18	which are subject of the inquiry are safe.	18	duty to be able to assess all of that expert evidence,
19	It is, of course, regrettable that this issue of	19	and it may well colour our view as we proceed.
20	butt-to-butt or this issue of embedment and/or	20	One of the reasons why Prof Hansford sits on this
21	engagement of the rebars into the couplers should have	21	Commission of Inquiry is because it was accepted by
22	arisen so late in the day. It has arisen, from what we	22	those who constituted this Inquiry that somebody of
23	can see, because of an independent and collateral set of	23	international eminence in engineering matters, both as
24	proceedings, entirely legitimate and very helpful in	24	to structural matters and as to project management
25	themselves, conducted outside of the Commission of	25	matters, must sit with me.

	Page 97		Page 99
1	So clearly, all of these issues fall under our ambit	1	Do you have anything you wish to say or change or
2	and all will be considered. I don't think I need to say	2	add to the phrase "would have been caused"?
3	anything further. I think we all know where we stand.	3	A. Yes. I think perhaps the sentence should start, "This
4	But we will keep a running eye on this and see how we	4	could have been caused by an out-of-tolerance
5	can assist. We ourselves may wish to have somebody	5	installation". So simply the substitution of "could"
6	called back to give more evidence. We don't know.	6	instead of "would".
7	MR SHIEH: Mr Chairman and Professor, may I next call our	7	Q. To follow up on that, in the context of the report and
8	expert for Leighton, Nick Southward.	8	the purpose of the report, were you intending to be
9	MR NICHOLAS JOHAN SOUTHWARD (sworn)	9	judgmental or fault-attributing in that particular
10	Examination-in-chief by MR SHIEH	10	sentence?
11	Q. Mr Southward, can I trouble you to look at the expert	11	A. Absolutely not. That's not part of my brief.
12	bundle in front of you, tab 5. You can see that is	12	Q. Next, can I ask you to look at internal page 49 of 53.
13	a report entitled "MTRCL Shatin to Central Link	13	Yes?
14	contract 1112, Hung Hom Station & stabling sidings,	14	A. Yes.
15	change of details at eastern diaphragm walls and slabs";	15	Q. There is a reference at the top of the page to:
16	do you see that?	16	"The relationship between characteristic yield
17	A. Yes.	17	strength and ultimate tensile strength may be
18	Q. Usually in these expert reports one looks at the signing	18	conservatively taken as 5 per cent."
19	page, and in this particular case we see that at the	19	Now, do you have anything to change or to add, to
20	next page, internal page 2.	20	say in respect of that sentence?
21	A. Yes.	21	A. Yes. This unfortunately is a typographic error and
22	Q. That is your signature there?	22	really it should say "20 per cent" in this context.
23	A. Yes.	23	COMMISSIONER HANSFORD: So the 5 should be a 20?
24	Q. What follows is a table of contents, and all the way	24	A. So the 5 should be a 20, yes.
25	down to the final page, page 83, consists of your report	25	MR SHIEH: Does that have any consequential effect on any
	Page 98		Page 100
1	Page 98 and its various appendices attached?	1	Page 100 part of the numbers in this report?
1 2		1 2	
	and its various appendices attached? A. (Nodded head). COMMISSIONER HANSFORD: Page 83?		part of the numbers in this report? A. It does, yes. So the next single line which says: "Thus the minimum fracture load allowed for a bar
2	and its various appendices attached? A. (Nodded head). COMMISSIONER HANSFORD: Page 83? MR SHIEH: 53, sorry.	2	part of the numbers in this report? A. It does, yes. So the next single line which says:
2 3	and its various appendices attached? A. (Nodded head). COMMISSIONER HANSFORD: Page 83?	2 3	part of the numbers in this report? A. It does, yes. So the next single line which says: "Thus the minimum fracture load allowed for a bar
2 3 4	and its various appendices attached? A. (Nodded head). COMMISSIONER HANSFORD: Page 83? MR SHIEH: 53, sorry. COMMISSIONER HANSFORD: It's 53 plus appendices. MR SHIEH: 53 is the end of the report itself. 83 would be	2 3 4	<ul><li>part of the numbers in this report?</li><li>A. It does, yes. So the next single line which says:</li><li>"Thus the minimum fracture load allowed for a bar coupler assembly"</li><li>The value should be 727, not 636.</li><li>Q. 727?</li></ul>
2 3 4 5 6 7	<ul> <li>and its various appendices attached?</li> <li>A. (Nodded head).</li> <li>COMMISSIONER HANSFORD: Page 83?</li> <li>MR SHIEH: 53, sorry.</li> <li>COMMISSIONER HANSFORD: It's 53 plus appendices.</li> <li>MR SHIEH: 53 is the end of the report itself. 83 would be the end of everything else, so when I said all the way</li> </ul>	2 3 4 5	<ul> <li>part of the numbers in this report?</li> <li>A. It does, yes. So the next single line which says:</li> <li>"Thus the minimum fracture load allowed for a bar coupler assembly"</li> <li>The value should be 727, not 636.</li> <li>Q. 727?</li> <li>A. Yes.</li> </ul>
2 3 4 5 6 7 8	<ul> <li>and its various appendices attached?</li> <li>A. (Nodded head).</li> <li>COMMISSIONER HANSFORD: Page 83?</li> <li>MR SHIEH: 53, sorry.</li> <li>COMMISSIONER HANSFORD: It's 53 plus appendices.</li> <li>MR SHIEH: 53 is the end of the report itself. 83 would be the end of everything else, so when I said all the way down to 83, I did say the report and the appendices.</li> </ul>	2 3 4 5 6 7 8	<ul> <li>part of the numbers in this report?</li> <li>A. It does, yes. So the next single line which says:</li> <li>"Thus the minimum fracture load allowed for a bar coupler assembly"</li> <li>The value should be 727, not 636.</li> <li>Q. 727?</li> <li>A. Yes.</li> <li>Q. Thank you.</li> </ul>
2 3 4 5 6 7 8 9	<ul> <li>and its various appendices attached?</li> <li>A. (Nodded head).</li> <li>COMMISSIONER HANSFORD: Page 83?</li> <li>MR SHIEH: 53, sorry.</li> <li>COMMISSIONER HANSFORD: It's 53 plus appendices.</li> <li>MR SHIEH: 53 is the end of the report itself. 83 would be the end of everything else, so when I said all the way down to 83, I did say the report and the appendices.</li> <li>COMMISSIONER HANSFORD: I understand, it's just I don't have</li> </ul>	2 3 4 5 6 7 8 9	<ul> <li>part of the numbers in this report?</li> <li>A. It does, yes. So the next single line which says: <ul> <li>"Thus the minimum fracture load allowed for a bar coupler assembly"</li> <li>The value should be 727, not 636.</li> </ul> </li> <li>Q. 727?</li> <li>A. Yes.</li> <li>Q. Thank you. <ul> <li>Subject to these two comments and changes, you put</li> </ul> </li> </ul>
2 3 4 5 6 7 8 9 10	<ul> <li>and its various appendices attached?</li> <li>A. (Nodded head).</li> <li>COMMISSIONER HANSFORD: Page 83?</li> <li>MR SHIEH: 53, sorry.</li> <li>COMMISSIONER HANSFORD: It's 53 plus appendices.</li> <li>MR SHIEH: 53 is the end of the report itself. 83 would be the end of everything else, so when I said all the way down to 83, I did say the report and the appendices.</li> <li>COMMISSIONER HANSFORD: I understand, it's just I don't have the pages numbered after 53. They are just appendix</li> </ul>	2 3 4 5 6 7 8 9 10	<ul> <li>part of the numbers in this report?</li> <li>A. It does, yes. So the next single line which says: <ul> <li>"Thus the minimum fracture load allowed for a bar coupler assembly"</li> <li>The value should be 727, not 636.</li> </ul> </li> <li>Q. 727?</li> <li>A. Yes.</li> <li>Q. Thank you. <ul> <li>Subject to these two comments and changes, you put forward your report as evidence in this Commission of</li> </ul> </li> </ul>
2 3 4 5 6 7 8 9 10 11	<ul> <li>and its various appendices attached?</li> <li>A. (Nodded head).</li> <li>COMMISSIONER HANSFORD: Page 83?</li> <li>MR SHIEH: 53, sorry.</li> <li>COMMISSIONER HANSFORD: It's 53 plus appendices.</li> <li>MR SHIEH: 53 is the end of the report itself. 83 would be the end of everything else, so when I said all the way down to 83, I did say the report and the appendices.</li> <li>COMMISSIONER HANSFORD: I understand, it's just I don't have the pages numbered after 53. They are just appendix numbers.</li> </ul>	2 3 4 5 6 7 8 9 10 11	<ul> <li>part of the numbers in this report?</li> <li>A. It does, yes. So the next single line which says: <ul> <li>"Thus the minimum fracture load allowed for a bar coupler assembly"</li> <li>The value should be 727, not 636.</li> </ul> </li> <li>Q. 727?</li> <li>A. Yes.</li> <li>Q. Thank you. <ul> <li>Subject to these two comments and changes, you put forward your report as evidence in this Commission of Inquiry?</li> </ul> </li> </ul>
2 3 4 5 6 7 8 9 10 11 12	<ul> <li>and its various appendices attached?</li> <li>A. (Nodded head).</li> <li>COMMISSIONER HANSFORD: Page 83?</li> <li>MR SHIEH: 53, sorry.</li> <li>COMMISSIONER HANSFORD: It's 53 plus appendices.</li> <li>MR SHIEH: 53 is the end of the report itself. 83 would be the end of everything else, so when I said all the way down to 83, I did say the report and the appendices.</li> <li>COMMISSIONER HANSFORD: I understand, it's just I don't have the pages numbered after 53. They are just appendix numbers.</li> <li>MR SHIEH: I'm sorry.</li> </ul>	2 3 4 5 6 7 8 9 10 11 12	<ul> <li>part of the numbers in this report?</li> <li>A. It does, yes. So the next single line which says: <ul> <li>"Thus the minimum fracture load allowed for a bar coupler assembly"</li> <li>The value should be 727, not 636.</li> </ul> </li> <li>Q. 727?</li> <li>A. Yes.</li> <li>Q. Thank you. <ul> <li>Subject to these two comments and changes, you put forward your report as evidence in this Commission of Inquiry?</li> </ul> </li> <li>A. Yes.</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13	<ul> <li>and its various appendices attached?</li> <li>A. (Nodded head).</li> <li>COMMISSIONER HANSFORD: Page 83?</li> <li>MR SHIEH: 53, sorry.</li> <li>COMMISSIONER HANSFORD: It's 53 plus appendices.</li> <li>MR SHIEH: 53 is the end of the report itself. 83 would be the end of everything else, so when I said all the way down to 83, I did say the report and the appendices.</li> <li>COMMISSIONER HANSFORD: I understand, it's just I don't have the pages numbered after 53. They are just appendix numbers.</li> <li>MR SHIEH: I'm sorry.</li> <li>Mr Southward, before I ask you to formally put</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13	<ul> <li>part of the numbers in this report?</li> <li>A. It does, yes. So the next single line which says: <ul> <li>"Thus the minimum fracture load allowed for a bar coupler assembly"</li> <li>The value should be 727, not 636.</li> </ul> </li> <li>Q. 727? <ul> <li>A. Yes.</li> </ul> </li> <li>Q. Thank you. <ul> <li>Subject to these two comments and changes, you put forward your report as evidence in this Commission of Inquiry?</li> </ul> </li> <li>A. Yes.</li> <li>Q. Mr Southward, I understand you have prepared some slides</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14	<ul> <li>and its various appendices attached?</li> <li>A. (Nodded head).</li> <li>COMMISSIONER HANSFORD: Page 83?</li> <li>MR SHIEH: 53, sorry.</li> <li>COMMISSIONER HANSFORD: It's 53 plus appendices.</li> <li>MR SHIEH: 53 is the end of the report itself. 83 would be the end of everything else, so when I said all the way down to 83, I did say the report and the appendices.</li> <li>COMMISSIONER HANSFORD: I understand, it's just I don't have the pages numbered after 53. They are just appendix numbers.</li> <li>MR SHIEH: I'm sorry.</li> <li>Mr Southward, before I ask you to formally put forward your expert report as evidence and also to</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14	<ul> <li>part of the numbers in this report?</li> <li>A. It does, yes. So the next single line which says: <ul> <li>"Thus the minimum fracture load allowed for a bar coupler assembly"</li> <li>The value should be 727, not 636.</li> </ul> </li> <li>Q. 727?</li> <li>A. Yes.</li> <li>Q. Thank you. <ul> <li>Subject to these two comments and changes, you put forward your report as evidence in this Commission of Inquiry?</li> </ul> </li> <li>A. Yes.</li> <li>Q. Mr Southward, I understand you have prepared some slides and an oral presentation summarising the evidence, so</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15	<ul> <li>and its various appendices attached?</li> <li>A. (Nodded head).</li> <li>COMMISSIONER HANSFORD: Page 83?</li> <li>MR SHIEH: 53, sorry.</li> <li>COMMISSIONER HANSFORD: It's 53 plus appendices.</li> <li>MR SHIEH: 53 is the end of the report itself. 83 would be the end of everything else, so when I said all the way down to 83, I did say the report and the appendices.</li> <li>COMMISSIONER HANSFORD: I understand, it's just I don't have the pages numbered after 53. They are just appendix numbers.</li> <li>MR SHIEH: I'm sorry.</li> <li>Mr Southward, before I ask you to formally put forward your expert report as evidence and also to deliver your synopsis orally, can I just take you to two</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15	<ul> <li>part of the numbers in this report?</li> <li>A. It does, yes. So the next single line which says: <ul> <li>"Thus the minimum fracture load allowed for a bar coupler assembly"</li> <li>The value should be 727, not 636.</li> </ul> </li> <li>Q. 727?</li> <li>A. Yes.</li> <li>Q. Thank you. <ul> <li>Subject to these two comments and changes, you put forward your report as evidence in this Commission of Inquiry?</li> </ul> </li> <li>A. Yes.</li> <li>Q. Mr Southward, I understand you have prepared some slides and an oral presentation summarising the evidence, so may I now invite you to start your presentation.</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	<ul> <li>and its various appendices attached?</li> <li>A. (Nodded head).</li> <li>COMMISSIONER HANSFORD: Page 83?</li> <li>MR SHIEH: 53, sorry.</li> <li>COMMISSIONER HANSFORD: It's 53 plus appendices.</li> <li>MR SHIEH: 53 is the end of the report itself. 83 would be the end of everything else, so when I said all the way down to 83, I did say the report and the appendices.</li> <li>COMMISSIONER HANSFORD: I understand, it's just I don't have the pages numbered after 53. They are just appendix numbers.</li> <li>MR SHIEH: I'm sorry.</li> <li>Mr Southward, before I ask you to formally put forward your expert report as evidence and also to deliver your synopsis orally, can I just take you to two points in your report.</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	<ul> <li>part of the numbers in this report?</li> <li>A. It does, yes. So the next single line which says: <ul> <li>"Thus the minimum fracture load allowed for a bar coupler assembly"</li> <li>The value should be 727, not 636.</li> </ul> </li> <li>Q. 727?</li> <li>A. Yes.</li> <li>Q. Thank you. <ul> <li>Subject to these two comments and changes, you put forward your report as evidence in this Commission of Inquiry?</li> </ul> </li> <li>A. Yes.</li> <li>Q. Mr Southward, I understand you have prepared some slides and an oral presentation summarising the evidence, so may I now invite you to start your presentation.</li> <li>CHAIRMAN: If we could just hear a bit about yourself.</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	<ul> <li>and its various appendices attached?</li> <li>A. (Nodded head).</li> <li>COMMISSIONER HANSFORD: Page 83?</li> <li>MR SHIEH: 53, sorry.</li> <li>COMMISSIONER HANSFORD: It's 53 plus appendices.</li> <li>MR SHIEH: 53 is the end of the report itself. 83 would be the end of everything else, so when I said all the way down to 83, I did say the report and the appendices.</li> <li>COMMISSIONER HANSFORD: I understand, it's just I don't have the pages numbered after 53. They are just appendix numbers.</li> <li>MR SHIEH: I'm sorry.</li> <li>Mr Southward, before I ask you to formally put forward your expert report as evidence and also to deliver your synopsis orally, can I just take you to two points in your report.</li> <li>First of all, can I ask you to look at</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	<ul> <li>part of the numbers in this report?</li> <li>A. It does, yes. So the next single line which says: <ul> <li>"Thus the minimum fracture load allowed for a bar coupler assembly"</li> <li>The value should be 727, not 636.</li> </ul> </li> <li>Q. 727? <ul> <li>A. Yes.</li> </ul> </li> <li>Q. Thank you. <ul> <li>Subject to these two comments and changes, you put forward your report as evidence in this Commission of Inquiry?</li> </ul> </li> <li>A. Yes.</li> <li>Q. Mr Southward, I understand you have prepared some slides and an oral presentation summarising the evidence, so may I now invite you to start your presentation.</li> <li>CHAIRMAN: If we could just hear a bit about yourself.</li> <li>A. I have the words.</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	<ul> <li>and its various appendices attached?</li> <li>A. (Nodded head).</li> <li>COMMISSIONER HANSFORD: Page 83?</li> <li>MR SHIEH: 53, sorry.</li> <li>COMMISSIONER HANSFORD: It's 53 plus appendices.</li> <li>MR SHIEH: 53 is the end of the report itself. 83 would be the end of everything else, so when I said all the way down to 83, I did say the report and the appendices.</li> <li>COMMISSIONER HANSFORD: I understand, it's just I don't have the pages numbered after 53. They are just appendix numbers.</li> <li>MR SHIEH: I'm sorry.</li> <li>Mr Southward, before I ask you to formally put forward your expert report as evidence and also to deliver your synopsis orally, can I just take you to two points in your report.</li> <li>First of all, can I ask you to look at paragraph 7.4.3. That's where you dealt with technical</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	<ul> <li>part of the numbers in this report?</li> <li>A. It does, yes. So the next single line which says: <ul> <li>"Thus the minimum fracture load allowed for a bar coupler assembly"</li> <li>The value should be 727, not 636.</li> </ul> </li> <li>Q. 727?</li> <li>A. Yes.</li> <li>Q. Thank you. <ul> <li>Subject to these two comments and changes, you put forward your report as evidence in this Commission of Inquiry?</li> </ul> </li> <li>A. Yes.</li> <li>Q. Mr Southward, I understand you have prepared some slides and an oral presentation summarising the evidence, so may I now invite you to start your presentation.</li> <li>CHAIRMAN: If we could just hear a bit about yourself.</li> <li>A. I have the words.</li> <li>CHAIRMAN: Thank you very much.</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	<ul> <li>and its various appendices attached?</li> <li>A. (Nodded head).</li> <li>COMMISSIONER HANSFORD: Page 83?</li> <li>MR SHIEH: 53, sorry.</li> <li>COMMISSIONER HANSFORD: It's 53 plus appendices.</li> <li>MR SHIEH: 53 is the end of the report itself. 83 would be the end of everything else, so when I said all the way down to 83, I did say the report and the appendices.</li> <li>COMMISSIONER HANSFORD: I understand, it's just I don't have the pages numbered after 53. They are just appendix numbers.</li> <li>MR SHIEH: I'm sorry.</li> <li>Mr Southward, before I ask you to formally put forward your expert report as evidence and also to deliver your synopsis orally, can I just take you to two points in your report.</li> <li>First of all, can I ask you to look at paragraph 7.4.3. That's where you dealt with technical query no. 34; do you see that? It's internal page 18</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	<ul> <li>part of the numbers in this report?</li> <li>A. It does, yes. So the next single line which says: <ul> <li>"Thus the minimum fracture load allowed for a bar coupler assembly"</li> <li>The value should be 727, not 636.</li> </ul> </li> <li>Q. 727?</li> <li>A. Yes.</li> <li>Q. Thank you. <ul> <li>Subject to these two comments and changes, you put forward your report as evidence in this Commission of Inquiry?</li> </ul> </li> <li>A. Yes.</li> <li>Q. Mr Southward, I understand you have prepared some slides and an oral presentation summarising the evidence, so may I now invite you to start your presentation.</li> <li>CHAIRMAN: If we could just hear a bit about yourself.</li> <li>A. I have the words.</li> <li>CHAIRMAN: Thank you very much.</li> <li>A. Mr Chairman and Prof Hansford, my name is Nick</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	<ul> <li>and its various appendices attached?</li> <li>A. (Nodded head).</li> <li>COMMISSIONER HANSFORD: Page 83?</li> <li>MR SHIEH: 53, sorry.</li> <li>COMMISSIONER HANSFORD: It's 53 plus appendices.</li> <li>MR SHIEH: 53 is the end of the report itself. 83 would be the end of everything else, so when I said all the way down to 83, I did say the report and the appendices.</li> <li>COMMISSIONER HANSFORD: I understand, it's just I don't have the pages numbered after 53. They are just appendix numbers.</li> <li>MR SHIEH: I'm sorry.</li> <li>Mr Southward, before I ask you to formally put forward your expert report as evidence and also to deliver your synopsis orally, can I just take you to two points in your report.</li> <li>First of all, can I ask you to look at paragraph 7.4.3. That's where you dealt with technical query no. 34; do you see that?</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	<ul> <li>part of the numbers in this report?</li> <li>A. It does, yes. So the next single line which says: <ul> <li>"Thus the minimum fracture load allowed for a bar coupler assembly"</li> <li>The value should be 727, not 636.</li> </ul> </li> <li>Q. 727? <ul> <li>A. Yes.</li> </ul> </li> <li>Q. Thank you. <ul> <li>Subject to these two comments and changes, you put forward your report as evidence in this Commission of Inquiry?</li> </ul> </li> <li>A. Yes.</li> <li>Q. Mr Southward, I understand you have prepared some slides and an oral presentation summarising the evidence, so may I now invite you to start your presentation.</li> <li>CHAIRMAN: If we could just hear a bit about yourself.</li> <li>A. I have the words.</li> <li>CHAIRMAN: Thank you very much.</li> </ul> <li>A. Mr Chairman and Prof Hansford, my name is Nick Southward. I am an executive director of Tony Gee and</li>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	<ul> <li>and its various appendices attached?</li> <li>A. (Nodded head).</li> <li>COMMISSIONER HANSFORD: Page 83?</li> <li>MR SHIEH: 53, sorry.</li> <li>COMMISSIONER HANSFORD: It's 53 plus appendices.</li> <li>MR SHIEH: 53 is the end of the report itself. 83 would be the end of everything else, so when I said all the way down to 83, I did say the report and the appendices.</li> <li>COMMISSIONER HANSFORD: I understand, it's just I don't have the pages numbered after 53. They are just appendix numbers.</li> <li>MR SHIEH: I'm sorry.</li> <li>Mr Southward, before I ask you to formally put forward your expert report as evidence and also to deliver your synopsis orally, can I just take you to two points in your report.</li> <li>First of all, can I ask you to look at paragraph 7.4.3. That's where you dealt with technical query no. 34; do you see that? It's internal page 18 of 53; do you see that?</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	<ul> <li>part of the numbers in this report?</li> <li>A. It does, yes. So the next single line which says: <ul> <li>"Thus the minimum fracture load allowed for a bar coupler assembly"</li> <li>The value should be 727, not 636.</li> </ul> </li> <li>Q. 727?</li> <li>A. Yes.</li> <li>Q. Thank you. <ul> <li>Subject to these two comments and changes, you put forward your report as evidence in this Commission of Inquiry?</li> </ul> </li> <li>A. Yes.</li> <li>Q. Mr Southward, I understand you have prepared some slides and an oral presentation summarising the evidence, so may I now invite you to start your presentation.</li> <li>CHAIRMAN: If we could just hear a bit about yourself.</li> <li>A. I have the words.</li> <li>CHAIRMAN: Thank you very much.</li> <li>A. Mr Chairman and Prof Hansford, my name is Nick Southward. I am an executive director of Tony Gee and Partners and I am the independent expert appointed to</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>and its various appendices attached?</li> <li>A. (Nodded head).</li> <li>COMMISSIONER HANSFORD: Page 83?</li> <li>MR SHIEH: 53, sorry.</li> <li>COMMISSIONER HANSFORD: It's 53 plus appendices.</li> <li>MR SHIEH: 53 is the end of the report itself. 83 would be the end of everything else, so when I said all the way down to 83, I did say the report and the appendices.</li> <li>COMMISSIONER HANSFORD: I understand, it's just I don't have the pages numbered after 53. They are just appendix numbers.</li> <li>MR SHIEH: I'm sorry.</li> <li>Mr Southward, before I ask you to formally put forward your expert report as evidence and also to deliver your synopsis orally, can I just take you to two points in your report.</li> <li>First of all, can I ask you to look at paragraph 7.4.3. That's where you dealt with technical query no. 34; do you see that?</li> <li>A. Yes.</li> <li>Q. In the second full paragraph, you said:</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>part of the numbers in this report?</li> <li>A. It does, yes. So the next single line which says: <ul> <li>"Thus the minimum fracture load allowed for a bar coupler assembly"</li> <li>The value should be 727, not 636.</li> </ul> </li> <li>Q. 727?</li> <li>A. Yes.</li> <li>Q. Thank you. <ul> <li>Subject to these two comments and changes, you put forward your report as evidence in this Commission of Inquiry?</li> </ul> </li> <li>A. Yes.</li> <li>Q. Mr Southward, I understand you have prepared some slides and an oral presentation summarising the evidence, so may I now invite you to start your presentation.</li> <li>CHAIRMAN: If we could just hear a bit about yourself.</li> <li>A. I have the words.</li> <li>CHAIRMAN: Thank you very much.</li> <li>A. Mr Chairman and Prof Hansford, my name is Nick Southward. I am an executive director of Tony Gee and Partners and I am the independent expert appointed to the Commission of Inquiry on behalf of Leighton.</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	<ul> <li>and its various appendices attached?</li> <li>A. (Nodded head).</li> <li>COMMISSIONER HANSFORD: Page 83?</li> <li>MR SHIEH: 53, sorry.</li> <li>COMMISSIONER HANSFORD: It's 53 plus appendices.</li> <li>MR SHIEH: 53 is the end of the report itself. 83 would be the end of everything else, so when I said all the way down to 83, I did say the report and the appendices.</li> <li>COMMISSIONER HANSFORD: I understand, it's just I don't have the pages numbered after 53. They are just appendix numbers.</li> <li>MR SHIEH: I'm sorry.</li> <li>Mr Southward, before I ask you to formally put forward your expert report as evidence and also to deliver your synopsis orally, can I just take you to two points in your report.</li> <li>First of all, can I ask you to look at paragraph 7.4.3. That's where you dealt with technical query no. 34; do you see that? It's internal page 18 of 53; do you see that?</li> <li>A. Yes.</li> <li>Q. In the second full paragraph, you said: "This would have been caused by an out-of-tolerance</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	<ul> <li>part of the numbers in this report?</li> <li>A. It does, yes. So the next single line which says: <ul> <li>"Thus the minimum fracture load allowed for a bar coupler assembly"</li> <li>The value should be 727, not 636.</li> </ul> </li> <li>Q. 727?</li> <li>A. Yes.</li> <li>Q. Thank you. <ul> <li>Subject to these two comments and changes, you put forward your report as evidence in this Commission of Inquiry?</li> </ul> </li> <li>A. Yes.</li> <li>Q. Mr Southward, I understand you have prepared some slides and an oral presentation summarising the evidence, so may I now invite you to start your presentation.</li> <li>CHAIRMAN: If we could just hear a bit about yourself.</li> <li>A. I have the words.</li> <li>CHAIRMAN: Thank you very much.</li> <li>A. Mr Chairman and Prof Hansford, my name is Nick Southward. I am an executive director of Tony Gee and Partners and I am the independent expert appointed to the Commission of Inquiry on behalf of Leighton. <ul> <li>I would like to thank you both for allowing me to appear</li> </ul> </li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>and its various appendices attached?</li> <li>A. (Nodded head).</li> <li>COMMISSIONER HANSFORD: Page 83?</li> <li>MR SHIEH: 53, sorry.</li> <li>COMMISSIONER HANSFORD: It's 53 plus appendices.</li> <li>MR SHIEH: 53 is the end of the report itself. 83 would be the end of everything else, so when I said all the way down to 83, I did say the report and the appendices.</li> <li>COMMISSIONER HANSFORD: I understand, it's just I don't have the pages numbered after 53. They are just appendix numbers.</li> <li>MR SHIEH: I'm sorry.</li> <li>Mr Southward, before I ask you to formally put forward your expert report as evidence and also to deliver your synopsis orally, can I just take you to two points in your report.</li> <li>First of all, can I ask you to look at paragraph 7.4.3. That's where you dealt with technical query no. 34; do you see that?</li> <li>A. Yes.</li> <li>Q. In the second full paragraph, you said:</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>part of the numbers in this report?</li> <li>A. It does, yes. So the next single line which says: <ul> <li>"Thus the minimum fracture load allowed for a bar coupler assembly"</li> <li>The value should be 727, not 636.</li> </ul> </li> <li>Q. 727?</li> <li>A. Yes.</li> <li>Q. Thank you. <ul> <li>Subject to these two comments and changes, you put forward your report as evidence in this Commission of Inquiry?</li> </ul> </li> <li>A. Yes.</li> <li>Q. Mr Southward, I understand you have prepared some slides and an oral presentation summarising the evidence, so may I now invite you to start your presentation.</li> <li>CHAIRMAN: If we could just hear a bit about yourself.</li> <li>A. I have the words.</li> <li>CHAIRMAN: Thank you very much.</li> <li>A. Mr Chairman and Prof Hansford, my name is Nick Southward. I am an executive director of Tony Gee and Partners and I am the independent expert appointed to the Commission of Inquiry on behalf of Leighton.</li> </ul>

25 (Pages 97 to 100)

	Page 101		Page 103
1	30 years, the last 25 of which I have spent in	1	COMMISSIONER HANSFORD: Thank you.
2	Hong Kong. I have only a small amount of publications	2	A. Next slide, please.
3	and awards to my name because I choose to work at the	3	I'm sure you are all familiar by now with the layout
4	sharp or pointy end of the civil engineering industry,	4	of the station, but to remind, we are talking about the
5	practising real structural design for large civil	5	junction of the upper EWL slab in red and the D-wall on
6	engineering infrastructure projects.	6	the left-hand side in blue. This is circled in yellow
7	I have designed personally some significant	7	on the slide.
8	infrastructure projects in Hong Kong. I typically	8	Next slide, please. This is a 3D graphic which is
9	design structures for contractors, mainly in design and	9	a representation of the reinforcement arrangement at the
10	build situations, so I am skilled in preparing	10	top of a typical D-wall panel. You will see that the
11	cost-effective, practical and buildable designs that	11	EWL slab was to be connected to the D-wall using
12	comply with all rules, regulations and design codes.	12	L-shaped T40 rebars through couplers in the top and
13	I am a chartered civil engineer. I am a fellow of	13	bottom surfaces of the slab. The OTE was connected to
14	the Hong Kong Institution of Engineers. I am a member		the D-wall in a like manner.
15	of the Institution of Civil Engineers in the UK. And	15	Next slide, please. However, for practical
16	I am a registered professional engineer in Hong Kong.	16	construction reasons, the original arrangement of
17	My primary brief has been to look at the Hung Hom	17	reinforcement had to be re-arranged to provide space in
18	Station structure and investigate whether the sequence	18	the middle of the panel for construction equipment to be
19	of events that occurred during construction has had any	19	inserted into its top. As a result, the horizontal bars
20	impact on the overall structural integrity of the	20	at the top of the D-wall panels were re-arranged into
21	station structure, and to advise if, in my opinion, the	21	three layers, to provide a space in the middle. Two
22	structure is safe.	22	layers of rebars, which are the magenta and green
23	I can cut to the chase and advise that in my opinion	23	coloured bars, originally L-shaped, are no longer turned
24	the structure is safe. I will now continue to explain	24	down into the D-wall but are extended to the other face
25	why.	25	of the D-wall, with a coupler at each end, and they are
	Page 102		Page 104
1	There are three key areas which I wish to highlight	1	arranged in two groups of four bars, which provide
2	from my report.	2	a clear space in the middle.
3	Next slide, please. First, on the design change of	3	There is also an additional layer of rebar which is
4	the horizontal reinforcement in the EWL slab from the	4	the yellow bars at the bottom. This is provided so that
5	use of couplers to continuous rebars, my view is that	5	the total number of horizontal bars per panel remained
6	the changed design is stronger and more robust than the	6	unchanged from the original design. All three layers of
7	original accepted design detail. It is compliant with	7	this rebar were planned to be extended into the OTE slab
8	all the relevant design codes, and it is structurally	8	for their anchorage.
9	safe.	9	This was design change number 1 and was submitted
10	Next slide, please. Second, on the length of the	10	and accepted for construction by the Buildings
11	threaded end of the rebars, my opinion is that the	11	Department. This change to the original design had no
12	minimum acceptable embedded length is 26.4 millimetres	12	overall effect on the global stability of the station
13	embedded into the coupler, based on the results of the	13	structure.
14	load tests undertaken so far.	14	Later, it transpired that the position of the
15	Third, my report explains that there is significant	15	horizontal couplers in some isolated D-wall panels were
16	structural redundancy in the design, or in simple terms	16	misaligned. To remedy the problem, it was proposed to
17	spare capacity in the rebar connections. For the top	17	trim off the top portion of the D-wall from the EWL
18	layer of the EWL slab as it connects into the D-wall,	18	slab sorry, to trim off the top portion of the D-wall
19	this is 40 per cent. The bottom layer, 50 per cent.	19	so that bars from the EWL slab could be installed at the
20	But I have to stress that this opinion is based on the	20	correct level. This involved removing the top layer of
21	findings of three separate large engineering consultancy	21	the coupled rebars and replacing them with continuous
22	firms and not my own calculations, as doing those	22	bars.
23	calculations was not part of my brief.	23	These incidents were the precursor for the decision
24	COMMISSIONER HANSFORD: Sorry, and those three firms?		taken to make a minor change to the accepted design as
25	A. Atkins, Arup and COWI.	25	follows.

	Page 105		Page 107
1	Next slide, please. This shows how the top portion	1	In fact, I am of the view that the change marks
2	of the D-wall was trimmed down to expose the transverse	2	an improvement to the design. It increases the amount
3	reinforcement and the couplers.	3	of reinforcement that connects the slab and the wall, so
4	Next slide, please. This slide shows how those bars	4	the structure has an increased amount of strength,
5	and couplers were replaced with two continuous layers of	5	robustness, redundancy, spare capacity. The bending
6	bars which passed over the top of the D-wall from the	6	strength of this EWL slab connection has increased by
7	EWL side and were anchored into the OTE slab in the same		50 per cent from the original design.
8	way as the change 1 design.	8	Next slide, please. The change also eliminates the
9	Now, I have to stress that this is a 3D	9	vertical construction joints at the top, between the EWL
10	representation. It's not meant to show the actual	10	slab, the D-wall and the OTE slab. These interfaces are
11	arrangement of the bars and the lapping that connected	11	points of high stress. And as a matter of good
12	to them. It's just a graphic for illustration.	12	practice, the Hong Kong Code of Practice for Concrete
13	COMMISSIONER HANSFORD: Sure.	13	recommends construction joints are avoided in points of
14	A. So was this change compliant with building codes? Under		high stress. The top section of the joints, which you
15	the Hong Kong Code of Practice for Structural Use of	15	can see on the left-hand side, the top section of those
16	Concrete, both the versions of 2004 and 2013,	16	joints were eliminated by the continuous or monolithic
17	reinforcement continuity in concrete is allowed to be	17	concrete pour across the EWL slab, across the top of the
18	provided using bar laps, welding or couplers. Such	18	D-wall, into the OTE slab.
19	choices are present in all international design codes.	19	Importantly, the construction joint has now been
20	The change, however, from change 1 to change 2, was	20	moved to a horizontal location, embedded within the
21	just a simple matter of substituting straight,	21	overall body of the concrete, and is at a position where
22	continuous bars instead of coupled bars. So it's	22	the stress on that construction joint is lower than that
23	completely compliant with what's allowed, with what is	23	at the original locations.
24	stipulated in the codes.	24	The trimming down of the top of the D-wall did not
25	Next slide, please. This is just a simple,	25	affect its integrity. Such trimming down of the top
	Page 106		Page 108
1	side-by-side illustration of the principal effects of	1	section is no different from the trimming of the section
2	the change. It's just a repeat of the three previous	2	of the over-poured concrete above the top of the D-wall.
3	slides but it shows clearly the order of sequence of the	3	Such trimming was finished by the use of hand-held
4	changes.	4	breakers, which is the accepted practice for preparation
5	Next slide, please. This slide gives us a closer	5	of construction joints.
6	look at how much additional reinforcement has been	6	On the issue of minimum embedded length of threads,
7	placed across the joint. If you count the bars that	7	in my opinion, it is wrong to suggest that the entire
8	cross the D-wall, you will see that they have increased	8	threaded end of a rebar must be screwed into a coupler
9			
	from 24 number on the left to 36 on the right. So the	9	with no visible threads outside.
10	from 24 number on the left to 36 on the right. So the 24 bars on the left are the magenta, green and yellow	9 10	with no visible threads outside. MR PENNICOTT: The next slide?
10 11	24 bars on the left are the magenta, green and yellow	10	MR PENNICOTT: The next slide?
11	24 bars on the left are the magenta, green and yellow bars, and they are now replaced with an increased number	10 11	
11 12	24 bars on the left are the magenta, green and yellow bars, and they are now replaced with an increased number of magenta and green bars on the right.	10	<ul><li>MR PENNICOTT: The next slide?</li><li>A. I'm going to say now, next slide. I wanted to say that bit first.</li></ul>
11 12 13	<ul><li>24 bars on the left are the magenta, green and yellow</li><li>bars, and they are now replaced with an increased number</li><li>of magenta and green bars on the right.</li><li>So what was the effect of the changes? It is my</li></ul>	10 11 12 13	<ul><li>MR PENNICOTT: The next slide?</li><li>A. I'm going to say now, next slide. I wanted to say that bit first.</li><li>Here is the theoretical arrangement of</li></ul>
11 12	<ul><li>24 bars on the left are the magenta, green and yellow bars, and they are now replaced with an increased number of magenta and green bars on the right.</li><li>So what was the effect of the changes? It is my view that the change to use continuous rebars has had no</li></ul>	10 11 12	<ul><li>MR PENNICOTT: The next slide?</li><li>A. I'm going to say now, next slide. I wanted to say that bit first.</li><li>Here is the theoretical arrangement of an 88 millimetre long T40 coupler with reinforcement</li></ul>
11 12 13 14	<ul><li>24 bars on the left are the magenta, green and yellow bars, and they are now replaced with an increased number of magenta and green bars on the right.</li><li>So what was the effect of the changes? It is my view that the change to use continuous rebars has had no effect on the design, performance, behaviour or</li></ul>	10 11 12 13 14	<ul><li>MR PENNICOTT: The next slide?</li><li>A. I'm going to say now, next slide. I wanted to say that bit first.</li><li>Here is the theoretical arrangement of an 88 millimetre long T40 coupler with reinforcement bars screwed into both ends. Theoretically,</li></ul>
11 12 13 14 15	<ul><li>24 bars on the left are the magenta, green and yellow bars, and they are now replaced with an increased number of magenta and green bars on the right.</li><li>So what was the effect of the changes? It is my view that the change to use continuous rebars has had no</li></ul>	10 11 12 13 14 15	<ul> <li>MR PENNICOTT: The next slide?</li> <li>A. I'm going to say now, next slide. I wanted to say that bit first.</li> <li>Here is the theoretical arrangement of an 88 millimetre long T40 coupler with reinforcement bars screwed into both ends. Theoretically, 44 millimetres of each rebar is screwed into the coupler</li> </ul>
11 12 13 14 15 16	<ul><li>24 bars on the left are the magenta, green and yellow</li><li>bars, and they are now replaced with an increased number of magenta and green bars on the right.</li><li>So what was the effect of the changes? It is my view that the change to use continuous rebars has had no effect on the design, performance, behaviour or durability of the EWL slab and the connection to the</li></ul>	10 11 12 13 14 15 16	<ul><li>MR PENNICOTT: The next slide?</li><li>A. I'm going to say now, next slide. I wanted to say that bit first.</li><li>Here is the theoretical arrangement of an 88 millimetre long T40 coupler with reinforcement bars screwed into both ends. Theoretically,</li></ul>
11 12 13 14 15 16 17	<ul> <li>24 bars on the left are the magenta, green and yellow bars, and they are now replaced with an increased number of magenta and green bars on the right.</li> <li>So what was the effect of the changes? It is my view that the change to use continuous rebars has had no effect on the design, performance, behaviour or durability of the EWL slab and the connection to the D-wall. The member sizes, sequence of construction and</li> </ul>	10 11 12 13 14 15 16 17	<ul> <li>MR PENNICOTT: The next slide?</li> <li>A. I'm going to say now, next slide. I wanted to say that bit first.</li> <li>Here is the theoretical arrangement of an 88 millimetre long T40 coupler with reinforcement bars screwed into both ends. Theoretically, 44 millimetres of each rebar is screwed into the coupler on each side, on a butt-to-butt basis. The spacing of</li> </ul>
11 12 13 14 15 16 17 18	<ul> <li>24 bars on the left are the magenta, green and yellow bars, and they are now replaced with an increased number of magenta and green bars on the right.</li> <li>So what was the effect of the changes? It is my view that the change to use continuous rebars has had no effect on the design, performance, behaviour or durability of the EWL slab and the connection to the D-wall. The member sizes, sequence of construction and load parts remain the same. The top reinforcement in</li> </ul>	10 11 12 13 14 15 16 17 18	<ul> <li>MR PENNICOTT: The next slide?</li> <li>A. I'm going to say now, next slide. I wanted to say that bit first.</li> <li>Here is the theoretical arrangement of an 88 millimetre long T40 coupler with reinforcement bars screwed into both ends. Theoretically, 44 millimetres of each rebar is screwed into the coupler on each side, on a butt-to-butt basis. The spacing of the threads is 4 millimetres, so each threaded end has</li> </ul>
11 12 13 14 15 16 17 18 19	<ul> <li>24 bars on the left are the magenta, green and yellow bars, and they are now replaced with an increased number of magenta and green bars on the right.</li> <li>So what was the effect of the changes? It is my view that the change to use continuous rebars has had no effect on the design, performance, behaviour or durability of the EWL slab and the connection to the D-wall. The member sizes, sequence of construction and load parts remain the same. The top reinforcement in the EWL slab remains anchored into the OTE slab as per</li> </ul>	10 11 12 13 14 15 16 17 18 19	<ul> <li>MR PENNICOTT: The next slide?</li> <li>A. I'm going to say now, next slide. I wanted to say that bit first.</li> <li>Here is the theoretical arrangement of an 88 millimetre long T40 coupler with reinforcement bars screwed into both ends. Theoretically, 44 millimetres of each rebar is screwed into the coupler on each side, on a butt-to-butt basis. The spacing of the threads is 4 millimetres, so each threaded end has 10/11 threads inside the coupler. That depends on the</li> </ul>
11 12 13 14 15 16 17 18 19 20	<ul> <li>24 bars on the left are the magenta, green and yellow bars, and they are now replaced with an increased number of magenta and green bars on the right.</li> <li>So what was the effect of the changes? It is my view that the change to use continuous rebars has had no effect on the design, performance, behaviour or durability of the EWL slab and the connection to the D-wall. The member sizes, sequence of construction and load parts remain the same. The top reinforcement in the EWL slab remains anchored into the OTE slab as per the change 1 design. The deletion of couplers at the</li> </ul>	10 11 12 13 14 15 16 17 18 19 20	<ul> <li>MR PENNICOTT: The next slide?</li> <li>A. I'm going to say now, next slide. I wanted to say that bit first.</li> <li>Here is the theoretical arrangement of an 88 millimetre long T40 coupler with reinforcement bars screwed into both ends. Theoretically, 44 millimetres of each rebar is screwed into the coupler on each side, on a butt-to-butt basis. The spacing of the threads is 4 millimetres, so each threaded end has 10/11 threads inside the coupler. That depends on the discussion we had yesterday about how much of the</li> </ul>
11 12 13 14 15 16 17 18 19 20 21	24 bars on the left are the magenta, green and yellow bars, and they are now replaced with an increased number of magenta and green bars on the right. So what was the effect of the changes? It is my view that the change to use continuous rebars has had no effect on the design, performance, behaviour or durability of the EWL slab and the connection to the D-wall. The member sizes, sequence of construction and load parts remain the same. The top reinforcement in the EWL slab remains anchored into the OTE slab as per the change 1 design. The deletion of couplers at the top level of the D-wall has no effect on the tension	10 11 12 13 14 15 16 17 18 19 20 21	<ul> <li>MR PENNICOTT: The next slide?</li> <li>A. I'm going to say now, next slide. I wanted to say that bit first.</li> <li>Here is the theoretical arrangement of <ul> <li>an 88 millimetre long T40 coupler with reinforcement</li> <li>bars screwed into both ends. Theoretically,</li> <li>44 millimetres of each rebar is screwed into the coupler</li> <li>on each side, on a butt-to-butt basis. The spacing of</li> <li>the threads is 4 millimetres, so each threaded end has</li> <li>10/11 threads inside the coupler. That depends on the</li> <li>discussion we had yesterday about how much of the</li> </ul> </li> </ul>
111 12 13 14 15 16 17 18 19 20 21 22	24 bars on the left are the magenta, green and yellow bars, and they are now replaced with an increased number of magenta and green bars on the right. So what was the effect of the changes? It is my view that the change to use continuous rebars has had no effect on the design, performance, behaviour or durability of the EWL slab and the connection to the D-wall. The member sizes, sequence of construction and load parts remain the same. The top reinforcement in the EWL slab remains anchored into the OTE slab as per the change 1 design. The deletion of couplers at the top level of the D-wall has no effect on the tension forces in the bars or the manner in which those forces	10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>MR PENNICOTT: The next slide?</li> <li>A. I'm going to say now, next slide. I wanted to say that bit first.</li> <li>Here is the theoretical arrangement of an 88 millimetre long T40 coupler with reinforcement bars screwed into both ends. Theoretically, 44 millimetres of each rebar is screwed into the coupler on each side, on a butt-to-butt basis. The spacing of the threads is 4 millimetres, so each threaded end has 10/11 threads inside the coupler. That depends on the discussion we had yesterday about how much of the chamfer is present.</li> <li>However, BOSA has confirmed that it usually adds</li> </ul>
11 12 13 14 15 16 17 18 19 20 21 22 23	24 bars on the left are the magenta, green and yellow bars, and they are now replaced with an increased number of magenta and green bars on the right. So what was the effect of the changes? It is my view that the change to use continuous rebars has had no effect on the design, performance, behaviour or durability of the EWL slab and the connection to the D-wall. The member sizes, sequence of construction and load parts remain the same. The top reinforcement in the EWL slab remains anchored into the OTE slab as per the change 1 design. The deletion of couplers at the top level of the D-wall has no effect on the tension forces in the bars or the manner in which those forces are anchored into the OTE slab concrete. The bending	10 11 12 13 14 15 16 17 18 19 20 21 22 23	<ul> <li>MR PENNICOTT: The next slide?</li> <li>A. I'm going to say now, next slide. I wanted to say that bit first.</li> <li>Here is the theoretical arrangement of <ul> <li>an 88 millimetre long T40 coupler with reinforcement</li> <li>bars screwed into both ends. Theoretically,</li> <li>44 millimetres of each rebar is screwed into the coupler</li> <li>on each side, on a butt-to-butt basis. The spacing of</li> <li>the threads is 4 millimetres, so each threaded end has</li> <li>10/11 threads inside the coupler. That depends on the</li> <li>discussion we had yesterday about how much of the</li> <li>chamfer is present.</li> <li>However, BOSA has confirmed that it usually adds</li> </ul> </li> </ul>

	Page 109		Page 111
1	Next slide, please. Normally, the coupler is fully	1	For me, looking at it from the perspective of the
2	screwed on to the parent bar, that is the bar in the	2	structural safety of the coupler assembly, I'm actually
3	D-wall that the coupler is first attached to prior to	3	pleased to see that the largest failure load was with
4	the D-wall construction, as we can see from BOSA's own		60 per cent thread engagement. I say this because it
5	illustration.	5	proves that screwing the bar into the coupler more than
6	Coupled with BOSA's description that a maximum of	6	60 per cent has no effect on the strength of the coupler
7	two visible threads outside a coupler is allowed for	7	assembly. At 60 per cent engagement, the bar outside
8	proper installation, this may result in the continuing	8	the coupler broke first. At 70 per cent engagement, the
9	rebar having an embedment length of 36 millimetres.	9	bar outside broke. At 100 per cent engagement, the bar
10	Next slide, please. This slide shows, on the left	10	outside broke first. So once the bar is screwed into
11	side, a continuation bar with a 44 millimetre threaded	11	the coupler by 60 per cent, the threads in that
12	end, screwed correctly into the coupler, with two	12	60 per cent embedment are stronger than the bar.
13	visible threads outside. It shows that the bars are not	13	This is evidenced quite clearly in calculation by
14	butt-to-butt. In this sketch, the gap is 4 millimetres.	14	the contents of appendix V of Prof McQuillan's report,
15	But if the parent bar on the right had been threaded	15	which shows the BOSA thread strength calculation table.
16	with a zero tolerance, then the gap would be	16	We have seen that table a lot as well.
17	8 millimetres.	17	You can see in this table that the theoretical
18	I am not showing this sketch with the intention of	18	strength of the combined threads, as you increase as
19	discussing the number of threads engaged inside the	19	you add more and more threads to the calculation,
20	coupler. I refer solely to the embedded length, because	20	between six number and tend threads, the combined
21	we could use this as a comparison for the opening-up	21	strength increases linearly from 601MPa to 1,002MPa.
22	test results, which measure embedment length, not	22	That's just the strength of the threads. But that
23	engagement threads.	23	increase in threads does nothing for the bar, which has
24	The upshot is that BOSA allowed two exposed threads	24	a lower tensile strength of 529MPa and is therefore
25	in their tolerances, and because of that fact the	25	doomed to failure as soon as the number of threads are
	Page 110		Page 112
1	minimum embedment length could not be greater than	1	six and above.
2	36 millimetres.	2	We also discussed this this morning, when Prof Yeung
3	Next slide, please. This is just a side issue but	3	was queried on his slide, and there was a discussion
4	this shows the same sketch, redrawn, but the	4	about the linear line of that graph, and if that chart
5	continuation bar now has a threaded length of	5	was plotted correctly that one there then the
6	48 millimetres, but is still embedded by 36. This shows	6	experimental test results would be plotted above the
7	how it's possible to have three exposed threads showing	7	line by a healthy margin. It's about 30 per cent.
8	on the continuation bar in that situation. So seeing	8	So Prof Yeung said, "Look, but if the calculation is
9	three exposed threads cannot by itself be a reason to	9	redone for 500MPa, then the strength of the threads will
10	condemn a coupler assembly, because it could still have	10	increase", and that is correct. The linear line, the
11	a 36 millimetre embedment.	11	calculation line, will increase by 8 per cent, which is
12	Importantly, BOSA's specifications, their	12	the ratio of the 500 grade rebar to the 460 grade rebar.
13	requirements, are not to be equated with the actual	13	But the tests of the bars, the failure loads of the
14	strength performance requirements.	14	bars, show the bars failing by well, I don't know the
15	Next slide, please. We have seen these load test	15	exact number, but it looks like about 30 per cent, from
16	results a lot in the last few days. They show that	16	the graph. So there is still a very healthy margin
17	60 per cent of the threads engaged in a coupler	17	between calculation and the experimental test results.
18	sorry, I should say yes, 60 per cent of the threads	18	There's also been discussion about the fatigue
19	engaged in a coupler is sufficient for structural	19	loading and cyclic loading on the bars and couplers
20	safety, ie 26.4 millimetres, which is 60 per cent of 44.	20	under repetitive train loadings, and there's also been
21		21	discussion about the 0.1 elongation and the cyclic
	Prof Au expressed bewilderment, basically, that the		
22	test with 60 per cent thread engagement had the largest	22	testing of those couplers.
22 23	test with 60 per cent thread engagement had the largest failure load. He said he couldn't understand why this	22 23	testing of those couplers. Now, the variation in stress in the reinforcement
22	test with 60 per cent thread engagement had the largest	22	testing of those couplers.

	Page 113		Page 115
1	carried out by COWI and they have I asked them to	1	behaviour that would necessitate the use of type II
2	tell me, when the trains go on the platform slab, what's	2	couplers in this location.
3	the variation in stress in the reinforcement? The train	3	We have done some very basic calculations to
4	load is insignificant compared to the weight of the slab	4	demonstrate this. These were performed in the last day,
5	and the pressures upon the soil and all the forces	5	in very limited time, and use the methods stated in the
6	acting on that joint. So the actual variation in stress	6	New Zealand and Australian seismic design codes to
7	is only 15 to 20MPa.	7	calculate the yield displacement capacity. The yield
8	COMMISSIONER HANSFORD: Sorry, just so we can understand		displacement capacity of an element is that amount that
9	what you are saying, because we then talk about cyclic	9	the structural component has to deform in order to
10	loads. You are coming to that?	10	
11	A. I was just about to say, yes. So 15MPa, this is a low	11	it's calculating the physical movement.
12	stress. Therefore, I can't envisage that the effects of	12	• • •
13	fatigue or cyclic loading will be a problem.	13	
14	We also discussed this morning the BOSA letter dated	14	<b>v</b> 1
15	7 January, which is something that I've not seen until	15	
16	this morning, but one of the counsel took Prof Yeung	16	*
17	through that and there was a comment on whether or not	17	the reinforcement inside.
18	the couplers would be able to withstand the cyclic	18	
19	loading tests there was a comment about whether the	19	
20	threads should be fully engaged or not for that test.	20	
21	Again, I've not studied that letter but I would just	21	was written and published in 2007 by Priestley, Calvi
22	like to point out that 15MPa is only about 3 per cent of	22	and Kowalsky, and represent the state-of-the-art. The
23	the design stress of the bar, where the cyclic testing	23	yield displacement capacity of the slab calculates to be
24	load is 60 per cent. So what's going to happen in	24	
25	reality is quite different from any theoretical lab	25	
	Page 114		Page 116
1	test.	1	a different way.
2	Next slide, please. There is significant structural	2	Now, this is the start of an extremely complex
3	redundancy or robustness, or in simple terms spare	3	method in which to determine the seismic performance
4	capacity, in the rebar connections. Based on the	4	characteristics of a structure. This method is not in
5	calculation and assessments three of international,	5	use here in Hong Kong due to the low seismicity in the
6	extremely experienced and reputable consultants	6	region. I am therefore not going to dwell on this any
7	Atkins, Arups and COWI there is at least 40 per cent	7	longer. My point is simply to indicate some numbers to
8	spare capacity in the top surface of the EWL D-wall	8	give back into the statement that was agreed in the
9	connection.	9	expert meeting in December.
10			
	COMMISSIONER HANSFORD: Do you mean the top mat?	10	But despite there being no strength requirement for
11	COMMISSIONER HANSFORD: Do you mean the top mat? A. The top mat.	10 11	
11 12			But despite there being no strength requirement for
	A. The top mat.	11	But despite there being no strength requirement for rebar or ductility couplers, I believe that continuing
12	A. The top mat. COMMISSIONER HANSFORD: Okay.	11 12	But despite there being no strength requirement for rebar or ductility couplers, I believe that continuing to comply with the Hong Kong Code of Practice would be
12 13	<ul><li>A. The top mat.</li><li>COMMISSIONER HANSFORD: Okay.</li><li>A. This means that 40 per cent of that rebar can be</li></ul>	11 12 13	But despite there being no strength requirement for rebar or ductility couplers, I believe that continuing to comply with the Hong Kong Code of Practice would be a defensible outcome. As there is at least 50 per cent
12 13 14	<ul><li>A. The top mat.</li><li>COMMISSIONER HANSFORD: Okay.</li><li>A. This means that 40 per cent of that rebar can be completely removed and the structure would still satisfy</li></ul>	11 12 13 14	But despite there being no strength requirement for rebar or ductility couplers, I believe that continuing to comply with the Hong Kong Code of Practice would be a defensible outcome. As there is at least 50 per cent spare capacity in the number of the bottom slab rebars
12 13 14 15	<ul><li>A. The top mat.</li><li>COMMISSIONER HANSFORD: Okay.</li><li>A. This means that 40 per cent of that rebar can be completely removed and the structure would still satisfy all relevant design codes and would still be safe.</li></ul>	11 12 13 14 15	But despite there being no strength requirement for rebar or ductility couplers, I believe that continuing to comply with the Hong Kong Code of Practice would be a defensible outcome. As there is at least 50 per cent spare capacity in the number of the bottom slab rebars passing into the D-wall via couplers, we could consider
12 13 14 15 16	<ul><li>A. The top mat.</li><li>COMMISSIONER HANSFORD: Okay.</li><li>A. This means that 40 per cent of that rebar can be completely removed and the structure would still satisfy all relevant design codes and would still be safe.</li><li>For the bottom surface, I agree that there is no</li></ul>	11 12 13 14 15 16	But despite there being no strength requirement for rebar or ductility couplers, I believe that continuing to comply with the Hong Kong Code of Practice would be a defensible outcome. As there is at least 50 per cent spare capacity in the number of the bottom slab rebars passing into the D-wall via couplers, we could consider 50 per cent of those couplers ineffective without any
12 13 14 15 16 17	<ul> <li>A. The top mat.</li> <li>COMMISSIONER HANSFORD: Okay.</li> <li>A. This means that 40 per cent of that rebar can be completely removed and the structure would still satisfy all relevant design codes and would still be safe.</li> <li>For the bottom surface, I agree that there is no strength requirement for those bars, as the section will</li> </ul>	11 12 13 14 15 16 17	But despite there being no strength requirement for rebar or ductility couplers, I believe that continuing to comply with the Hong Kong Code of Practice would be a defensible outcome. As there is at least 50 per cent spare capacity in the number of the bottom slab rebars passing into the D-wall via couplers, we could consider 50 per cent of those couplers ineffective without any implication on code compliance.
12 13 14 15 16 17 18	<ul> <li>A. The top mat.</li> <li>COMMISSIONER HANSFORD: Okay.</li> <li>A. This means that 40 per cent of that rebar can be completely removed and the structure would still satisfy all relevant design codes and would still be safe.</li> <li>For the bottom surface, I agree that there is no strength requirement for those bars, as the section will always remain in compression. There has, however, been</li> </ul>	11 12 13 14 15 16 17 18	But despite there being no strength requirement for rebar or ductility couplers, I believe that continuing to comply with the Hong Kong Code of Practice would be a defensible outcome. As there is at least 50 per cent spare capacity in the number of the bottom slab rebars passing into the D-wall via couplers, we could consider 50 per cent of those couplers ineffective without any implication on code compliance. COMMISSIONER HANSFORD: What do you mean by "defensible
12 13 14 15 16 17 18 19	<ul> <li>A. The top mat.</li> <li>COMMISSIONER HANSFORD: Okay.</li> <li>A. This means that 40 per cent of that rebar can be completely removed and the structure would still satisfy all relevant design codes and would still be safe.</li> <li>For the bottom surface, I agree that there is no strength requirement for those bars, as the section will always remain in compression. There has, however, been much discussion with previous experts over the issue of</li> </ul>	11 12 13 14 15 16 17 18 19	But despite there being no strength requirement for rebar or ductility couplers, I believe that continuing to comply with the Hong Kong Code of Practice would be a defensible outcome. As there is at least 50 per cent spare capacity in the number of the bottom slab rebars passing into the D-wall via couplers, we could consider 50 per cent of those couplers ineffective without any implication on code compliance. COMMISSIONER HANSFORD: What do you mean by "defensible outcome"?
12 13 14 15 16 17 18 19 20	<ul> <li>A. The top mat.</li> <li>COMMISSIONER HANSFORD: Okay.</li> <li>A. This means that 40 per cent of that rebar can be completely removed and the structure would still satisfy all relevant design codes and would still be safe.</li> <li>For the bottom surface, I agree that there is no strength requirement for those bars, as the section will always remain in compression. There has, however, been much discussion with previous experts over the issue of the requirement for type II ductility couplers. The</li> </ul>	111 12 13 14 15 16 17 18 19 20 21	<ul> <li>But despite there being no strength requirement for rebar or ductility couplers, I believe that continuing to comply with the Hong Kong Code of Practice would be a defensible outcome. As there is at least 50 per cent spare capacity in the number of the bottom slab rebars passing into the D-wall via couplers, we could consider 50 per cent of those couplers ineffective without any implication on code compliance.</li> <li>COMMISSIONER HANSFORD: What do you mean by "defensible outcome"?</li> <li>A. I mean this would be a sensible idea; one that could be</li> </ul>
12 13 14 15 16 17 18 19 20 21	<ul> <li>A. The top mat.</li> <li>COMMISSIONER HANSFORD: Okay.</li> <li>A. This means that 40 per cent of that rebar can be completely removed and the structure would still satisfy all relevant design codes and would still be safe.</li> <li>For the bottom surface, I agree that there is no strength requirement for those bars, as the section will always remain in compression. There has, however, been much discussion with previous experts over the issue of the requirement for type II ductility couplers. The issue we discussed and agreed at the expert meeting in</li> </ul>	111 12 13 14 15 16 17 18 19 20 21	<ul> <li>But despite there being no strength requirement for rebar or ductility couplers, I believe that continuing to comply with the Hong Kong Code of Practice would be a defensible outcome. As there is at least 50 per cent spare capacity in the number of the bottom slab rebars passing into the D-wall via couplers, we could consider 50 per cent of those couplers ineffective without any implication on code compliance.</li> <li>COMMISSIONER HANSFORD: What do you mean by "defensible outcome"?</li> <li>A. I mean this would be a sensible idea; one that could be defended quite easily, not taking any risks or anything.</li> </ul>
12 13 14 15 16 17 18 19 20 21 22	<ul> <li>A. The top mat.</li> <li>COMMISSIONER HANSFORD: Okay.</li> <li>A. This means that 40 per cent of that rebar can be completely removed and the structure would still satisfy all relevant design codes and would still be safe.</li> <li>For the bottom surface, I agree that there is no strength requirement for those bars, as the section will always remain in compression. There has, however, been much discussion with previous experts over the issue of the requirement for type II ductility couplers. The issue we discussed and agreed at the expert meeting in December was that the seismic movement or performance of</li> </ul>	11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>But despite there being no strength requirement for rebar or ductility couplers, I believe that continuing to comply with the Hong Kong Code of Practice would be a defensible outcome. As there is at least 50 per cent spare capacity in the number of the bottom slab rebars passing into the D-wall via couplers, we could consider 50 per cent of those couplers ineffective without any implication on code compliance.</li> <li>COMMISSIONER HANSFORD: What do you mean by "defensible outcome"?</li> <li>A. I mean this would be a sensible idea; one that could be defended quite easily, not taking any risks or anything.</li> <li>COMMISSIONER HANSFORD: So conservative?</li> </ul>

	Page 117		Page 119
1	So the joint. During Prof Au's evidence, much	1	consider that shear force just acting on that wall.
2	discussion was given to the performance of the internal	2	COMMISSIONER HANSFORD: And this manuscript here is from
3	actions inside the joint, between the D-wall, EWL and	3	Atkins?
4	OTE slabs. I had not included a checking of the joint	4	A. This is their calculation which I extracted from the
5	in my report because there is no difference between	5	submission they make.
6	change 1 and change 2, and I had already accepted the	6	So there are some aspects of this calculation that
7	fact that the change 1 was previously accepted for	7	I don't fully understand. It's handwritten and so
8	construction by the Buildings Department. I have no	8	clearly it would be good to have a discussion with the
9	reason to doubt their view that the joint was	9	actual engineer by himself who wrote that. But if this
10	acceptable.	10	is the approach they have used, then this is very
11	Structural engineers have many different ways of	11	conservative, and it would certainly demonstrate
12	analysing and designing structural elements and details.	12	compliance for both change 1 and for the issue of
13	This particular joint could be designed using any of the	13	horizontal shear stresses for change 2.
14	following methods shown.	14	Next slide, please.
15	Next slide, please. There is the clamping theory	15	COMMISSIONER HANSFORD: Sorry, I don't wish to labour the
16	concept as discussed by Prof McQuillan. There is the	16	point, Mr Southward can we go back to the slide?
17	Atkins calculation method, which they submitted in	17	There. All of that on the right-hand side is Atkins',
18	December, which in my opinion is extremely conservative.	18	including the writing in red; is that correct?
19	There is Prof Au's specialist beam-column joint method,	19	A. Yes.
20	which he did not describe to us. There is my preference	20	COMMISSIONER HANSFORD: Thank you.
21	in practice of using finite element analysis, using 2D	21	A. My bit is the graphic.
22	plate elements or 3D solid brick elements.	22	COMMISSIONER HANSFORD: Yes, understood.
23	COMMISSIONER HANSFORD: Which, for the benefit of lay	23	A. I have considered the presentation yesterday from
24	people, is a computer modelling process?	24	Prof Au and his free body diagram, which is shown on
25	A. This is a fairly sophisticated computer modelling	25	this slide. So I've just extracted that from his
	Page 118		Page 120
1	process that calculates the internal stresses in	1	presentation.
2	structures.	2	It is easy to allay his concern.
3	COMMISSIONER HANSFORD: Indeed.	3	Next slide, please. Looking at a close-up detail of
4	A. In quite some detail.	4	the yellow slice, we can see there are two layers of T50
5	COMMISSIONER HANSFORD: Thank you.	5	vertical bars and two layers of T40 bars that cross this
6	A. And there is a strut-and-tie analysis.	6	interface. So these are the vertical bars drawn in
7	The point is that there are many ways to skin a cat.	7	black. Two of those bars are T40 bars and two of those
8	This applies equally well in structural engineering as	8	bars are T50 bars.
9	it does to any other application in life. All ways,	9	There is so much reinforcement, in fact, that the
10	however, will result in a design that is safe and	10	basic shear capacity of the steel bars in dowel action
11	serviceable.	11	alone is enough to resist the tension load developed in
12	Next slide, please. I have reviewed the Atkins	12	the horizontal T40 bars at the top of the slab. So you
13	calculation which is shown on this slide. This is	13	can see the red arrow which is that's the tension
14	an extremely conservative approach, whereby they have	14	force in the T40 bars, and that is pulling the yellow
15	considered the vertical element of the D-wall inside the	15	slice to the left. That pulling is basically resisted
4 -	considered the vertical element of the D-wall inside the		
16	EWL slab to be isolated, on its own, and they have	16	by the steel bars. The steel bars would have to be
16 17		16 17	by the steel bars. The steel bars would have to be sheared. The steel bars would have to break in order
17 18	EWL slab to be isolated, on its own, and they have checked that for an internal shear force that is generated by the applied bending moment, and they have	17 18	sheared. The steel bars would have to break in order for the yellow slice to move.
17 18 19	EWL slab to be isolated, on its own, and they have checked that for an internal shear force that is generated by the applied bending moment, and they have divided that applied bending moment by the lever arm	17 18 19	sheared. The steel bars would have to break in order for the yellow slice to move. COMMISSIONER HANSFORD: And again, for lay people, dowel
17 18 19 20	EWL slab to be isolated, on its own, and they have checked that for an internal shear force that is generated by the applied bending moment, and they have divided that applied bending moment by the lever arm between the compression zone and the steel	17 18	<ul><li>sheared. The steel bars would have to break in order</li><li>for the yellow slice to move.</li><li>COMMISSIONER HANSFORD: And again, for lay people, dowel action?</li></ul>
17 18 19 20 21	EWL slab to be isolated, on its own, and they have checked that for an internal shear force that is generated by the applied bending moment, and they have divided that applied bending moment by the lever arm	17 18 19 20 21	sheared. The steel bars would have to break in order for the yellow slice to move. COMMISSIONER HANSFORD: And again, for lay people, dowel
<ol> <li>17</li> <li>18</li> <li>19</li> <li>20</li> <li>21</li> <li>22</li> </ol>	EWL slab to be isolated, on its own, and they have checked that for an internal shear force that is generated by the applied bending moment, and they have divided that applied bending moment by the lever arm between the compression zone and the steel reinforcement. That has given them an internal shear force.	17 18 19 20 21 22	<ul><li>sheared. The steel bars would have to break in order for the yellow slice to move.</li><li>COMMISSIONER HANSFORD: And again, for lay people, dowel action?</li><li>A. Dowel action is exactly well, actually, I'll explain that.</li></ul>
<ol> <li>17</li> <li>18</li> <li>19</li> <li>20</li> <li>21</li> <li>22</li> <li>23</li> </ol>	EWL slab to be isolated, on its own, and they have checked that for an internal shear force that is generated by the applied bending moment, and they have divided that applied bending moment by the lever arm between the compression zone and the steel reinforcement. That has given them an internal shear force. That's a very conservative way, because there is	<ol> <li>17</li> <li>18</li> <li>19</li> <li>20</li> <li>21</li> <li>22</li> <li>23</li> </ol>	<ul><li>sheared. The steel bars would have to break in order for the yellow slice to move.</li><li>COMMISSIONER HANSFORD: And again, for lay people, dowel action?</li><li>A. Dowel action is exactly well, actually, I'll explain that.</li><li>COMMISSIONER HANSFORD: Very good.</li></ul>
<ol> <li>17</li> <li>18</li> <li>19</li> <li>20</li> <li>21</li> <li>22</li> </ol>	EWL slab to be isolated, on its own, and they have checked that for an internal shear force that is generated by the applied bending moment, and they have divided that applied bending moment by the lever arm between the compression zone and the steel reinforcement. That has given them an internal shear force.	17 18 19 20 21 22	<ul><li>sheared. The steel bars would have to break in order for the yellow slice to move.</li><li>COMMISSIONER HANSFORD: And again, for lay people, dowel action?</li><li>A. Dowel action is exactly well, actually, I'll explain that.</li></ul>

	Page 121		Page 123
1	half of that of its tensile strength. There are four	1	the clamping action referred to by Prof McQuillan in his
2	layers of vertical bars but there are only two layers of	2	report.
3	horizontal bars, and the vertical bars are bigger, they	3	Next slide, please. Here, we have the strut-and-tie
4	are T50, so the cross-sectional area of the vertical	4	system that provides equilibrium in the joint for the
5	steel is much more than twice the cross-sectional area	5	change 2 design.
6	of the horizontal blue steel.	6	COMMISSIONER HANSFORD: Isn't it the same?
7	COMMISSIONER HANSFORD: So they are resisting?	7	A. You will see, if we flick back and forth between the two
8	A. They are resisting. That doesn't allow for the fact	8	slides if you could do that, please that there is
9	that there is 40 per cent spare capacity in this joint	9	no difference in the strut-and-tie arrangement between
10	anyway.	10	the two systems. By this I mean the manner in which the
11	To answer your question about the dowel action,	11	forces are transferred between the reinforcements in the
12	I can also refer here to the last slide, Prof Yeung's	12	slab and the wall.
13	presentation yesterday. If you'll remember, this showed	13	This is because I'm sorry, I've already said
14	a bolt connecting two plates, and Prof Yeung explained	14	that.
15	that the purpose of the bolt is to stop the two plates	15	Next slide, please. So the results of this
16	sliding apart.	16	strut-and-tie analysis. Typically, these types of
17	COMMISSIONER HANSFORD: Was it Prof Yeung or Prof Au	17	analysis should be done by hand, and when I learned
18	A. Prof Yeung. He explained that the purpose of the bolt	18	engineering I had to do strut-and-tie calculations by
19	is to stop the two plates sliding apart.	19	hand. But it's much faster to do this by a computer.
20	In our case here, the steel reinforcement bars are	20	So on the right-hand side are the computed strut-and-tie
21	doing exactly that, exactly the same job as the bolts in	21	forces. There are two main areas of blue tension within
22	Prof Yeung's slide. Thus the yellow free body securely	22	the D-wall. There's a vertical tension of approximately
23	anchored to the D-wall below, it cannot move or slip and	23	3,400 kilonewtons on the back face of the D-wall, which
24	there is no concern over the presence of a construction	24	is easily resisted by the three vertical layers of
25	joint.	25	reinforcement at this location.
	Page 122		Page 124
1	Page 122 Strut-and-tie method, which is the final method on	1	Page 124 There is a diagonal tension of 450 kilonewtons in
1 2		1 2	-
	Strut-and-tie method, which is the final method on		There is a diagonal tension of 450 kilonewtons in
2	Strut-and-tie method, which is the final method on my list, are simple ways to represent and analyse the	2	There is a diagonal tension of 450 kilonewtons in the D-wall within the depth of the OTE slab. This
2 3	Strut-and-tie method, which is the final method on my list, are simple ways to represent and analyse the transfer of forces from one structural element to	2 3	There is a diagonal tension of 450 kilonewtons in the D-wall within the depth of the OTE slab. This diagonal tension will be resisted by the horizontal
2 3 4	Strut-and-tie method, which is the final method on my list, are simple ways to represent and analyse the transfer of forces from one structural element to another. They are especially useful at corner joints	2 3 4	There is a diagonal tension of 450 kilonewtons in the D-wall within the depth of the OTE slab. This diagonal tension will be resisted by the horizontal shear links
2 3 4 5	Strut-and-tie method, which is the final method on my list, are simple ways to represent and analyse the transfer of forces from one structural element to another. They are especially useful at corner joints such as this. Indeed, use of such a method was	2 3 4 5	There is a diagonal tension of 450 kilonewtons in the D-wall within the depth of the OTE slab. This diagonal tension will be resisted by the horizontal shear links COMMISSIONER HANSFORD: Sorry, is that the 474?
2 3 4 5 6	Strut-and-tie method, which is the final method on my list, are simple ways to represent and analyse the transfer of forces from one structural element to another. They are especially useful at corner joints such as this. Indeed, use of such a method was suggested by Prof Au in his expert report. The method	2 3 4 5 6	There is a diagonal tension of 450 kilonewtons in the D-wall within the depth of the OTE slab. This diagonal tension will be resisted by the horizontal shear links COMMISSIONER HANSFORD: Sorry, is that the 474? A. That's the 474, yes.
2 3 4 5 6 7	Strut-and-tie method, which is the final method on my list, are simple ways to represent and analyse the transfer of forces from one structural element to another. They are especially useful at corner joints such as this. Indeed, use of such a method was suggested by Prof Au in his expert report. The method consists of diagrammatically representing the forces	2 3 4 5 6 7	There is a diagonal tension of 450 kilonewtons in the D-wall within the depth of the OTE slab. This diagonal tension will be resisted by the horizontal shear links COMMISSIONER HANSFORD: Sorry, is that the 474? A. That's the 474, yes. COMMISSIONER HANSFORD: Thank you.
2 3 4 5 6 7 8	Strut-and-tie method, which is the final method on my list, are simple ways to represent and analyse the transfer of forces from one structural element to another. They are especially useful at corner joints such as this. Indeed, use of such a method was suggested by Prof Au in his expert report. The method consists of diagrammatically representing the forces inside the joint and demonstrating a feasible load path	2 3 4 5 6 7 8	There is a diagonal tension of 450 kilonewtons in the D-wall within the depth of the OTE slab. This diagonal tension will be resisted by the horizontal shear links COMMISSIONER HANSFORD: Sorry, is that the 474? A. That's the 474, yes. COMMISSIONER HANSFORD: Thank you. A. This diagonal tension is resisted by the horizontal
2 3 4 5 6 7 8 9	Strut-and-tie method, which is the final method on my list, are simple ways to represent and analyse the transfer of forces from one structural element to another. They are especially useful at corner joints such as this. Indeed, use of such a method was suggested by Prof Au in his expert report. The method consists of diagrammatically representing the forces inside the joint and demonstrating a feasible load path to transfer the tension forces in the slabs to the	2 3 4 5 6 7 8 9	<ul> <li>There is a diagonal tension of 450 kilonewtons in the D-wall within the depth of the OTE slab. This diagonal tension will be resisted by the horizontal shear links</li> <li>COMMISSIONER HANSFORD: Sorry, is that the 474?</li> <li>A. That's the 474, yes.</li> <li>COMMISSIONER HANSFORD: Thank you.</li> <li>A. This diagonal tension is resisted by the horizontal shear links which are equally spaced at 150 millimetres</li> </ul>
2 3 4 5 6 7 8 9 10	Strut-and-tie method, which is the final method on my list, are simple ways to represent and analyse the transfer of forces from one structural element to another. They are especially useful at corner joints such as this. Indeed, use of such a method was suggested by Prof Au in his expert report. The method consists of diagrammatically representing the forces inside the joint and demonstrating a feasible load path to transfer the tension forces in the slabs to the tension forces in the D-wall.	2 3 4 5 6 7 8 9 10	There is a diagonal tension of 450 kilonewtons in the D-wall within the depth of the OTE slab. This diagonal tension will be resisted by the horizontal shear links COMMISSIONER HANSFORD: Sorry, is that the 474? A. That's the 474, yes. COMMISSIONER HANSFORD: Thank you. A. This diagonal tension is resisted by the horizontal shear links which are equally spaced at 150 millimetres up the D-wall.
2 3 4 5 6 7 8 9 10 11	Strut-and-tie method, which is the final method on my list, are simple ways to represent and analyse the transfer of forces from one structural element to another. They are especially useful at corner joints such as this. Indeed, use of such a method was suggested by Prof Au in his expert report. The method consists of diagrammatically representing the forces inside the joint and demonstrating a feasible load path to transfer the tension forces in the slabs to the tension forces in the D-wall. So, in the last day, we have had a look at	2 3 4 5 6 7 8 9 10 11	<ul> <li>There is a diagonal tension of 450 kilonewtons in the D-wall within the depth of the OTE slab. This diagonal tension will be resisted by the horizontal shear links</li> <li>COMMISSIONER HANSFORD: Sorry, is that the 474?</li> <li>A. That's the 474, yes.</li> <li>COMMISSIONER HANSFORD: Thank you.</li> <li>A. This diagonal tension is resisted by the horizontal shear links which are equally spaced at 150 millimetres up the D-wall.</li> <li>So after resolving for the fact that those</li> </ul>
2 3 4 5 6 7 8 9 10 11 12	Strut-and-tie method, which is the final method on my list, are simple ways to represent and analyse the transfer of forces from one structural element to another. They are especially useful at corner joints such as this. Indeed, use of such a method was suggested by Prof Au in his expert report. The method consists of diagrammatically representing the forces inside the joint and demonstrating a feasible load path to transfer the tension forces in the slabs to the tension forces in the D-wall. So, in the last day, we have had a look at a possible strut-and-tie representation, in order to do	2 3 4 5 6 7 8 9 10 11 12	<ul> <li>There is a diagonal tension of 450 kilonewtons in the D-wall within the depth of the OTE slab. This diagonal tension will be resisted by the horizontal shear links</li> <li>COMMISSIONER HANSFORD: Sorry, is that the 474?</li> <li>A. That's the 474, yes.</li> <li>COMMISSIONER HANSFORD: Thank you.</li> <li>A. This diagonal tension is resisted by the horizontal shear links which are equally spaced at 150 millimetres up the D-wall.</li> <li>So after resolving for the fact that those horizontal shear links aren't diagonal, they are horizontal, there proves to be 100 per cent more reinforcement than required.</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13	Strut-and-tie method, which is the final method on my list, are simple ways to represent and analyse the transfer of forces from one structural element to another. They are especially useful at corner joints such as this. Indeed, use of such a method was suggested by Prof Au in his expert report. The method consists of diagrammatically representing the forces inside the joint and demonstrating a feasible load path to transfer the tension forces in the slabs to the tension forces in the D-wall. So, in the last day, we have had a look at a possible strut-and-tie representation, in order to do the simple checking calculations referred to by Prof Au.	2 3 4 5 6 7 8 9 10 11 12 13	<ul> <li>There is a diagonal tension of 450 kilonewtons in the D-wall within the depth of the OTE slab. This diagonal tension will be resisted by the horizontal shear links</li> <li>COMMISSIONER HANSFORD: Sorry, is that the 474?</li> <li>A. That's the 474, yes.</li> <li>COMMISSIONER HANSFORD: Thank you.</li> <li>A. This diagonal tension is resisted by the horizontal shear links which are equally spaced at 150 millimetres up the D-wall.</li> <li>So after resolving for the fact that those horizontal shear links aren't diagonal, they are horizontal, there proves to be 100 per cent more</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14	Strut-and-tie method, which is the final method on my list, are simple ways to represent and analyse the transfer of forces from one structural element to another. They are especially useful at corner joints such as this. Indeed, use of such a method was suggested by Prof Au in his expert report. The method consists of diagrammatically representing the forces inside the joint and demonstrating a feasible load path to transfer the tension forces in the slabs to the tension forces in the D-wall. So, in the last day, we have had a look at a possible strut-and-tie representation, in order to do the simple checking calculations referred to by Prof Au. This slide shows the base data for checking of the joint. These are the ultimate limit state moments and shears on the joint, and they are extracted from the	2 3 4 5 6 7 8 9 10 11 12 13 14	<ul> <li>There is a diagonal tension of 450 kilonewtons in the D-wall within the depth of the OTE slab. This diagonal tension will be resisted by the horizontal shear links</li> <li>COMMISSIONER HANSFORD: Sorry, is that the 474?</li> <li>A. That's the 474, yes.</li> <li>COMMISSIONER HANSFORD: Thank you.</li> <li>A. This diagonal tension is resisted by the horizontal shear links which are equally spaced at 150 millimetres up the D-wall.</li> <li>So after resolving for the fact that those horizontal shear links aren't diagonal, they are horizontal, there proves to be 100 per cent more reinforcement than required.</li> <li>Next slide, please. As of 14 January, 75 tests have been carried out. Of these 75 tests, 73 show embedment</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15	Strut-and-tie method, which is the final method on my list, are simple ways to represent and analyse the transfer of forces from one structural element to another. They are especially useful at corner joints such as this. Indeed, use of such a method was suggested by Prof Au in his expert report. The method consists of diagrammatically representing the forces inside the joint and demonstrating a feasible load path to transfer the tension forces in the slabs to the tension forces in the D-wall. So, in the last day, we have had a look at a possible strut-and-tie representation, in order to do the simple checking calculations referred to by Prof Au. This slide shows the base data for checking of the joint. These are the ultimate limit state moments and shears on the joint, and they are extracted from the original Atkins design calculations for a typical panel,	2 3 4 5 6 7 8 9 10 11 12 13 14 15	<ul> <li>There is a diagonal tension of 450 kilonewtons in the D-wall within the depth of the OTE slab. This diagonal tension will be resisted by the horizontal shear links</li> <li>COMMISSIONER HANSFORD: Sorry, is that the 474?</li> <li>A. That's the 474, yes.</li> <li>COMMISSIONER HANSFORD: Thank you.</li> <li>A. This diagonal tension is resisted by the horizontal shear links which are equally spaced at 150 millimetres up the D-wall.</li> <li>So after resolving for the fact that those horizontal shear links aren't diagonal, they are horizontal, there proves to be 100 per cent more reinforcement than required.</li> <li>Next slide, please. As of 14 January, 75 tests have been carried out. Of these 75 tests, 73 show embedment length which is greater than 26.4 millimetres, which is</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	Strut-and-tie method, which is the final method on my list, are simple ways to represent and analyse the transfer of forces from one structural element to another. They are especially useful at corner joints such as this. Indeed, use of such a method was suggested by Prof Au in his expert report. The method consists of diagrammatically representing the forces inside the joint and demonstrating a feasible load path to transfer the tension forces in the slabs to the tension forces in the D-wall. So, in the last day, we have had a look at a possible strut-and-tie representation, in order to do the simple checking calculations referred to by Prof Au. This slide shows the base data for checking of the joint. These are the ultimate limit state moments and shears on the joint, and they are extracted from the	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	There is a diagonal tension of 450 kilonewtons in the D-wall within the depth of the OTE slab. This diagonal tension will be resisted by the horizontal shear links COMMISSIONER HANSFORD: Sorry, is that the 474? A. That's the 474, yes. COMMISSIONER HANSFORD: Thank you. A. This diagonal tension is resisted by the horizontal shear links which are equally spaced at 150 millimetres up the D-wall. So after resolving for the fact that those horizontal shear links aren't diagonal, they are horizontal, there proves to be 100 per cent more reinforcement than required. Next slide, please. As of 14 January, 75 tests have been carried out. Of these 75 tests, 73 show embedment length which is greater than 26.4 millimetres, which is the number from the test, 60 per cent of 44 millimetre
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	Strut-and-tie method, which is the final method on my list, are simple ways to represent and analyse the transfer of forces from one structural element to another. They are especially useful at corner joints such as this. Indeed, use of such a method was suggested by Prof Au in his expert report. The method consists of diagrammatically representing the forces inside the joint and demonstrating a feasible load path to transfer the tension forces in the slabs to the tension forces in the D-wall. So, in the last day, we have had a look at a possible strut-and-tie representation, in order to do the simple checking calculations referred to by Prof Au. This slide shows the base data for checking of the joint. These are the ultimate limit state moments and shears on the joint, and they are extracted from the original Atkins design calculations for a typical panel,	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	There is a diagonal tension of 450 kilonewtons in the D-wall within the depth of the OTE slab. This diagonal tension will be resisted by the horizontal shear links COMMISSIONER HANSFORD: Sorry, is that the 474? A. That's the 474, yes. COMMISSIONER HANSFORD: Thank you. A. This diagonal tension is resisted by the horizontal shear links which are equally spaced at 150 millimetres up the D-wall. So after resolving for the fact that those horizontal shear links aren't diagonal, they are horizontal, there proves to be 100 per cent more reinforcement than required. Next slide, please. As of 14 January, 75 tests have been carried out. Of these 75 tests, 73 show embedment length which is greater than 26.4 millimetres, which is the number from the test, 60 per cent of 44 millimetre thread. That's 97 per cent. 51 show an embedment
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	Strut-and-tie method, which is the final method on my list, are simple ways to represent and analyse the transfer of forces from one structural element to another. They are especially useful at corner joints such as this. Indeed, use of such a method was suggested by Prof Au in his expert report. The method consists of diagrammatically representing the forces inside the joint and demonstrating a feasible load path to transfer the tension forces in the slabs to the tension forces in the D-wall. So, in the last day, we have had a look at a possible strut-and-tie representation, in order to do the simple checking calculations referred to by Prof Au. This slide shows the base data for checking of the joint. These are the ultimate limit state moments and shears on the joint, and they are extracted from the original Atkins design calculations for a typical panel, which in this instance is EH113.	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	There is a diagonal tension of 450 kilonewtons in the D-wall within the depth of the OTE slab. This diagonal tension will be resisted by the horizontal shear links COMMISSIONER HANSFORD: Sorry, is that the 474? A. That's the 474, yes. COMMISSIONER HANSFORD: Thank you. A. This diagonal tension is resisted by the horizontal shear links which are equally spaced at 150 millimetres up the D-wall. So after resolving for the fact that those horizontal shear links aren't diagonal, they are horizontal, there proves to be 100 per cent more reinforcement than required. Next slide, please. As of 14 January, 75 tests have been carried out. Of these 75 tests, 73 show embedment length which is greater than 26.4 millimetres, which is the number from the test, 60 per cent of 44 millimetre
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	Strut-and-tie method, which is the final method on my list, are simple ways to represent and analyse the transfer of forces from one structural element to another. They are especially useful at corner joints such as this. Indeed, use of such a method was suggested by Prof Au in his expert report. The method consists of diagrammatically representing the forces inside the joint and demonstrating a feasible load path to transfer the tension forces in the slabs to the tension forces in the D-wall. So, in the last day, we have had a look at a possible strut-and-tie representation, in order to do the simple checking calculations referred to by Prof Au. This slide shows the base data for checking of the joint. These are the ultimate limit state moments and shears on the joint, and they are extracted from the original Atkins design calculations for a typical panel, which in this instance is EH113. Next slide, please. This is one possible strut-and-tie system that provides equilibrium in the joint for the change 1 design. The red lines indicate	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	There is a diagonal tension of 450 kilonewtons in the D-wall within the depth of the OTE slab. This diagonal tension will be resisted by the horizontal shear links COMMISSIONER HANSFORD: Sorry, is that the 474? A. That's the 474, yes. COMMISSIONER HANSFORD: Thank you. A. This diagonal tension is resisted by the horizontal shear links which are equally spaced at 150 millimetres up the D-wall. So after resolving for the fact that those horizontal shear links aren't diagonal, they are horizontal, there proves to be 100 per cent more reinforcement than required. Next slide, please. As of 14 January, 75 tests have been carried out. Of these 75 tests, 73 show embedment length which is greater than 26.4 millimetres, which is the number from the test, 60 per cent of 44 millimetre thread. That's 97 per cent. 51 show an embedment length which is greater than 36 millimetres, ie 68 per cent.
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	Strut-and-tie method, which is the final method on my list, are simple ways to represent and analyse the transfer of forces from one structural element to another. They are especially useful at corner joints such as this. Indeed, use of such a method was suggested by Prof Au in his expert report. The method consists of diagrammatically representing the forces inside the joint and demonstrating a feasible load path to transfer the tension forces in the slabs to the tension forces in the D-wall. So, in the last day, we have had a look at a possible strut-and-tie representation, in order to do the simple checking calculations referred to by Prof Au. This slide shows the base data for checking of the joint. These are the ultimate limit state moments and shears on the joint, and they are extracted from the original Atkins design calculations for a typical panel, which in this instance is EH113. Next slide, please. This is one possible strut-and-tie system that provides equilibrium in the joint for the change 1 design. The red lines indicate zones of compression or struts. The blue lines indicate	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	There is a diagonal tension of 450 kilonewtons in the D-wall within the depth of the OTE slab. This diagonal tension will be resisted by the horizontal shear links COMMISSIONER HANSFORD: Sorry, is that the 474? A. That's the 474, yes. COMMISSIONER HANSFORD: Thank you. A. This diagonal tension is resisted by the horizontal shear links which are equally spaced at 150 millimetres up the D-wall. So after resolving for the fact that those horizontal shear links aren't diagonal, they are horizontal, there proves to be 100 per cent more reinforcement than required. Next slide, please. As of 14 January, 75 tests have been carried out. Of these 75 tests, 73 show embedment length which is greater than 26.4 millimetres, which is the number from the test, 60 per cent of 44 millimetre thread. That's 97 per cent. 51 show an embedment length which is greater than 36 millimetres, ie 68 per cent. I am not an expert in statistics, so I can't
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	Strut-and-tie method, which is the final method on my list, are simple ways to represent and analyse the transfer of forces from one structural element to another. They are especially useful at corner joints such as this. Indeed, use of such a method was suggested by Prof Au in his expert report. The method consists of diagrammatically representing the forces inside the joint and demonstrating a feasible load path to transfer the tension forces in the slabs to the tension forces in the D-wall. So, in the last day, we have had a look at a possible strut-and-tie representation, in order to do the simple checking calculations referred to by Prof Au. This slide shows the base data for checking of the joint. These are the ultimate limit state moments and shears on the joint, and they are extracted from the original Atkins design calculations for a typical panel, which in this instance is EH113. Next slide, please. This is one possible strut-and-tie system that provides equilibrium in the joint for the change 1 design. The red lines indicate zones of compression or struts. The blue lines indicate lines of tension or ties.	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	There is a diagonal tension of 450 kilonewtons in the D-wall within the depth of the OTE slab. This diagonal tension will be resisted by the horizontal shear links COMMISSIONER HANSFORD: Sorry, is that the 474? A. That's the 474, yes. COMMISSIONER HANSFORD: Thank you. A. This diagonal tension is resisted by the horizontal shear links which are equally spaced at 150 millimetres up the D-wall. So after resolving for the fact that those horizontal shear links aren't diagonal, they are horizontal, there proves to be 100 per cent more reinforcement than required. Next slide, please. As of 14 January, 75 tests have been carried out. Of these 75 tests, 73 show embedment length which is greater than 26.4 millimetres, which is the number from the test, 60 per cent of 44 millimetre thread. That's 97 per cent. 51 show an embedment length which is greater than 36 millimetres, ie 68 per cent. I am not an expert in statistics, so I can't extrapolate these results to cover the whole structure,
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	Strut-and-tie method, which is the final method on my list, are simple ways to represent and analyse the transfer of forces from one structural element to another. They are especially useful at corner joints such as this. Indeed, use of such a method was suggested by Prof Au in his expert report. The method consists of diagrammatically representing the forces inside the joint and demonstrating a feasible load path to transfer the tension forces in the slabs to the tension forces in the D-wall. So, in the last day, we have had a look at a possible strut-and-tie representation, in order to do the simple checking calculations referred to by Prof Au. This slide shows the base data for checking of the joint. These are the ultimate limit state moments and shears on the joint, and they are extracted from the original Atkins design calculations for a typical panel, which in this instance is EH113. Next slide, please. This is one possible strut-and-tie system that provides equilibrium in the joint for the change 1 design. The red lines indicate zones of compression or struts. The blue lines indicate	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	There is a diagonal tension of 450 kilonewtons in the D-wall within the depth of the OTE slab. This diagonal tension will be resisted by the horizontal shear links COMMISSIONER HANSFORD: Sorry, is that the 474? A. That's the 474, yes. COMMISSIONER HANSFORD: Thank you. A. This diagonal tension is resisted by the horizontal shear links which are equally spaced at 150 millimetres up the D-wall. So after resolving for the fact that those horizontal shear links aren't diagonal, they are horizontal, there proves to be 100 per cent more reinforcement than required. Next slide, please. As of 14 January, 75 tests have been carried out. Of these 75 tests, 73 show embedment length which is greater than 26.4 millimetres, which is the number from the test, 60 per cent of 44 millimetre thread. That's 97 per cent. 51 show an embedment length which is greater than 36 millimetres, ie 68 per cent. I am not an expert in statistics, so I can't

	Page 125		Page 127
1	that with the large margin of safety in the design of	1	yesterday, at page 119. It actually starts at the
2	the structure, that the structure will remain adequate	2	bottom of 118, where at line 21 Prof Yeung looked at
3	and will be safe.	3	a slide which he incorporated into his slides, where he
4	So, to summarise, in the course of construction of	4	said:
5	MTRCL's original design of the station, some changes in		"For the next slide, we are talking about the top of
6	the D-wall reinforcement details were implemented for	6	the connection between the diaphragm wall and the EWL
7	ease of practical construction. After construction of	7	slab, and for this picture I need to give credit to
8	the D-walls, Leighton constructed the connection using	8	Mr Southward. I take this picture directly from his
9	an improved detail that provided superior strength and	9	report. This report is very illustrative"
10	robustness but remained practical for them to construct.	10	Now, I understand that that slide is also a part of
11	The change of detail was compliant with all relevant	11	a slide that you have just presented. It would be slide
12	design codes used for the design of the station	12	number either 7 or 8. Can I just trouble the
13	structure, and the resulting structure is now stronger	13	Secretariat to try to locate slide number 7 or it's
14	and more robust than the original compliant detail. The	14	number 8. Yes.
15	structure continues to be safe design, suitable for its	15	I understand this to be what Prof Yeung was
16	intended use. These changes were part of the normal	16	referring to, because this depicts the second change.
17	construction process and did not represent any	17	He said, at the top of page 119:
18	significant or material change in the design of the	18	" you can see three different types of bars.
19	structure.	19	When I went to engineering school the first thing
20	The results of the testing of the bar couplers which	20	I learned is to do engineering drawing, and the first
21	have been opened up have shown that the significant	21	thing I was told by my professor is even though you try
22	majority have embedded lengths in excess of what's	22	to do a sketch, try to do things in scale. So I think
23	needed. Testing to destruction of the bar coupler	23	Mr Southward may think the same way.
24	assemblies has shown that this embedded length may be	24	If you look at this one now, it's very interesting,
25	reduced to 26.4 millimetres. The independent design	25	if you look at the thickness of the diaphragm wall, it
	Page 126		Page 128
1	reviews of the structure all show that there is at least	1	should be about 1.2 metres; we all know that. Then if
2	40 per cent spare capacity in the design of the coupled	2	you look at these bars now, they are probably a little
3	reinforcement connection between the EWL slab and the	3	bit more than 1 metre on one side and a little bit more
4	D-wall.	4	than 1 metre on the other side. So one thing now I do
5	It follows, therefore, that at least 40 per cent of	5	not have evidence is: is this really the bar
6	the bar couplers could be considered to be ineffective,	6	configuration? That means the bar is not really
7	but yet the structural integrity of the platform slab	7	continuous but one bar with two lap lengths on the other
8	will remain intact and the structure will remain safe	8	side and then the steel from the EWL actually have a lap
9	and suitable for use. The bar couplers at the bottom	9	now with a bar sticking out from the diaphragm wall."
10	surface are not used as structural design elements, so	10	Could I then ask you to look at the sketch again.
11	it would be safe to allow 50 per cent of these to be	11	Can I just ask you this very simple question. By this
12	considered ineffective.	12	sketch, were you intending to demonstrate the use of any
13	However, the opening-up test results to date do not	13	laps in the bars?
14	indicate that it would be necessary to disregard as	14	A. No. The purpose of the sketch was just to show the bars
15	large a percentage of bar couplers as mentioned above.	15	going through the wall, but the lengths either side are
16	In fact only a small percentage are below strength	16	immaterial, not part of the sketch.
17	requirement and are no cause for concern in terms of	17	Q. Could you repeat that, please?
18	structural safety. The structure is, in my opinion,	18	A. The purpose of the sketch was just to show the bars
19	safe.	19	going through the wall. It wasn't meant to represent
20	CHAIRMAN: Thank you.	20	the actual reinforcement arrangement in the slabs each
21	MR SHIEH: Thank you, Dr Southward.	21	side.
22	Perhaps I can just conclude by raising one question	22	Q. Thank you. So the magenta is one layer, the green is
23			the other layer?
24	your sketches yesterday by Prof Yeung.	24	A. Yes.
25	Can I ask you to look at the transcript of	25	MR SHIEH: Thank you. Thank you very much for your

32 (Pages 125 to 128)

	Page 129		Page 131
1	presentation.	1	standard, typical panel.
2	What happens next, as you might have seen from	2	Q. That's fine. I understand. That's pretty
3	observing the proceedings, is that counsel for the other	3	straightforward. Thank you very much.
4	parties may have some questions for you. In the course	4	Then if you go to slide 16, which is the table of
5	of their doing so or afterwards, Mr Chairman and	5	test results.
6	Prof Hansford may have their own questions for you also.	6	You gave some evidence earlier on, during the course
7	After all that, I would have, if I think necessary,	7	of your presentation, regarding the other types of
8	wrapping-up re-examination questions for you. So please	8	tests. This we know is a static load test, and you've
9	remain seated while others ask you their questions.	9	described it, if I may say so, very helpfully, the way
	MR PENNICOTT: Sir, appreciating that we are finishing at	10	in which the bar breaks at the 60 per cent, 70 per cent
11	quarter to five this evening, would you like to take the	11	and 100 per cent.
12	break now? I'm going to be very short, I can tell you,	12	You mentioned, but perhaps did not deal with, one of
12	no more than about ten minutes.	12	the other tests called an elongation test; do you recall
	CHAIRMAN: Why don't you finish?	14	that?
	MR PENNICOTT: Absolutely. I'm more than happy to do that.		A. Yes, I did.
15	Examination by MR PENNICOTT	15	
	Q. Mr Southward, good afternoon.		Q. And that's one of, I think, the requirements of the
		17	Buildings Department.
	A. Thank you.	18	What's your view, if you have one, about the
	Q. Thank you very much for coming along to give evidence to	19	usefulness of that type of test in the situation we find
20	the Commission, thank you for your reports, and thank	20	ourselves?
21	you for your cooperation in the joint statement as well.	21	A. My brief has been to look at the strength side, the
22	As you know, I'm one of the counsel to the	22	structural safety; is the structure safe? So that's
23	Commission and I just have a few questions really by way	23	where I've come from.
24	of clarification of a couple of matters that I would	24	The testing of couplers to compliance to BD rules is
25	like to discuss with you.	25	a kind of is a different thing. It's testing them
	Page 130		Page 132
1	I think it's probably easiest to do that, certainly	1	with respect to the specification requirements, so that
2	in the first instance, by reference to your slides,	2	those couplers can be used in any situation anywhere.
3	which are extremely helpful. Thank you very much.	3	Here we are looking at a very specific application, so
4	Can we look at slide 9, please. This really is just	4	I've just looked at it from the point of view of
5	a point of clarification, as I say, Mr Southward.	5	strength.
6	You refer to "Two layers of T40 bars at	6	Q. So, if I've understood it correctly then, the elongation
7	150 millimetre centres, total 24 bars per panel", and	7	test, is it your understanding, has nothing to do with
8	then in the next diagram you say:	8	strength?
9	"Three layers of T40 bars in two groups, total	9	A. The elongation test is to do with how much the bar moves
10	24 bars per panel"	10	between the coupler. I don't think, to be honest, it
11	That's the first change, and then the second change,	11	would really affect the strength result, because it
12	to:	12	takes a certain load to break the bar. And, okay, there
13	"Two layers of T40 bars at 150 millimetre centres,	13	might be some movement, but you still get the strength
		14	in the bar. You still get the strength that you need.
14	total 36 bars per panel"	17	
14 15	total 36 bars per panel" When you say "per panel", as I understand this is	14	Q. Right.
	1 1		
15	When you say "per panel", as I understand this is	15	Q. Right.
15 16	When you say "per panel", as I understand this is just illustrative of a typical panel?	15 16	<ul><li>Q. Right.</li><li>A. So you can do tests, the elongation tests, but they are</li></ul>
15 16 17	<ul><li>When you say "per panel", as I understand this is just illustrative of a typical panel?</li><li>A. That is a typical D-wall panel which is maybe 5 to</li></ul>	15 16 17	<ul><li>Q. Right.</li><li>A. So you can do tests, the elongation tests, but they are to do with meeting specification requirements and not to</li></ul>
15 16 17 18	<ul><li>When you say "per panel", as I understand this is just illustrative of a typical panel?</li><li>A. That is a typical D-wall panel which is maybe 5 to 6 metres long. It's drawn to scale, it's drawn from a real D-wall panel detail.</li></ul>	15 16 17 18	<ul><li>Q. Right.</li><li>A. So you can do tests, the elongation tests, but they are to do with meeting specification requirements and not to do with the strength of the structure.</li></ul>
15 16 17 18 19	<ul><li>When you say "per panel", as I understand this is just illustrative of a typical panel?</li><li>A. That is a typical D-wall panel which is maybe 5 to 6 metres long. It's drawn to scale, it's drawn from</li></ul>	15 16 17 18 19	<ul><li>Q. Right.</li><li>A. So you can do tests, the elongation tests, but they are to do with meeting specification requirements and not to do with the strength of the structure.</li><li>Q. Okay.</li></ul>
15 16 17 18 19 20	<ul><li>When you say "per panel", as I understand this is just illustrative of a typical panel?</li><li>A. That is a typical D-wall panel which is maybe 5 to 6 metres long. It's drawn to scale, it's drawn from a real D-wall panel detail.</li><li>Q. So it's just taken one of the panels for a typical</li></ul>	15 16 17 18 19 20	<ul> <li>Q. Right.</li> <li>A. So you can do tests, the elongation tests, but they are to do with meeting specification requirements and not to do with the strength of the structure.</li> <li>Q. Okay.</li> <li>COMMISSIONER HANSFORD: Sorry, Mr Southward so are you</li> </ul>
15 16 17 18 19 20 21	<ul><li>When you say "per panel", as I understand this is just illustrative of a typical panel?</li><li>A. That is a typical D-wall panel which is maybe 5 to 6 metres long. It's drawn to scale, it's drawn from a real D-wall panel detail.</li><li>Q. So it's just taken one of the panels for a typical panel?</li><li>A. Yes.</li></ul>	15 16 17 18 19 20 21	<ul> <li>Q. Right.</li> <li>A. So you can do tests, the elongation tests, but they are to do with meeting specification requirements and not to do with the strength of the structure.</li> <li>Q. Okay.</li> <li>COMMISSIONER HANSFORD: Sorry, Mr Southward so are you saying you don't believe elongation to be relevant to</li> </ul>
15 16 17 18 19 20 21 22	<ul><li>When you say "per panel", as I understand this is just illustrative of a typical panel?</li><li>A. That is a typical D-wall panel which is maybe 5 to 6 metres long. It's drawn to scale, it's drawn from a real D-wall panel detail.</li><li>Q. So it's just taken one of the panels for a typical panel?</li></ul>	<ol> <li>15</li> <li>16</li> <li>17</li> <li>18</li> <li>19</li> <li>20</li> <li>21</li> <li>22</li> </ol>	<ul> <li>Q. Right.</li> <li>A. So you can do tests, the elongation tests, but they are to do with meeting specification requirements and not to do with the strength of the structure.</li> <li>Q. Okay.</li> <li>COMMISSIONER HANSFORD: Sorry, Mr Southward so are you saying you don't believe elongation to be relevant to this project?</li> </ul>

1	COMMISSIONER HANSFORD: But it could be relevant for some	1	338.
2	other purpose?	2	CHAIRMAN: I think we saw that one last time, 339.
3	A. To provide a general to make a coupler that can meet	3	MR PENNICOTT: 352, how about that one? I don't know what's
4	any use anywhere in the construction industry, I'm sure	4	happened to the numbering. 352. Thank you very much.
5	there are tests that you would have to do. And	5	Just a general question first before we look at one
6	elongation and cyclic loading would be one of them, yes.	6	or two points, Mr Southward. The government have used,
7	COMMISSIONER HANSFORD: I understand that, but I'm just	7	it appears, a figure of 37 millimetres as a criteria.
8	wondering, to be satisfied with a coupler for this	8	Do you have any observations about that figure?
9	location, for this project maybe this is not	9	A. To be honest, I don't understand where it came from or
10	something you've looked at, but is the elongation	10	how they've reached it. I can't see I'm sure there's
11	capability of these couplers of any relevance?	11	a rationale to it but I don't know what it is, so
12	A. I don't believe it is because the structure has already	12	I can't really comment on it.
13	been built, it's there. The load on the couplers is	13	Q. Okay. I think I may be wrong but I think that it
14	already there.	14	comes about like this, that you take a BOSA threaded
15	COMMISSIONER HANSFORD: Yes.	15	rebar, you assume it has ten threads to it, to give you
16	A. Okay? You've got massive forces on the wall, you've got	16	40 millimetres. The phased array technology that's
17	the weight of the slab. The structure has taken up its	17	being used to measure the engagement or the embedment
18	shape. There is no sign of any distress.	18	has a tolerance of 3 millimetres. And so 40 minus 3 is
19	So if something elongates if it elongates too	19	37 millimetres. That's my understanding of how they get
20	much, you would visibly see the distress, but there is	20	at it.
21	no	21	But if you haven't looked at it, don't worry.
22	COMMISSIONER HANSFORD: That distress would be visible now	22	A. Yes, okay. I understand now. Yes, I see. So they've
23	A in terms of cracking. That distress would be	23	just taken it's plus or minus 3 millimetres so
24	visible, yes, but if there was a problem with	24	they've taken the very worst result, as what their
25	elongation with these couplers, that distress would be	25	criteria would be?
	Page 134		Page 136
1	visible now, but we've not seen any distress.	1	Q. That's my understanding. If one thinks about a couple
2	COMMISSIONER HANSFORD: Thank you.	2	of these results, and one sort of has that figure of
3	A. Maybe if I could just add that the future loading that's	3	37 millimetres in mind can we look at, for example,
4	going on to this structure now is really just the	4	number 50, item 50.
5	trains, and the trains are a very small proportion.	5	We can see that the engagement length as it's
6	COMMISSIONER HANSFORD: As you have already told us, yes	6	described here which is at the top, don't worry about
7	A. So the coupler has taken up its load, it's working, it's	7	it for 50 is 36.8 millimetres: do you see that?
8	there, there's no distress, and the future load is going	8	A. Yes.
9	to be quite small.	9	Q. And on the right-hand side, on the right column, the
10	COMMISSIONER HANSFORD: Thank you.	10	number of exposed threads is said to be one to two. So
11	MR PENNICOTT: But my understanding, Mr Southward, is that	11	let's suppose it's one thread showing. So one has, on
12	the dead load is something of the order of 90 per cent	12	one view, a total length of thread of in excess of 40,
13	or so and the live load is the remaining 10 per cent.	13	4 millimetres per thread?
14	A. Yes.	14	A. Yes.
15	Q. Does that accord with your understanding?	15	Q. If you take the proposition that in fact it's two
16	A. Around there.	16	threads, that would give you 8 millimetres, and so
17	Q. All right.	17	you've got a thread of something like 44 millimetres.
18	Could I ask you, please, to look at not at your	18	With that brief analysis, again, how do you see the
19	slide because they are quite difficult to read from the	19	relevance of the figure of 37 millimetres?
20	slide but can we look at the test results that you	20	A. To be honest, I think they should all be being compared
21	have appended but I think are more easily read	21	to what strength do we actually need, and that strength
22	elsewhere. Could we therefore look, please, at OU338.	22	is so far, the tests have shown that strength is 26.
23	A. Okay. That's a little bit difficult for my eyesight.	23	There may be more tests and that's fine, but on the
24	I'll wait until it's on the screen.	24	results of what's been tested so far, 26 is where you
25	Q. They will pop it up on the screen as well. That's fine.	25	should go.
			-

Page 133

34 (Pages 133 to 136)

	Page 137		Page 139
1	MR PENNICOTT: Yes. All right. Thank you very much,	1	effectively start again tomorrow, you know. I'm just
2	Mr Southward. I have nothing further. Thank you very	2	a bit concerned, if you feel that you need Prof Au with
3	much.	3	you, that the questions you put before you have the
4	CHAIRMAN: Good. We will have it's quarter of an hour	4	assistance and support of Prof Au may prove to be
5	until 4 o'clock. You are reminded you have heard it	5	without much value and that you'll need to effectively
6	being said with others that once you are giving	6	start from square one tomorrow, or are you satisfied
7	evidence, you must keep your own counsel entirely and	7	that you've got some potent questions you can put
8	not discuss your evidence until it is completed.	8	without the assistance of Prof Au?
9	WITNESS: Sure.	9	MR CHOW: Sir, the problem is I'm not sure whether Prof Au
10	CHAIRMAN: Good. Thank you very much.	10	will be available to help me tonight, so I don't want to
11	(3.43 pm)	11	delay the process, and perhaps it turns out to be
12	(A short adjournment)	12	a wasteful exercise. Honestly, I myself, I don't think
13	(4.02 pm)	13	it would be helpful to the Commission for me to enter
14	MR CONNOR: I have no questions for Mr Southward. Thank	14	into a debate on the minute details to the forces and
15	you.	15	stresses and all these values.
16	MR BOULDING: None from me, sir.	16	CHAIRMAN: No.
17	CHAIRMAN: Thank you very much.	17	MR CHOW: So I have no intention to go into that. I would
18	MR CHOW: Mr Chairman and Prof Hansford, the government has	18	prefer that I will just ask questions from a high level,
19	some questions, but before I start, can I put down	19	on a principle level, rather than to go into the
20	a marker here? You will no doubt appreciate that during	20	details. To that extent, I don't really need detailed
21	Mr Southward's explanation, by taking us through various	21	assistance from Prof Au.
22	slides, in particular the later part of the slides about	22	CHAIRMAN: Good. Then I'm more than happy for you to begin.
23	the strut-and-tie models and also the New Zealand	23	But, sorry, help me here. You are saying the
24	state-of-the-art design and theory, all that my first	24	diagrams prepared were not available to Prof Au?
25	observation is these have not been put to Prof Au, so	25	MR CHOW: I'm referring to slides 23, 24 and 25, and
	Page 138		Page 140
1	Prof Au has had no opportunity to deal with it. That's	1	although some of the slides before that, for example on
2	point number one.	2	page 22, the diagram, that actually is existing in
3	Point number two is I have had no opportunity to get	3	somebody else's report, but while Mr Southward explained
4			
	input from Prof Au. I have no intention to delay the	4	
5	input from Prof Au. I have no intention to delay the process, so what I have decided to do is to try to deal	4 5	what he has done to it, this is something new, as far as I'm concerned.
5 6	process, so what I have decided to do is to try to deal		what he has done to it, this is something new, as far as I'm concerned.
6	process, so what I have decided to do is to try to deal with those matters the best I can while I'm on my feet	5	what he has done to it, this is something new, as far as I'm concerned. CHAIRMAN: All right. I see the point you make. Well,
	process, so what I have decided to do is to try to deal with those matters the best I can while I'm on my feet from a relatively high level of way, but in the event	5 6	<ul><li>what he has done to it, this is something new, as far as I'm concerned.</li><li>CHAIRMAN: All right. I see the point you make. Well, good. Why don't you commence, and obviously you can</li></ul>
6 7 8	process, so what I have decided to do is to try to deal with those matters the best I can while I'm on my feet from a relatively high level of way, but in the event that if later on I receive input from whatever sources,	5 6 7	<ul><li>what he has done to it, this is something new, as far as I'm concerned.</li><li>CHAIRMAN: All right. I see the point you make. Well, good. Why don't you commence, and obviously you can reserve your position insofar as you may wish to</li></ul>
6 7 8 9	process, so what I have decided to do is to try to deal with those matters the best I can while I'm on my feet from a relatively high level of way, but in the event that if later on I receive input from whatever sources, I may need to come back on some of the details regarding	5 6 7 8	<ul><li>what he has done to it, this is something new, as far as I'm concerned.</li><li>CHAIRMAN: All right. I see the point you make. Well, good. Why don't you commence, and obviously you can</li></ul>
6 7 8	process, so what I have decided to do is to try to deal with those matters the best I can while I'm on my feet from a relatively high level of way, but in the event that if later on I receive input from whatever sources, I may need to come back on some of the details regarding Mr Southward's evidence. So with that marker	5 6 7 8 9 10	<ul><li>what he has done to it, this is something new, as far as I'm concerned.</li><li>CHAIRMAN: All right. I see the point you make. Well, good. Why don't you commence, and obviously you can reserve your position insofar as you may wish to continue tomorrow with further questions.</li></ul>
6 7 8 9 10	process, so what I have decided to do is to try to deal with those matters the best I can while I'm on my feet from a relatively high level of way, but in the event that if later on I receive input from whatever sources, I may need to come back on some of the details regarding	5 6 7 8 9 10	<ul> <li>what he has done to it, this is something new, as far as I'm concerned.</li> <li>CHAIRMAN: All right. I see the point you make. Well, good. Why don't you commence, and obviously you can reserve your position insofar as you may wish to continue tomorrow with further questions.</li> <li>MR CHOW: Thank you, sir.</li> </ul>
6 7 8 9 10 11	process, so what I have decided to do is to try to deal with those matters the best I can while I'm on my feet from a relatively high level of way, but in the event that if later on I receive input from whatever sources, I may need to come back on some of the details regarding Mr Southward's evidence. So with that marker CHAIRMAN: Could we perhaps I don't know if anybody else	5 6 7 8 9 10 11	<ul> <li>what he has done to it, this is something new, as far as I'm concerned.</li> <li>CHAIRMAN: All right. I see the point you make. Well, good. Why don't you commence, and obviously you can reserve your position insofar as you may wish to continue tomorrow with further questions.</li> <li>MR CHOW: Thank you, sir.</li> <li>COMMISSIONER HANSFORD: Can I just add one point, though</li> </ul>
6 7 8 9 10 11 12	process, so what I have decided to do is to try to deal with those matters the best I can while I'm on my feet from a relatively high level of way, but in the event that if later on I receive input from whatever sources, I may need to come back on some of the details regarding Mr Southward's evidence. So with that marker CHAIRMAN: Could we perhaps I don't know if anybody else wishes to ask questions of our witness on behalf of	5 6 7 8 9 10 11 12	<ul> <li>what he has done to it, this is something new, as far as I'm concerned.</li> <li>CHAIRMAN: All right. I see the point you make. Well, good. Why don't you commence, and obviously you can reserve your position insofar as you may wish to continue tomorrow with further questions.</li> <li>MR CHOW: Thank you, sir.</li> <li>COMMISSIONER HANSFORD: Can I just add one point, though Chairman? Of course, Mr Southward and Prof Au were both</li> </ul>
6 7 8 9 10 11 12 13	process, so what I have decided to do is to try to deal with those matters the best I can while I'm on my feet from a relatively high level of way, but in the event that if later on I receive input from whatever sources, I may need to come back on some of the details regarding Mr Southward's evidence. So with that marker CHAIRMAN: Could we perhaps I don't know if anybody else wishes to ask questions of our witness on behalf of China Technology?	5 6 7 8 9 10 11 12 13	<ul> <li>what he has done to it, this is something new, as far as I'm concerned.</li> <li>CHAIRMAN: All right. I see the point you make. Well, good. Why don't you commence, and obviously you can reserve your position insofar as you may wish to continue tomorrow with further questions.</li> <li>MR CHOW: Thank you, sir.</li> <li>COMMISSIONER HANSFORD: Can I just add one point, though Chairman? Of course, Mr Southward and Prof Au were both at the joint meeting of structural experts where</li> </ul>
6 7 8 9 10 11 12 13 14	<ul> <li>process, so what I have decided to do is to try to deal with those matters the best I can while I'm on my feet from a relatively high level of way, but in the event that if later on I receive input from whatever sources, I may need to come back on some of the details regarding Mr Southward's evidence. So with that marker</li> <li>CHAIRMAN: Could we perhaps I don't know if anybody else wishes to ask questions of our witness on behalf of China Technology?</li> <li>MR SO: We have some questions, but obviously we will</li> </ul>	5 6 7 8 9 10 11 12 13 14	<ul> <li>what he has done to it, this is something new, as far as I'm concerned.</li> <li>CHAIRMAN: All right. I see the point you make. Well, good. Why don't you commence, and obviously you can reserve your position insofar as you may wish to continue tomorrow with further questions.</li> <li>MR CHOW: Thank you, sir.</li> <li>COMMISSIONER HANSFORD: Can I just add one point, though Chairman? Of course, Mr Southward and Prof Au were both at the joint meeting of structural experts where presumably matters of this nature I know it's</li> </ul>
6 7 8 9 10 11 12 13 14 15	<ul> <li>process, so what I have decided to do is to try to deal with those matters the best I can while I'm on my feet from a relatively high level of way, but in the event that if later on I receive input from whatever sources, I may need to come back on some of the details regarding Mr Southward's evidence. So with that marker</li> <li>CHAIRMAN: Could we perhaps I don't know if anybody else wishes to ask questions of our witness on behalf of China Technology?</li> <li>MR SO: We have some questions, but obviously we will appreciate if the government can go first because there</li> </ul>	5 6 7 8 9 10 11 12 13 14 15	<ul> <li>what he has done to it, this is something new, as far as I'm concerned.</li> <li>CHAIRMAN: All right. I see the point you make. Well, good. Why don't you commence, and obviously you can reserve your position insofar as you may wish to continue tomorrow with further questions.</li> <li>MR CHOW: Thank you, sir.</li> <li>COMMISSIONER HANSFORD: Can I just add one point, though Chairman? Of course, Mr Southward and Prof Au were both at the joint meeting of structural experts where presumably matters of this nature I know it's a without-prejudice meeting so we can't know the</li> </ul>
6 7 8 9 10 11 12 13 14 15 16	<ul> <li>process, so what I have decided to do is to try to deal with those matters the best I can while I'm on my feet from a relatively high level of way, but in the event that if later on I receive input from whatever sources, I may need to come back on some of the details regarding Mr Southward's evidence. So with that marker</li> <li>CHAIRMAN: Could we perhaps I don't know if anybody else wishes to ask questions of our witness on behalf of China Technology?</li> <li>MR SO: We have some questions, but obviously we will appreciate if the government can go first because there might be issues arising out of the cross-examination of</li> </ul>	5 6 7 8 9 10 11 12 13 14 15 16	<ul> <li>what he has done to it, this is something new, as far as I'm concerned.</li> <li>CHAIRMAN: All right. I see the point you make. Well, good. Why don't you commence, and obviously you can reserve your position insofar as you may wish to continue tomorrow with further questions.</li> <li>MR CHOW: Thank you, sir.</li> <li>COMMISSIONER HANSFORD: Can I just add one point, though Chairman? Of course, Mr Southward and Prof Au were both at the joint meeting of structural experts where presumably matters of this nature I know it's a without-prejudice meeting so we can't know the details but presumably matters of this nature were</li> </ul>
6 7 8 9 10 11 12 13 14 15 16 17	<ul> <li>process, so what I have decided to do is to try to deal with those matters the best I can while I'm on my feet from a relatively high level of way, but in the event that if later on I receive input from whatever sources, I may need to come back on some of the details regarding Mr Southward's evidence. So with that marker</li> <li>CHAIRMAN: Could we perhaps I don't know if anybody else wishes to ask questions of our witness on behalf of China Technology?</li> <li>MR SO: We have some questions, but obviously we will appreciate if the government can go first because there might be issues arising out of the cross-examination of the government.</li> </ul>	5 6 7 8 9 10 11 12 13 14 15 16 17	<ul> <li>what he has done to it, this is something new, as far as I'm concerned.</li> <li>CHAIRMAN: All right. I see the point you make. Well, good. Why don't you commence, and obviously you can reserve your position insofar as you may wish to continue tomorrow with further questions.</li> <li>MR CHOW: Thank you, sir.</li> <li>COMMISSIONER HANSFORD: Can I just add one point, though Chairman? Of course, Mr Southward and Prof Au were both at the joint meeting of structural experts where presumably matters of this nature I know it's a without-prejudice meeting so we can't know the details but presumably matters of this nature were discussed.</li> </ul>
6 7 8 9 10 11 12 13 14 15 16 17 18	<ul> <li>process, so what I have decided to do is to try to deal with those matters the best I can while I'm on my feet from a relatively high level of way, but in the event that if later on I receive input from whatever sources, I may need to come back on some of the details regarding Mr Southward's evidence. So with that marker</li> <li>CHAIRMAN: Could we perhaps I don't know if anybody else wishes to ask questions of our witness on behalf of China Technology?</li> <li>MR SO: We have some questions, but obviously we will appreciate if the government can go first because there might be issues arising out of the cross-examination of the government.</li> <li>MR CHOW: Sir, I'm happy to do that. Actually, at the</li> </ul>	5 6 7 8 9 10 11 12 13 14 15 16 17 18	<ul> <li>what he has done to it, this is something new, as far as I'm concerned.</li> <li>CHAIRMAN: All right. I see the point you make. Well, good. Why don't you commence, and obviously you can reserve your position insofar as you may wish to continue tomorrow with further questions.</li> <li>MR CHOW: Thank you, sir.</li> <li>COMMISSIONER HANSFORD: Can I just add one point, though Chairman? Of course, Mr Southward and Prof Au were both at the joint meeting of structural experts where presumably matters of this nature I know it's a without-prejudice meeting so we can't know the details but presumably matters of this nature were discussed.</li> <li>MR CHOW: Prof Hansford, I myself have no knowledge of what</li> </ul>
6 7 8 9 10 11 12 13 14 15 16 17 18 19	<ul> <li>process, so what I have decided to do is to try to deal with those matters the best I can while I'm on my feet from a relatively high level of way, but in the event that if later on I receive input from whatever sources, I may need to come back on some of the details regarding Mr Southward's evidence. So with that marker</li> <li>CHAIRMAN: Could we perhaps I don't know if anybody else wishes to ask questions of our witness on behalf of China Technology?</li> <li>MR SO: We have some questions, but obviously we will appreciate if the government can go first because there might be issues arising out of the cross-examination of the government.</li> <li>MR CHOW: Sir, I'm happy to do that. Actually, at the moment, honestly, I don't anticipate that it will be</li> </ul>	5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	<ul> <li>what he has done to it, this is something new, as far as I'm concerned.</li> <li>CHAIRMAN: All right. I see the point you make. Well, good. Why don't you commence, and obviously you can reserve your position insofar as you may wish to continue tomorrow with further questions.</li> <li>MR CHOW: Thank you, sir.</li> <li>COMMISSIONER HANSFORD: Can I just add one point, though Chairman? Of course, Mr Southward and Prof Au were both at the joint meeting of structural experts where presumably matters of this nature I know it's a without-prejudice meeting so we can't know the details but presumably matters of this nature were discussed.</li> <li>MR CHOW: Prof Hansford, I myself have no knowledge of what has been discussed at the without-prejudice meeting.</li> </ul>
6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	<ul> <li>process, so what I have decided to do is to try to deal with those matters the best I can while I'm on my feet from a relatively high level of way, but in the event that if later on I receive input from whatever sources, I may need to come back on some of the details regarding Mr Southward's evidence. So with that marker</li> <li>CHAIRMAN: Could we perhaps I don't know if anybody else wishes to ask questions of our witness on behalf of China Technology?</li> <li>MR SO: We have some questions, but obviously we will appreciate if the government can go first because there might be issues arising out of the cross-examination of the government.</li> <li>MR CHOW: Sir, I'm happy to do that. Actually, at the moment, honestly, I don't anticipate that it will be worthwhile to take the time for me to come back on some</li> </ul>	5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	<ul> <li>what he has done to it, this is something new, as far as I'm concerned.</li> <li>CHAIRMAN: All right. I see the point you make. Well, good. Why don't you commence, and obviously you can reserve your position insofar as you may wish to continue tomorrow with further questions.</li> <li>MR CHOW: Thank you, sir.</li> <li>COMMISSIONER HANSFORD: Can I just add one point, though Chairman? Of course, Mr Southward and Prof Au were both at the joint meeting of structural experts where presumably matters of this nature I know it's a without-prejudice meeting so we can't know the details but presumably matters of this nature were discussed.</li> <li>MR CHOW: Prof Hansford, I myself have no knowledge of what has been discussed at the without-prejudice meeting.</li> <li>COMMISSIONER HANSFORD: No, none of us have.</li> </ul>
6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	<ul> <li>process, so what I have decided to do is to try to deal with those matters the best I can while I'm on my feet from a relatively high level of way, but in the event that if later on I receive input from whatever sources, I may need to come back on some of the details regarding Mr Southward's evidence. So with that marker</li> <li>CHAIRMAN: Could we perhaps I don't know if anybody else wishes to ask questions of our witness on behalf of China Technology?</li> <li>MR SO: We have some questions, but obviously we will appreciate if the government can go first because there might be issues arising out of the cross-examination of the government.</li> <li>MR CHOW: Sir, I'm happy to do that. Actually, at the moment, honestly, I don't anticipate that it will be worthwhile to take the time for me to come back on some of these matters, but I will just proceed on the basis</li> </ul>	5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	<ul> <li>what he has done to it, this is something new, as far as I'm concerned.</li> <li>CHAIRMAN: All right. I see the point you make. Well, good. Why don't you commence, and obviously you can reserve your position insofar as you may wish to continue tomorrow with further questions.</li> <li>MR CHOW: Thank you, sir.</li> <li>COMMISSIONER HANSFORD: Can I just add one point, though Chairman? Of course, Mr Southward and Prof Au were both at the joint meeting of structural experts where presumably matters of this nature I know it's a without-prejudice meeting so we can't know the details but presumably matters of this nature were discussed.</li> <li>MR CHOW: Prof Hansford, I myself have no knowledge of what has been discussed at the without-prejudice meeting.</li> <li>COMMISSIONER HANSFORD: No, none of us have.</li> <li>MR CHOW: That's the reason why my observation is made based</li> </ul>
6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>process, so what I have decided to do is to try to deal with those matters the best I can while I'm on my feet from a relatively high level of way, but in the event that if later on I receive input from whatever sources, I may need to come back on some of the details regarding Mr Southward's evidence. So with that marker</li> <li>CHAIRMAN: Could we perhaps I don't know if anybody else wishes to ask questions of our witness on behalf of China Technology?</li> <li>MR SO: We have some questions, but obviously we will appreciate if the government can go first because there might be issues arising out of the cross-examination of the government.</li> <li>MR CHOW: Sir, I'm happy to do that. Actually, at the moment, honestly, I don't anticipate that it will be worthwhile to take the time for me to come back on some of these matters, but I will just proceed on the basis of what I can at the moment. So, with permission,</li> </ul>	5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>what he has done to it, this is something new, as far as I'm concerned.</li> <li>CHAIRMAN: All right. I see the point you make. Well, good. Why don't you commence, and obviously you can reserve your position insofar as you may wish to continue tomorrow with further questions.</li> <li>MR CHOW: Thank you, sir.</li> <li>COMMISSIONER HANSFORD: Can I just add one point, though Chairman? Of course, Mr Southward and Prof Au were both at the joint meeting of structural experts where presumably matters of this nature I know it's a without-prejudice meeting so we can't know the details but presumably matters of this nature were discussed.</li> <li>MR CHOW: Prof Hansford, I myself have no knowledge of what has been discussed at the without-prejudice meeting.</li> <li>COMMISSIONER HANSFORD: No, none of us have.</li> <li>MR CHOW: That's the reason why my observation is made based on really what actually happened and what appears to me,</li> </ul>

1	Page 141		Page 143
1	MR CHOW: They may well be. I just have no information.	1	Q. Now, COWI analysis, in your expert report, you mention
2	CHAIRMAN: All right. Fine.	2	to us that you have not checked COWI's calculation in
3	MR SHIEH: If I may suggest, there are bound to be questions	3	detail. Does it remain the same position as far as that
4	on areas that do not turn on the "new topics" raised	4	is concerned?
5	orally by Mr Southward. So perhaps in order not to lose	5	A. Correct, yes.
6	unnecessary time, I would endorse what was suggested by	6	Q. So you we have also looked at, for myself briefly,
7	Mr Chairman. We on our part, insofar as is relevant,	7	COWI's supporting documents, which are contained in four
8	will obviously have no problem if, for example,	8	big volumes, over 4,000 pages of documents.
9	overnight, instructions are taken, just as this morning	9	A. Okay.
10	Mr Boulding and myself, having taken instructions	10	Q. From COWI's summary report, it also well, it simply
11	overnight, came back and sought leave to reopen. So we	11	lists out the percentage utilisation of bending moment
12	would absolutely have no problem with that.	12	and shear stress at some critical section, in particular
13	CHAIRMAN: That helps. Thank you very much.	13	the interface between the EWL slab and the diaphragm
14	Cross-examination by MR CHOW	14	wall; right?
15	MR CHOW: Good afternoon, Mr Southward.	15	In COWI's report, under various notes, it mentioned
16	A. Good afternoon.	16	that there are sections in which the result shows that
17	Q. I represent the government and I have some questions.	17	the percentage utilisation has gone up to 167 per cent.
18	Now we are all fresh in our minds as to what you said in	18	Do you recall that?
19	relation to those slides, I would prefer to start by	19	A. Yes.
20	taking you through some of the slides and I will try to	20	Q. And COWI takes the view that those results are
21	get further clarification from you, if you don't mind.	21	unrealistic I think this is the word that COWI used?
22	A. Sure.	22	A. Yes, I believe that, yes.
23	Q. When we were looking at slide 3, about the key areas,	23	Q. And dismissed that being a problem, a problematic area,
24	you mention that you base your view in relation to	24	but COWI offered no explanation whatsoever. Is that
25	redundancy by reference to the fact that three separate	25	what your understanding is as well?
	Page 142		Page 144
1			
1	consultants have carried out some checking. So you	1	A. Yes. I believe they've done a finite element analysis
1 2	consultants have carried out some checking. So you relied on the result of those checking in coming to your	1 2	A. Yes. I believe they've done a finite element analysis of the slab. The interpretation of these results can be
	- · ·		
2	relied on the result of those checking in coming to your view that the structure has extensive redundancy or spare capacity. Do you recall that?	2	of the slab. The interpretation of these results can be at times tricky. If the modelling is not 100 per cent, or sometimes even if it is 100 per cent, you will get
2 3	relied on the result of those checking in coming to your view that the structure has extensive redundancy or	2 3	of the slab. The interpretation of these results can be at times tricky. If the modelling is not 100 per cent,
2 3 4	<ul><li>relied on the result of those checking in coming to your view that the structure has extensive redundancy or spare capacity. Do you recall that?</li><li>A. I believe I said that, yes.</li><li>Q. You also mentioned Atkins, OAP and COWI as the three</li></ul>	2 3 4	of the slab. The interpretation of these results can be at times tricky. If the modelling is not 100 per cent, or sometimes even if it is 100 per cent, you will get discontinuities between changes in section, and those discontinuities can throw up isolated spots of very high
2 3 4 5	<ul><li>relied on the result of those checking in coming to your view that the structure has extensive redundancy or spare capacity. Do you recall that?</li><li>A. I believe I said that, yes.</li><li>Q. You also mentioned Atkins, OAP and COWI as the three consultants, their work you have relied on?</li></ul>	2 3 4 5	of the slab. The interpretation of these results can be at times tricky. If the modelling is not 100 per cent, or sometimes even if it is 100 per cent, you will get discontinuities between changes in section, and those discontinuities can throw up isolated spots of very high or very low results which don't make any sense and which
2 3 4 5 6	<ul><li>relied on the result of those checking in coming to your view that the structure has extensive redundancy or spare capacity. Do you recall that?</li><li>A. I believe I said that, yes.</li><li>Q. You also mentioned Atkins, OAP and COWI as the three consultants, their work you have relied on?</li><li>A. Yes.</li></ul>	2 3 4 5 6	of the slab. The interpretation of these results can be at times tricky. If the modelling is not 100 per cent, or sometimes even if it is 100 per cent, you will get discontinuities between changes in section, and those discontinuities can throw up isolated spots of very high or very low results which don't make any sense and which couldn't happen in reality, when you compare to the
2 3 4 5 6 7	<ul><li>relied on the result of those checking in coming to your view that the structure has extensive redundancy or spare capacity. Do you recall that?</li><li>A. I believe I said that, yes.</li><li>Q. You also mentioned Atkins, OAP and COWI as the three consultants, their work you have relied on?</li><li>A. Yes.</li><li>Q. Am I right to say that as far as Atkins' exercise is</li></ul>	2 3 4 5 6 7 8 9	of the slab. The interpretation of these results can be at times tricky. If the modelling is not 100 per cent, or sometimes even if it is 100 per cent, you will get discontinuities between changes in section, and those discontinuities can throw up isolated spots of very high or very low results which don't make any sense and which couldn't happen in reality, when you compare to the pieces of concrete immediately adjacent to that
2 3 4 5 6 7 8	<ul> <li>relied on the result of those checking in coming to your view that the structure has extensive redundancy or spare capacity. Do you recall that?</li> <li>A. I believe I said that, yes.</li> <li>Q. You also mentioned Atkins, OAP and COWI as the three consultants, their work you have relied on?</li> <li>A. Yes.</li> <li>Q. Am I right to say that as far as Atkins' exercise is concerned, what you have looked at is graphical</li> </ul>	2 3 4 5 6 7 8	of the slab. The interpretation of these results can be at times tricky. If the modelling is not 100 per cent, or sometimes even if it is 100 per cent, you will get discontinuities between changes in section, and those discontinuities can throw up isolated spots of very high or very low results which don't make any sense and which couldn't happen in reality, when you compare to the pieces of concrete immediately adjacent to that particular spot.
2 3 4 5 6 7 8 9 10 11	<ul> <li>relied on the result of those checking in coming to your view that the structure has extensive redundancy or spare capacity. Do you recall that?</li> <li>A. I believe I said that, yes.</li> <li>Q. You also mentioned Atkins, OAP and COWI as the three consultants, their work you have relied on?</li> <li>A. Yes.</li> <li>Q. Am I right to say that as far as Atkins' exercise is concerned, what you have looked at is graphical representation at various locations along the diaphragm</li> </ul>	2 3 4 5 6 7 8 9 10 11	<ul> <li>of the slab. The interpretation of these results can be at times tricky. If the modelling is not 100 per cent, or sometimes even if it is 100 per cent, you will get discontinuities between changes in section, and those discontinuities can throw up isolated spots of very high or very low results which don't make any sense and which couldn't happen in reality, when you compare to the pieces of concrete immediately adjacent to that particular spot.</li> <li>So it's not uncommon to get areas of to get</li> </ul>
2 3 4 5 6 7 8 9 10 11 12	<ul> <li>relied on the result of those checking in coming to your view that the structure has extensive redundancy or spare capacity. Do you recall that?</li> <li>A. I believe I said that, yes.</li> <li>Q. You also mentioned Atkins, OAP and COWI as the three consultants, their work you have relied on?</li> <li>A. Yes.</li> <li>Q. Am I right to say that as far as Atkins' exercise is concerned, what you have looked at is graphical representation at various locations along the diaphragm wall as the percentage reserve in terms of capacity; is</li> </ul>	2 3 4 5 6 7 8 9 10 11 12	<ul> <li>of the slab. The interpretation of these results can be at times tricky. If the modelling is not 100 per cent, or sometimes even if it is 100 per cent, you will get discontinuities between changes in section, and those discontinuities can throw up isolated spots of very high or very low results which don't make any sense and which couldn't happen in reality, when you compare to the pieces of concrete immediately adjacent to that particular spot.</li> <li>So it's not uncommon to get areas of to get isolated areas that have results which are not</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13	<ul> <li>relied on the result of those checking in coming to your view that the structure has extensive redundancy or spare capacity. Do you recall that?</li> <li>A. I believe I said that, yes.</li> <li>Q. You also mentioned Atkins, OAP and COWI as the three consultants, their work you have relied on?</li> <li>A. Yes.</li> <li>Q. Am I right to say that as far as Atkins' exercise is concerned, what you have looked at is graphical representation at various locations along the diaphragm wall as the percentage reserve in terms of capacity; is that right?</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13	<ul> <li>of the slab. The interpretation of these results can be at times tricky. If the modelling is not 100 per cent, or sometimes even if it is 100 per cent, you will get discontinuities between changes in section, and those discontinuities can throw up isolated spots of very high or very low results which don't make any sense and which couldn't happen in reality, when you compare to the pieces of concrete immediately adjacent to that particular spot.</li> <li>So it's not uncommon to get areas of to get isolated areas that have results which are not meaningful. So if it's not a meaningful result, then</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14	<ul> <li>relied on the result of those checking in coming to your view that the structure has extensive redundancy or spare capacity. Do you recall that?</li> <li>A. I believe I said that, yes.</li> <li>Q. You also mentioned Atkins, OAP and COWI as the three consultants, their work you have relied on?</li> <li>A. Yes.</li> <li>Q. Am I right to say that as far as Atkins' exercise is concerned, what you have looked at is graphical representation at various locations along the diaphragm wall as the percentage reserve in terms of capacity; is that right?</li> <li>A. Yes. Yes.</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14	<ul> <li>of the slab. The interpretation of these results can be at times tricky. If the modelling is not 100 per cent, or sometimes even if it is 100 per cent, you will get discontinuities between changes in section, and those discontinuities can throw up isolated spots of very high or very low results which don't make any sense and which couldn't happen in reality, when you compare to the pieces of concrete immediately adjacent to that particular spot.</li> <li>So it's not uncommon to get areas of to get isolated areas that have results which are not meaningful. So if it's not a meaningful result, then it's not a result to use.</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15	<ul> <li>relied on the result of those checking in coming to your view that the structure has extensive redundancy or spare capacity. Do you recall that?</li> <li>A. I believe I said that, yes.</li> <li>Q. You also mentioned Atkins, OAP and COWI as the three consultants, their work you have relied on?</li> <li>A. Yes.</li> <li>Q. Am I right to say that as far as Atkins' exercise is concerned, what you have looked at is graphical representation at various locations along the diaphragm wall as the percentage reserve in terms of capacity; is that right?</li> <li>A. Yes.</li> <li>Q. Atkins have not provided any supporting calculation or</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15	<ul> <li>of the slab. The interpretation of these results can be at times tricky. If the modelling is not 100 per cent, or sometimes even if it is 100 per cent, you will get discontinuities between changes in section, and those discontinuities can throw up isolated spots of very high or very low results which don't make any sense and which couldn't happen in reality, when you compare to the pieces of concrete immediately adjacent to that particular spot.</li> <li>So it's not uncommon to get areas of to get isolated areas that have results which are not meaningful. So if it's not a meaningful result, then it's not a result to use.</li> <li>Q. From my recollection, those stresses which according to</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	<ul> <li>relied on the result of those checking in coming to your view that the structure has extensive redundancy or spare capacity. Do you recall that?</li> <li>A. I believe I said that, yes.</li> <li>Q. You also mentioned Atkins, OAP and COWI as the three consultants, their work you have relied on?</li> <li>A. Yes.</li> <li>Q. Am I right to say that as far as Atkins' exercise is concerned, what you have looked at is graphical representation at various locations along the diaphragm wall as the percentage reserve in terms of capacity; is that right?</li> <li>A. Yes.</li> <li>Q. Atkins have not provided any supporting calculation or details of the assessment?</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	<ul> <li>of the slab. The interpretation of these results can be at times tricky. If the modelling is not 100 per cent, or sometimes even if it is 100 per cent, you will get discontinuities between changes in section, and those discontinuities can throw up isolated spots of very high or very low results which don't make any sense and which couldn't happen in reality, when you compare to the pieces of concrete immediately adjacent to that particular spot.</li> <li>So it's not uncommon to get areas of to get isolated areas that have results which are not meaningful. So if it's not a meaningful result, then it's not a result to use.</li> <li>Q. From my recollection, those stresses which according to the result of COWI's analysis, that amount to</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	<ul> <li>relied on the result of those checking in coming to your view that the structure has extensive redundancy or spare capacity. Do you recall that?</li> <li>A. I believe I said that, yes.</li> <li>Q. You also mentioned Atkins, OAP and COWI as the three consultants, their work you have relied on?</li> <li>A. Yes.</li> <li>Q. Am I right to say that as far as Atkins' exercise is concerned, what you have looked at is graphical representation at various locations along the diaphragm wall as the percentage reserve in terms of capacity; is that right?</li> <li>A. Yes.</li> <li>Q. Atkins have not provided any supporting calculation or details of the assessment?</li> <li>A. No.</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	<ul> <li>of the slab. The interpretation of these results can be at times tricky. If the modelling is not 100 per cent, or sometimes even if it is 100 per cent, you will get discontinuities between changes in section, and those discontinuities can throw up isolated spots of very high or very low results which don't make any sense and which couldn't happen in reality, when you compare to the pieces of concrete immediately adjacent to that particular spot.</li> <li>So it's not uncommon to get areas of to get isolated areas that have results which are not meaningful. So if it's not a meaningful result, then it's not a result to use.</li> <li>Q. From my recollection, those stresses which according to the result of COWI's analysis, that amount to 167 per cent utilisation, are shear stress; correct?</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	<ul> <li>relied on the result of those checking in coming to your view that the structure has extensive redundancy or spare capacity. Do you recall that?</li> <li>A. I believe I said that, yes.</li> <li>Q. You also mentioned Atkins, OAP and COWI as the three consultants, their work you have relied on?</li> <li>A. Yes.</li> <li>Q. Am I right to say that as far as Atkins' exercise is concerned, what you have looked at is graphical representation at various locations along the diaphragm wall as the percentage reserve in terms of capacity; is that right?</li> <li>A. Yes.</li> <li>Q. Atkins have not provided any supporting calculation or details of the assessment?</li> <li>A. No.</li> <li>Q. And as far as OAP's work is concerned, what I have found</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	<ul> <li>of the slab. The interpretation of these results can be at times tricky. If the modelling is not 100 per cent, or sometimes even if it is 100 per cent, you will get discontinuities between changes in section, and those discontinuities can throw up isolated spots of very high or very low results which don't make any sense and which couldn't happen in reality, when you compare to the pieces of concrete immediately adjacent to that particular spot.</li> <li>So it's not uncommon to get areas of to get isolated areas that have results which are not meaningful. So if it's not a meaningful result, then it's not a result to use.</li> <li>Q. From my recollection, those stresses which according to the result of COWI's analysis, that amount to 167 per cent utilisation, are shear stress; correct?</li> <li>A. I have to say I can't remember.</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	<ul> <li>relied on the result of those checking in coming to your view that the structure has extensive redundancy or spare capacity. Do you recall that?</li> <li>A. I believe I said that, yes.</li> <li>Q. You also mentioned Atkins, OAP and COWI as the three consultants, their work you have relied on?</li> <li>A. Yes.</li> <li>Q. Am I right to say that as far as Atkins' exercise is concerned, what you have looked at is graphical representation at various locations along the diaphragm wall as the percentage reserve in terms of capacity; is that right?</li> <li>A. Yes.</li> <li>Q. Atkins have not provided any supporting calculation or details of the assessment?</li> <li>A. No.</li> <li>Q. And as far as OAP's work is concerned, what I have found from the hearing bundles are 30 or 40-odd pages of</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	<ul> <li>of the slab. The interpretation of these results can be at times tricky. If the modelling is not 100 per cent, or sometimes even if it is 100 per cent, you will get discontinuities between changes in section, and those discontinuities can throw up isolated spots of very high or very low results which don't make any sense and which couldn't happen in reality, when you compare to the pieces of concrete immediately adjacent to that particular spot.</li> <li>So it's not uncommon to get areas of to get isolated areas that have results which are not meaningful. So if it's not a meaningful result, then it's not a result to use.</li> <li>Q. From my recollection, those stresses which according to the result of COWI's analysis, that amount to 167 per cent utilisation, are shear stress; correct?</li> <li>A. I have to say I can't remember.</li> <li>Q. Perhaps I can take you to COWI's report. I believe it's</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	<ul> <li>relied on the result of those checking in coming to your view that the structure has extensive redundancy or spare capacity. Do you recall that?</li> <li>A. I believe I said that, yes.</li> <li>Q. You also mentioned Atkins, OAP and COWI as the three consultants, their work you have relied on?</li> <li>A. Yes.</li> <li>Q. Am I right to say that as far as Atkins' exercise is concerned, what you have looked at is graphical representation at various locations along the diaphragm wall as the percentage reserve in terms of capacity; is that right?</li> <li>A. Yes.</li> <li>Q. Atkins have not provided any supporting calculation or details of the assessment?</li> <li>A. No.</li> <li>Q. And as far as OAP's work is concerned, what I have found from the hearing bundles are 30 or 40-odd pages of design checking which OAP described as spot-checks.</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	<ul> <li>of the slab. The interpretation of these results can be at times tricky. If the modelling is not 100 per cent, or sometimes even if it is 100 per cent, you will get discontinuities between changes in section, and those discontinuities can throw up isolated spots of very high or very low results which don't make any sense and which couldn't happen in reality, when you compare to the pieces of concrete immediately adjacent to that particular spot.</li> <li>So it's not uncommon to get areas of to get isolated areas that have results which are not meaningful. So if it's not a meaningful result, then it's not a result to use.</li> <li>Q. From my recollection, those stresses which according to the result of COWI's analysis, that amount to 167 per cent utilisation, are shear stress; correct?</li> <li>A. I have to say I can't remember.</li> <li>Q. Perhaps I can take you to COWI's report. I believe it's in tab</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	<ul> <li>relied on the result of those checking in coming to your view that the structure has extensive redundancy or spare capacity. Do you recall that?</li> <li>A. I believe I said that, yes.</li> <li>Q. You also mentioned Atkins, OAP and COWI as the three consultants, their work you have relied on?</li> <li>A. Yes.</li> <li>Q. Am I right to say that as far as Atkins' exercise is concerned, what you have looked at is graphical representation at various locations along the diaphragm wall as the percentage reserve in terms of capacity; is that right?</li> <li>A. Yes.</li> <li>Q. Atkins have not provided any supporting calculation or details of the assessment?</li> <li>A. No.</li> <li>Q. And as far as OAP's work is concerned, what I have found from the hearing bundles are 30 or 40-odd pages of design checking which OAP described as spot-checks.</li> <li>A. Yes.</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	<ul> <li>of the slab. The interpretation of these results can be at times tricky. If the modelling is not 100 per cent, or sometimes even if it is 100 per cent, you will get discontinuities between changes in section, and those discontinuities can throw up isolated spots of very high or very low results which don't make any sense and which couldn't happen in reality, when you compare to the pieces of concrete immediately adjacent to that particular spot.</li> <li>So it's not uncommon to get areas of to get isolated areas that have results which are not meaningful. So if it's not a meaningful result, then it's not a result to use.</li> <li>Q. From my recollection, those stresses which according to the result of COWI's analysis, that amount to 167 per cent utilisation, are shear stress; correct?</li> <li>A. I have to say I can't remember.</li> <li>Q. Perhaps I can take you to COWI's report. I believe it's in tab</li> <li>MR PENNICOTT: 4.</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>relied on the result of those checking in coming to your view that the structure has extensive redundancy or spare capacity. Do you recall that?</li> <li>A. I believe I said that, yes.</li> <li>Q. You also mentioned Atkins, OAP and COWI as the three consultants, their work you have relied on?</li> <li>A. Yes.</li> <li>Q. Am I right to say that as far as Atkins' exercise is concerned, what you have looked at is graphical representation at various locations along the diaphragm wall as the percentage reserve in terms of capacity; is that right?</li> <li>A. Yes. Yes.</li> <li>Q. Atkins have not provided any supporting calculation or details of the assessment?</li> <li>A. No.</li> <li>Q. And as far as OAP's work is concerned, what I have found from the hearing bundles are 30 or 40-odd pages of design checking which OAP described as spot-checks.</li> <li>A. Yes.</li> <li>Q. Is that also what you have looked at as well? Is that</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>of the slab. The interpretation of these results can be at times tricky. If the modelling is not 100 per cent, or sometimes even if it is 100 per cent, you will get discontinuities between changes in section, and those discontinuities can throw up isolated spots of very high or very low results which don't make any sense and which couldn't happen in reality, when you compare to the pieces of concrete immediately adjacent to that particular spot.</li> <li>So it's not uncommon to get areas of to get isolated areas that have results which are not meaningful. So if it's not a meaningful result, then it's not a result to use.</li> <li>Q. From my recollection, those stresses which according to the result of COWI's analysis, that amount to 167 per cent utilisation, are shear stress; correct?</li> <li>A. I have to say I can't remember.</li> <li>Q. Perhaps I can take you to COWI's report. I believe it's in tab</li> <li>MR CHOW: 6.</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	<ul> <li>relied on the result of those checking in coming to your view that the structure has extensive redundancy or spare capacity. Do you recall that?</li> <li>A. I believe I said that, yes.</li> <li>Q. You also mentioned Atkins, OAP and COWI as the three consultants, their work you have relied on?</li> <li>A. Yes.</li> <li>Q. Am I right to say that as far as Atkins' exercise is concerned, what you have looked at is graphical representation at various locations along the diaphragm wall as the percentage reserve in terms of capacity; is that right?</li> <li>A. Yes.</li> <li>Q. Atkins have not provided any supporting calculation or details of the assessment?</li> <li>A. No.</li> <li>Q. And as far as OAP's work is concerned, what I have found from the hearing bundles are 30 or 40-odd pages of design checking which OAP described as spot-checks.</li> <li>A. Yes.</li> <li>Q. Is that also what you have looked at and relied on; is</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	<ul> <li>of the slab. The interpretation of these results can be at times tricky. If the modelling is not 100 per cent, or sometimes even if it is 100 per cent, you will get discontinuities between changes in section, and those discontinuities can throw up isolated spots of very high or very low results which don't make any sense and which couldn't happen in reality, when you compare to the pieces of concrete immediately adjacent to that particular spot.</li> <li>So it's not uncommon to get areas of to get isolated areas that have results which are not meaningful. So if it's not a meaningful result, then it's not a result to use.</li> <li>Q. From my recollection, those stresses which according to the result of COWI's analysis, that amount to 167 per cent utilisation, are shear stress; correct?</li> <li>A. I have to say I can't remember.</li> <li>Q. Perhaps I can take you to COWI's report. I believe it's in tab</li> <li>MR PENNICOTT: 4.</li> <li>MR PENNICOTT: Tab 4.</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>relied on the result of those checking in coming to your view that the structure has extensive redundancy or spare capacity. Do you recall that?</li> <li>A. I believe I said that, yes.</li> <li>Q. You also mentioned Atkins, OAP and COWI as the three consultants, their work you have relied on?</li> <li>A. Yes.</li> <li>Q. Am I right to say that as far as Atkins' exercise is concerned, what you have looked at is graphical representation at various locations along the diaphragm wall as the percentage reserve in terms of capacity; is that right?</li> <li>A. Yes. Yes.</li> <li>Q. Atkins have not provided any supporting calculation or details of the assessment?</li> <li>A. No.</li> <li>Q. And as far as OAP's work is concerned, what I have found from the hearing bundles are 30 or 40-odd pages of design checking which OAP described as spot-checks.</li> <li>A. Yes.</li> <li>Q. Is that also what you have looked at as well? Is that</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>of the slab. The interpretation of these results can be at times tricky. If the modelling is not 100 per cent, or sometimes even if it is 100 per cent, you will get discontinuities between changes in section, and those discontinuities can throw up isolated spots of very high or very low results which don't make any sense and which couldn't happen in reality, when you compare to the pieces of concrete immediately adjacent to that particular spot.</li> <li>So it's not uncommon to get areas of to get isolated areas that have results which are not meaningful. So if it's not a meaningful result, then it's not a result to use.</li> <li>Q. From my recollection, those stresses which according to the result of COWI's analysis, that amount to 167 per cent utilisation, are shear stress; correct?</li> <li>A. I have to say I can't remember.</li> <li>Q. Perhaps I can take you to COWI's report. I believe it's in tab</li> <li>MR PENNICOTT: 4.</li> </ul>

	Page 145		Page 147
1	Yes, page 34 is a table showing the shear force	1	behaviour of the wall and the slab is not being
2	range of utilisation; do you see that?	2	represented properly in the model, because there is no
3	A. Yes.	3	other side, so the results could not be realistic.
4	Q. And under notes 6 there is a note saying:	4	COMMISSIONER HANSFORD: So, Mr Southward, obviously it's for
5	"Panel WH128 has a utilisation of 161 per cent.	5	COWI to answer the government's questions.
6	However this shear is at the extremity of the model and	6	A. Indeed.
7	not considered realistic."	7	COMMISSIONER HANSFORD: However, that's an explanation, but
8	If we go to page 44, the last page of the main body	8	you're saying I think you're saying
9	of the report, again it's a table setting out the shear	9	A. I think they say yes, they've said that it's at
10	force range of utilisation. Under note 3, it is	10	an end panel, so that would be my interpretation of the
11	recorded:	11	reason why it's overstressed.
12	"The utilisation of 161 per cent occurs at	12	COMMISSIONER HANSFORD: So is it the case, Mr Southward,
13	panel WH128."	13	that any computer model is only as good as the
14	This overstress, if I may use that term, according	14	assumptions in that model and they may or may not fully
15	to the result of the analysis, relates to shear stress,	15	represent reality?
16	not bending moment; right?	16	A. Only as good as the assumptions made, how it's modelled,
17	A. Yes.	17	how the results are interpreted. It's one big melting
18	Q. Do you agree that failure by shear is a brittle failure,	18	pot and you've got to work through it very carefully to
19	without any sign?	19	get the results.
20	A. Yes, failure by shear would be a brittle failure, yes.	20	COMMISSIONER HANSFORD: It's like a consultant interpreting
21	Q. Actually, one of we have prepared a list of questions	21	medical results.
22	and I believe it has been sent off to COWI for COWI's	22	A. Luckily, I've not had much experience of that.
23	clarification. One of the questions, I hope I would	23	COMMISSIONER HANSFORD: I've had a little bit.
24	like you to tell us whether you have any view on that.	24	But, you know, these questions on this subject from
25	A. I have not read those questions, so I can't have a view.	25	Mr Chow are very valid and important questions for COWI
	Page 146		Page 148
1	Page 146 Q. I will let you know. One of these questions is this:	1	Page 148 to answer.
1 2			-
	Q. I will let you know. One of these questions is this:		to answer. A. Indeed. COMMISSIONER HANSFORD: But they have actually given their
2	Q. I will let you know. One of these questions is this: given the computer calculation has shown some what COWI	2	to answer. A. Indeed. COMMISSIONER HANSFORD: But they have actually given their conclusions, I see, on page 39 of their report, and
2 3	Q. I will let you know. One of these questions is this: given the computer calculation has shown some what COWI describe as irregular result or unrealistic result, and	2 3	to answer. A. Indeed. COMMISSIONER HANSFORD: But they have actually given their conclusions, I see, on page 39 of their report, and indeed they address shear in items 2, 3 and 4. But that
2 3 4	Q. I will let you know. One of these questions is this: given the computer calculation has shown some what COWI describe as irregular result or unrealistic result, and it happens that those so-called unrealistic result seems to suggest that there were overstress in the structure now, COWI dismissed those as reliable	2 3 4	to answer. A. Indeed. COMMISSIONER HANSFORD: But they have actually given their conclusions, I see, on page 39 of their report, and
2 3 4 5	Q. I will let you know. One of these questions is this: given the computer calculation has shown some what COWI describe as irregular result or unrealistic result, and it happens that those so-called unrealistic result seems to suggest that there were overstress in the structure now, COWI dismissed those as reliable results. Our question to COWI is that if the same	2 3 4 5	to answer. A. Indeed. COMMISSIONER HANSFORD: But they have actually given their conclusions, I see, on page 39 of their report, and indeed they address shear in items 2, 3 and 4. But that doesn't invalidate Mr Chow's questions that they need to address.
2 3 4 5 6 7 8	Q. I will let you know. One of these questions is this: given the computer calculation has shown some what COWI describe as irregular result or unrealistic result, and it happens that those so-called unrealistic result seems to suggest that there were overstress in the structure now, COWI dismissed those as reliable results. Our question to COWI is that if the same computer calculation showed part of the result which are	2 3 4 5 6	to answer. A. Indeed. COMMISSIONER HANSFORD: But they have actually given their conclusions, I see, on page 39 of their report, and indeed they address shear in items 2, 3 and 4. But that doesn't invalidate Mr Chow's questions that they need to address. A. Yes.
2 3 4 5 6 7 8 9	Q. I will let you know. One of these questions is this: given the computer calculation has shown some what COWI describe as irregular result or unrealistic result, and it happens that those so-called unrealistic result seems to suggest that there were overstress in the structure now, COWI dismissed those as reliable results. Our question to COWI is that if the same computer calculation showed part of the result which are unrealistic, how can we be assured that results for	2 3 4 5 6 7	<ul> <li>to answer.</li> <li>A. Indeed.</li> <li>COMMISSIONER HANSFORD: But they have actually given their conclusions, I see, on page 39 of their report, and indeed they address shear in items 2, 3 and 4. But that doesn't invalidate Mr Chow's questions that they need to address.</li> <li>A. Yes.</li> <li>COMMISSIONER HANSFORD: Would you agree with that?</li> </ul>
2 3 4 5 6 7 8 9 10	Q. I will let you know. One of these questions is this: given the computer calculation has shown some what COWI describe as irregular result or unrealistic result, and it happens that those so-called unrealistic result seems to suggest that there were overstress in the structure now, COWI dismissed those as reliable results. Our question to COWI is that if the same computer calculation showed part of the result which are unrealistic, how can we be assured that results for other locations are reliable? Would it suggest that the	2 3 4 5 6 7 8 9 10	to answer. A. Indeed. COMMISSIONER HANSFORD: But they have actually given their conclusions, I see, on page 39 of their report, and indeed they address shear in items 2, 3 and 4. But that doesn't invalidate Mr Chow's questions that they need to address. A. Yes. COMMISSIONER HANSFORD: Would you agree with that? A. Yes, sure.
2 3 4 5 6 7 8 9 10 11	Q. I will let you know. One of these questions is this: given the computer calculation has shown some what COWI describe as irregular result or unrealistic result, and it happens that those so-called unrealistic result seems to suggest that there were overstress in the structure now, COWI dismissed those as reliable results. Our question to COWI is that if the same computer calculation showed part of the result which are unrealistic, how can we be assured that results for other locations are reliable? Would it suggest that the modelling itself has some problem?	2 3 4 5 6 7 8 9 10 11	to answer. A. Indeed. COMMISSIONER HANSFORD: But they have actually given their conclusions, I see, on page 39 of their report, and indeed they address shear in items 2, 3 and 4. But that doesn't invalidate Mr Chow's questions that they need to address. A. Yes. COMMISSIONER HANSFORD: Would you agree with that? A. Yes, sure. MR CHOW: Thank you, Prof Hansford.
2 3 4 5 6 7 8 9 10 11 12	<ul> <li>Q. I will let you know. One of these questions is this: given the computer calculation has shown some what COWI describe as irregular result or unrealistic result, and it happens that those so-called unrealistic result seems to suggest that there were overstress in the structure now, COWI dismissed those as reliable results. Our question to COWI is that if the same computer calculation showed part of the result which are unrealistic, how can we be assured that results for other locations are reliable? Would it suggest that the modelling itself has some problem?</li> <li>A. Well, they've only modelled they've modelled three</li> </ul>	2 3 4 5 6 7 8 9 10 11 12	<ul> <li>to answer.</li> <li>A. Indeed.</li> <li>COMMISSIONER HANSFORD: But they have actually given their conclusions, I see, on page 39 of their report, and indeed they address shear in items 2, 3 and 4. But that doesn't invalidate Mr Chow's questions that they need to address.</li> <li>A. Yes.</li> <li>COMMISSIONER HANSFORD: Would you agree with that?</li> <li>A. Yes, sure.</li> <li>MR CHOW: Thank you, Prof Hansford. <ul> <li>I would like to move on to another slide, page 16,</li> </ul> </li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13	<ul> <li>Q. I will let you know. One of these questions is this: given the computer calculation has shown some what COWI describe as irregular result or unrealistic result, and it happens that those so-called unrealistic result seems to suggest that there were overstress in the structure now, COWI dismissed those as reliable results. Our question to COWI is that if the same computer calculation showed part of the result which are unrealistic, how can we be assured that results for other locations are reliable? Would it suggest that the modelling itself has some problem?</li> <li>A. Well, they've only modelled they've modelled three discrete areas of the station, so in that, in those</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13	<ul> <li>to answer.</li> <li>A. Indeed.</li> <li>COMMISSIONER HANSFORD: But they have actually given their conclusions, I see, on page 39 of their report, and indeed they address shear in items 2, 3 and 4. But that doesn't invalidate Mr Chow's questions that they need to address.</li> <li>A. Yes.</li> <li>COMMISSIONER HANSFORD: Would you agree with that?</li> <li>A. Yes, sure.</li> <li>MR CHOW: Thank you, Prof Hansford. <ul> <li>I would like to move on to another slide, page 16, please, where you talk about the test result.</li> </ul> </li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14	<ul> <li>Q. I will let you know. One of these questions is this: given the computer calculation has shown some what COWI describe as irregular result or unrealistic result, and it happens that those so-called unrealistic result seems to suggest that there were overstress in the structure now, COWI dismissed those as reliable results. Our question to COWI is that if the same computer calculation showed part of the result which are unrealistic, how can we be assured that results for other locations are reliable? Would it suggest that the modelling itself has some problem?</li> <li>A. Well, they've only modelled they've modelled three discrete areas of the station, so in that, in those three discrete areas, there are only going to be</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14	<ul> <li>to answer.</li> <li>A. Indeed.</li> <li>COMMISSIONER HANSFORD: But they have actually given their conclusions, I see, on page 39 of their report, and indeed they address shear in items 2, 3 and 4. But that doesn't invalidate Mr Chow's questions that they need to address.</li> <li>A. Yes.</li> <li>COMMISSIONER HANSFORD: Would you agree with that?</li> <li>A. Yes, sure.</li> <li>MR CHOW: Thank you, Prof Hansford. <ul> <li>I would like to move on to another slide, page 16, please, where you talk about the test result.</li> <li>I recall what you said is at one point you said</li> </ul> </li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15	<ul> <li>Q. I will let you know. One of these questions is this: given the computer calculation has shown some what COWI describe as irregular result or unrealistic result, and it happens that those so-called unrealistic result seems to suggest that there were overstress in the structure now, COWI dismissed those as reliable results. Our question to COWI is that if the same computer calculation showed part of the result which are unrealistic, how can we be assured that results for other locations are reliable? Would it suggest that the modelling itself has some problem?</li> <li>A. Well, they've only modelled they've modelled three discrete areas of the station, so in that, in those three discrete areas, there are only going to be specific parts of that model that are going to give</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15	<ul> <li>to answer.</li> <li>A. Indeed.</li> <li>COMMISSIONER HANSFORD: But they have actually given their conclusions, I see, on page 39 of their report, and indeed they address shear in items 2, 3 and 4. But that doesn't invalidate Mr Chow's questions that they need to address.</li> <li>A. Yes.</li> <li>COMMISSIONER HANSFORD: Would you agree with that?</li> <li>A. Yes, sure.</li> <li>MR CHOW: Thank you, Prof Hansford. <ul> <li>I would like to move on to another slide, page 16, please, where you talk about the test result.</li> <li>I recall what you said is at one point you said there is only one sample tested; you would welcome that</li> </ul> </li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	<ul> <li>Q. I will let you know. One of these questions is this: given the computer calculation has shown some what COWI describe as irregular result or unrealistic result, and it happens that those so-called unrealistic result seems to suggest that there were overstress in the structure now, COWI dismissed those as reliable results. Our question to COWI is that if the same computer calculation showed part of the result which are unrealistic, how can we be assured that results for other locations are reliable? Would it suggest that the modelling itself has some problem?</li> <li>A. Well, they've only modelled they've modelled three discrete areas of the station, so in that, in those three discrete areas, there are only going to be specific parts of that model that are going to give realistic answers.</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	<ul> <li>to answer.</li> <li>A. Indeed.</li> <li>COMMISSIONER HANSFORD: But they have actually given their conclusions, I see, on page 39 of their report, and indeed they address shear in items 2, 3 and 4. But that doesn't invalidate Mr Chow's questions that they need to address.</li> <li>A. Yes.</li> <li>COMMISSIONER HANSFORD: Would you agree with that?</li> <li>A. Yes, sure.</li> <li>MR CHOW: Thank you, Prof Hansford. <ul> <li>I would like to move on to another slide, page 16, please, where you talk about the test result.</li> <li>I recall what you said is at one point you said there is only one sample tested; you would welcome that if more samples should be tested, then the result may be</li> </ul> </li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	<ul> <li>Q. I will let you know. One of these questions is this: given the computer calculation has shown some what COWI describe as irregular result or unrealistic result, and it happens that those so-called unrealistic result seems to suggest that there were overstress in the structure now, COWI dismissed those as reliable results. Our question to COWI is that if the same computer calculation showed part of the result which are unrealistic, how can we be assured that results for other locations are reliable? Would it suggest that the modelling itself has some problem?</li> <li>A. Well, they've only modelled they've modelled three discrete areas of the station, so in that, in those three discrete areas, there are only going to be specific parts of that model that are going to give realistic answers.</li> <li>You've seen it says that there was one failure which</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	<ul> <li>to answer.</li> <li>A. Indeed.</li> <li>COMMISSIONER HANSFORD: But they have actually given their conclusions, I see, on page 39 of their report, and indeed they address shear in items 2, 3 and 4. But that doesn't invalidate Mr Chow's questions that they need to address.</li> <li>A. Yes.</li> <li>COMMISSIONER HANSFORD: Would you agree with that?</li> <li>A. Yes, sure.</li> <li>MR CHOW: Thank you, Prof Hansford. <ul> <li>I would like to move on to another slide, page 16, please, where you talk about the test result.</li> <li>I recall what you said is at one point you said there is only one sample tested; you would welcome that if more samples should be tested, then the result may be more reliable. Do you recall that?</li> </ul> </li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	<ul> <li>Q. I will let you know. One of these questions is this: given the computer calculation has shown some what COWI describe as irregular result or unrealistic result, and it happens that those so-called unrealistic result seems to suggest that there were overstress in the structure now, COWI dismissed those as reliable results. Our question to COWI is that if the same computer calculation showed part of the result which are unrealistic, how can we be assured that results for other locations are reliable? Would it suggest that the modelling itself has some problem?</li> <li>A. Well, they've only modelled they've modelled three discrete areas of the station, so in that, in those three discrete areas, there are only going to be specific parts of that model that are going to give realistic answers.</li> <li>You've seen it says that there was one failure which was a shear failure in an end panel in their model.</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	<ul> <li>to answer.</li> <li>A. Indeed.</li> <li>COMMISSIONER HANSFORD: But they have actually given their conclusions, I see, on page 39 of their report, and indeed they address shear in items 2, 3 and 4. But that doesn't invalidate Mr Chow's questions that they need to address.</li> <li>A. Yes.</li> <li>COMMISSIONER HANSFORD: Would you agree with that?</li> <li>A. Yes, sure.</li> <li>MR CHOW: Thank you, Prof Hansford. <ul> <li>I would like to move on to another slide, page 16, please, where you talk about the test result.</li> <li>I recall what you said is at one point you said there is only one sample tested; you would welcome that if more samples should be tested, then the result may be more reliable. Do you recall that?</li> </ul> </li> <li>A. I can't recall exactly what I said. I don't think</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	<ul> <li>Q. I will let you know. One of these questions is this: given the computer calculation has shown some what COWI describe as irregular result or unrealistic result, and it happens that those so-called unrealistic result seems to suggest that there were overstress in the structure now, COWI dismissed those as reliable results. Our question to COWI is that if the same computer calculation showed part of the result which are unrealistic, how can we be assured that results for other locations are reliable? Would it suggest that the modelling itself has some problem?</li> <li>A. Well, they've only modelled they've modelled three discrete areas of the station, so in that, in those three discrete areas, there are only going to be specific parts of that model that are going to give realistic answers.</li> <li>You've seen it says that there was one failure which was a shear failure in an end panel in their model. Because it's an end panel, it's at the boundary, so the</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	<ul> <li>to answer.</li> <li>A. Indeed.</li> <li>COMMISSIONER HANSFORD: But they have actually given their conclusions, I see, on page 39 of their report, and indeed they address shear in items 2, 3 and 4. But that doesn't invalidate Mr Chow's questions that they need to address.</li> <li>A. Yes.</li> <li>COMMISSIONER HANSFORD: Would you agree with that?</li> <li>A. Yes, sure.</li> <li>MR CHOW: Thank you, Prof Hansford. <ul> <li>I would like to move on to another slide, page 16, please, where you talk about the test result.</li> <li>I recall what you said is at one point you said there is only one sample tested; you would welcome that if more samples should be tested, then the result may be more reliable. Do you recall that?</li> </ul> </li> <li>A. I can't recall exactly what I said. I don't think I said that.</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	<ul> <li>Q. I will let you know. One of these questions is this: given the computer calculation has shown some what COWI describe as irregular result or unrealistic result, and it happens that those so-called unrealistic result seems to suggest that there were overstress in the structure now, COWI dismissed those as reliable results. Our question to COWI is that if the same computer calculation showed part of the result which are unrealistic, how can we be assured that results for other locations are reliable? Would it suggest that the modelling itself has some problem?</li> <li>A. Well, they've only modelled they've modelled three discrete areas of the station, so in that, in those three discrete areas, there are only going to be specific parts of that model that are going to give realistic answers.</li> <li>You've seen it says that there was one failure which was a shear failure in an end panel in their model. Because it's an end panel, it's at the boundary, so the results in that would be completely unreliable.</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	<ul> <li>to answer.</li> <li>A. Indeed.</li> <li>COMMISSIONER HANSFORD: But they have actually given their conclusions, I see, on page 39 of their report, and indeed they address shear in items 2, 3 and 4. But that doesn't invalidate Mr Chow's questions that they need to address.</li> <li>A. Yes.</li> <li>COMMISSIONER HANSFORD: Would you agree with that?</li> <li>A. Yes, sure.</li> <li>MR CHOW: Thank you, Prof Hansford. <ul> <li>I would like to move on to another slide, page 16, please, where you talk about the test result.</li> <li>I recall what you said is at one point you said there is only one sample tested; you would welcome that if more samples should be tested, then the result may be more reliable. Do you recall that?</li> </ul> </li> <li>A. I can't recall exactly what I said. I don't think I said that.</li> <li>MR PENNICOTT: I didn't hear that either.</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	<ul> <li>Q. I will let you know. One of these questions is this: given the computer calculation has shown some what COWI describe as irregular result or unrealistic result, and it happens that those so-called unrealistic result seems to suggest that there were overstress in the structure now, COWI dismissed those as reliable results. Our question to COWI is that if the same computer calculation showed part of the result which are unrealistic, how can we be assured that results for other locations are reliable? Would it suggest that the modelling itself has some problem?</li> <li>A. Well, they've only modelled they've modelled three discrete areas of the station, so in that, in those three discrete areas, there are only going to be specific parts of that model that are going to give realistic answers.</li> <li>You've seen it says that there was one failure which was a shear failure in an end panel in their model. Because it's an end panel, it's at the boundary, so the results in that would be completely unreliable.</li> <li>Q. Why is that?</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	<ul> <li>to answer.</li> <li>A. Indeed.</li> <li>COMMISSIONER HANSFORD: But they have actually given their conclusions, I see, on page 39 of their report, and indeed they address shear in items 2, 3 and 4. But that doesn't invalidate Mr Chow's questions that they need to address.</li> <li>A. Yes.</li> <li>COMMISSIONER HANSFORD: Would you agree with that?</li> <li>A. Yes, sure.</li> <li>MR CHOW: Thank you, Prof Hansford. <ul> <li>I would like to move on to another slide, page 16, please, where you talk about the test result.</li> <li>I recall what you said is at one point you said there is only one sample tested; you would welcome that if more samples should be tested, then the result may be more reliable. Do you recall that?</li> </ul> </li> <li>A. I can't recall exactly what I said. I don't think I said that.</li> <li>MR PENNICOTT: I didn't hear that either.</li> <li>A. I just said, "These are the tests."</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>Q. I will let you know. One of these questions is this: given the computer calculation has shown some what COWI describe as irregular result or unrealistic result, and it happens that those so-called unrealistic result seems to suggest that there were overstress in the structure now, COWI dismissed those as reliable results. Our question to COWI is that if the same computer calculation showed part of the result which are unrealistic, how can we be assured that results for other locations are reliable? Would it suggest that the modelling itself has some problem?</li> <li>A. Well, they've only modelled they've modelled three discrete areas of the station, so in that, in those three discrete areas, there are only going to be specific parts of that model that are going to give realistic answers.</li> <li>You've seen it says that there was one failure which was a shear failure in an end panel in their model. Because it's an end panel, it's at the boundary, so the results in that would be completely unreliable.</li> <li>Q. Why is that?</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>to answer.</li> <li>A. Indeed.</li> <li>COMMISSIONER HANSFORD: But they have actually given their conclusions, I see, on page 39 of their report, and indeed they address shear in items 2, 3 and 4. But that doesn't invalidate Mr Chow's questions that they need to address.</li> <li>A. Yes.</li> <li>COMMISSIONER HANSFORD: Would you agree with that?</li> <li>A. Yes, sure.</li> <li>MR CHOW: Thank you, Prof Hansford. <ul> <li>I would like to move on to another slide, page 16, please, where you talk about the test result.</li> <li>I recall what you said is at one point you said there is only one sample tested; you would welcome that if more samples should be tested, then the result may be more reliable. Do you recall that?</li> </ul> </li> <li>A. I can't recall exactly what I said. I don't think I said that.</li> <li>MR PENNICOTT: I didn't hear that either.</li> <li>A. I just said, "These are the tests."</li> <li>CHAIRMAN: Sorry, where</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	<ul> <li>Q. I will let you know. One of these questions is this: given the computer calculation has shown some what COWI describe as irregular result or unrealistic result, and it happens that those so-called unrealistic result seems to suggest that there were overstress in the structure now, COWI dismissed those as reliable results. Our question to COWI is that if the same computer calculation showed part of the result which are unrealistic, how can we be assured that results for other locations are reliable? Would it suggest that the modelling itself has some problem?</li> <li>A. Well, they've only modelled they've modelled three discrete areas of the station, so in that, in those three discrete areas, there are only going to be specific parts of that model that are going to give realistic answers.</li> <li>You've seen it says that there was one failure which was a shear failure in an end panel in their model. Because it's an end panel, it's at the boundary, so the results in that would be completely unreliable.</li> <li>Q. Why is that?</li> <li>A. Because there's a complete discontinuity in their model. They've modelled this structure and then right at the</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	<ul> <li>to answer.</li> <li>A. Indeed.</li> <li>COMMISSIONER HANSFORD: But they have actually given their conclusions, I see, on page 39 of their report, and indeed they address shear in items 2, 3 and 4. But that doesn't invalidate Mr Chow's questions that they need to address.</li> <li>A. Yes.</li> <li>COMMISSIONER HANSFORD: Would you agree with that?</li> <li>A. Yes, sure.</li> <li>MR CHOW: Thank you, Prof Hansford. <ul> <li>I would like to move on to another slide, page 16, please, where you talk about the test result.</li> <li>I recall what you said is at one point you said there is only one sample tested; you would welcome that if more samples should be tested, then the result may be more reliable. Do you recall that?</li> </ul> </li> <li>A. I can't recall exactly what I said. I don't think I said that.</li> <li>MR PENNICOTT: I didn't hear that either.</li> <li>A. I just said, "These are the tests."</li> <li>CHAIRMAN: Sorry, where</li> <li>MR CHOW: You said something like, "Tm pleased to see</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>Q. I will let you know. One of these questions is this: given the computer calculation has shown some what COWI describe as irregular result or unrealistic result, and it happens that those so-called unrealistic result seems to suggest that there were overstress in the structure now, COWI dismissed those as reliable results. Our question to COWI is that if the same computer calculation showed part of the result which are unrealistic, how can we be assured that results for other locations are reliable? Would it suggest that the modelling itself has some problem?</li> <li>A. Well, they've only modelled they've modelled three discrete areas of the station, so in that, in those three discrete areas, there are only going to be specific parts of that model that are going to give realistic answers.</li> <li>You've seen it says that there was one failure which was a shear failure in an end panel in their model. Because it's an end panel, it's at the boundary, so the results in that would be completely unreliable.</li> <li>Q. Why is that?</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>to answer.</li> <li>A. Indeed.</li> <li>COMMISSIONER HANSFORD: But they have actually given their conclusions, I see, on page 39 of their report, and indeed they address shear in items 2, 3 and 4. But that doesn't invalidate Mr Chow's questions that they need to address.</li> <li>A. Yes.</li> <li>COMMISSIONER HANSFORD: Would you agree with that?</li> <li>A. Yes, sure.</li> <li>MR CHOW: Thank you, Prof Hansford. <ul> <li>I would like to move on to another slide, page 16, please, where you talk about the test result.</li> <li>I recall what you said is at one point you said there is only one sample tested; you would welcome that if more samples should be tested, then the result may be more reliable. Do you recall that?</li> </ul> </li> <li>A. I can't recall exactly what I said. I don't think I said that.</li> <li>MR PENNICOTT: I didn't hear that either.</li> <li>A. I just said, "These are the tests."</li> <li>CHAIRMAN: Sorry, where</li> </ul>

Γ

		Page 149		Page 151
	1	I've missed it.	1	that we need in the design. So that indicates to me
	2	COMMISSIONER HANSFORD: I didn't hear that.	2	that that coupler assembly is adequate.
	3	A. I can't recall.	3	Q. All right. Okay.
	4	MR PENNICOTT: I didn't hear it either.	4	Now, this morning, when I asked Prof Yeung questions
	5	MR CHOW: That's fine. Perhaps I have	5	on the test requirements set out in the American code,
	6	MR SHIEH: He might have said something like more tests can	6	AC133, and also 2004 Concrete Code in Hong Kong, in
	7	be done but it was not specifically as to whether or not	7	particular the elongation test do you recall that?
	8	they should be done. He was simply observing, "maybe	8	A. Yes.
	9	you can always do more tests", something like that. I'm	9	Q. So you know that that is a requirement under our
1	10	checking the transcript.	10	Hong Kong Concrete Code 2004, for elongation test, and
1	11	MR CHOW: Sorry, my apologies. Something like that.	11	it's about the maximum allowable residual elongation of
1	12	Can I ask you, then. The fact is only one sample	12	not more than 0.1 millimetre after the coupling assembly
1	13	was tested for each percentage of engaged length; right?	13	is subject to a load up to 60 per cent of the yield
1	14	A. Yes.	14	strength; you are aware of that?
1	15	Q. Do you think it would be better and make the result much	15	A. Yes.
1	16	more reliable if more samples of the same percentage of	16	Q. In the American code, AC133, there are other tests,
1	17	engaged length are being tested?	17	static compressive test, static tensile test, cyclic
1	18	A. Well, I mean, of course, the more you test, the more	18	load test. You are also aware of those tests as well?
1	19	confidence you get. Although I said I wasn't an expert	19	A. (Nodded head).
2	20	in statistics, I think that's what statistics is about.	20	Q. Do you know the reason why those tests were required?
2	21	But, you know, if you want to do more tests, you could.	21	A. I believe all these tests go towards making
2	22	That's not a problem. That doesn't change the results	22	a specification that is watertight so that that product
2	23	of what we see.	23	can be used in any application in the civil engineering
2	24	Q. Okay. I appreciate that you are not an expert in	24	industry. So you can use that coupler anywhere, I mean
~				
14	25	statistics. Can I also ask whether you are an expert in	25	in any application.
	25	statistics. Can I also ask whether you are an expert in Page 150	25	in any application. Page 152
		Page 150		Page 152
	1	Page 150 the behaviour of couplers?	1	Page 152 So I'm not saying that those tests are not relevant
	1 2	Page 150 the behaviour of couplers? A. I have used couplers in my structural design, so from	1 2	Page 152 So I'm not saying that those tests are not relevant for a coupler that you want to take off the shelf and
	1	Page 150 the behaviour of couplers? A. I have used couplers in my structural design, so from the point of view of the structural design, the	1	Page 152 So I'm not saying that those tests are not relevant for a coupler that you want to take off the shelf and use anywhere.
	1 2 3 4	Page 150 the behaviour of couplers? A. I have used couplers in my structural design, so from the point of view of the structural design, the application of the use of couplers in infrastructure	1 2 3	Page 152 So I'm not saying that those tests are not relevant for a coupler that you want to take off the shelf and use anywhere. Q. So is that what you guess or you know as a matter of
	1 2 3 4 5	Page 150 the behaviour of couplers? A. I have used couplers in my structural design, so from the point of view of the structural design, the application of the use of couplers in infrastructure works, yes, of course. I'm not an expert in the	1 2 3 4 5	Page 152 So I'm not saying that those tests are not relevant for a coupler that you want to take off the shelf and use anywhere. Q. So is that what you guess or you know as a matter of fact those are the reasons behind those requirements?
	1 2 3 4 5 6	Page 150 the behaviour of couplers? A. I have used couplers in my structural design, so from the point of view of the structural design, the application of the use of couplers in infrastructure works, yes, of course. I'm not an expert in the metallurgy inside couplers, no.	1 2 3 4	Page 152 So I'm not saying that those tests are not relevant for a coupler that you want to take off the shelf and use anywhere. Q. So is that what you guess or you know as a matter of fact those are the reasons behind those requirements? A. I wasn't involved in drafting the AC133, I wasn't
	1 2 3 4 5 6 7	Page 150 the behaviour of couplers? A. I have used couplers in my structural design, so from the point of view of the structural design, the application of the use of couplers in infrastructure works, yes, of course. I'm not an expert in the metallurgy inside couplers, no. Q. When you say you use couplers in your design, am I right	1 2 3 4 5 6 7	Page 152 So I'm not saying that those tests are not relevant for a coupler that you want to take off the shelf and use anywhere. Q. So is that what you guess or you know as a matter of fact those are the reasons behind those requirements? A. I wasn't involved in drafting the AC133, I wasn't involved in drafting the Hong Kong Code, so the reasons
	1 2 3 4 5 6 7 8	Page 150 the behaviour of couplers? A. I have used couplers in my structural design, so from the point of view of the structural design, the application of the use of couplers in infrastructure works, yes, of course. I'm not an expert in the metallurgy inside couplers, no. Q. When you say you use couplers in your design, am I right in understanding that by doing so, you relied on the	1 2 3 4 5 6 7 8	Page 152 So I'm not saying that those tests are not relevant for a coupler that you want to take off the shelf and use anywhere. Q. So is that what you guess or you know as a matter of fact those are the reasons behind those requirements? A. I wasn't involved in drafting the AC133, I wasn't involved in drafting the Hong Kong Code, so the reasons for these tests I mean, they're all to do with
	1 2 3 4 5 6 7 8 9	Page 150 the behaviour of couplers? A. I have used couplers in my structural design, so from the point of view of the structural design, the application of the use of couplers in infrastructure works, yes, of course. I'm not an expert in the metallurgy inside couplers, no. Q. When you say you use couplers in your design, am I right in understanding that by doing so, you relied on the catalogue or the strength data published by a particular	1 2 3 4 5 6 7 8 9	Page 152 So I'm not saying that those tests are not relevant for a coupler that you want to take off the shelf and use anywhere. Q. So is that what you guess or you know as a matter of fact those are the reasons behind those requirements? A. I wasn't involved in drafting the AC133, I wasn't involved in drafting the Hong Kong Code, so the reasons for these tests I mean, they're all to do with ensuring and guaranteeing the performance of the
1	1 2 3 4 5 6 7 8 9	Page 150 the behaviour of couplers? A. I have used couplers in my structural design, so from the point of view of the structural design, the application of the use of couplers in infrastructure works, yes, of course. I'm not an expert in the metallurgy inside couplers, no. Q. When you say you use couplers in your design, am I right in understanding that by doing so, you relied on the catalogue or the strength data published by a particular coupler manufacturer, and you made use of those data in	1 2 3 4 5 6 7 8 9 10	Page 152 So I'm not saying that those tests are not relevant for a coupler that you want to take off the shelf and use anywhere. Q. So is that what you guess or you know as a matter of fact those are the reasons behind those requirements? A. I wasn't involved in drafting the AC133, I wasn't involved in drafting the Hong Kong Code, so the reasons for these tests I mean, they're all to do with ensuring and guaranteeing the performance of the coupler
1	1 2 3 4 5 6 7 8 9 10 11	<ul><li>Page 150</li><li>the behaviour of couplers?</li><li>A. I have used couplers in my structural design, so from the point of view of the structural design, the application of the use of couplers in infrastructure works, yes, of course. I'm not an expert in the metallurgy inside couplers, no.</li><li>Q. When you say you use couplers in your design, am I right in understanding that by doing so, you relied on the catalogue or the strength data published by a particular coupler manufacturer, and you made use of those data in your design, and then you specified certain type of</li></ul>	1 2 3 4 5 6 7 8 9	Page 152 So I'm not saying that those tests are not relevant for a coupler that you want to take off the shelf and use anywhere. Q. So is that what you guess or you know as a matter of fact those are the reasons behind those requirements? A. I wasn't involved in drafting the AC133, I wasn't involved in drafting the Hong Kong Code, so the reasons for these tests I mean, they're all to do with ensuring and guaranteeing the performance of the coupler Q. I see.
	1 2 3 4 5 6 7 8 9 10 11 12	<ul> <li>Page 150</li> <li>the behaviour of couplers?</li> <li>A. I have used couplers in my structural design, so from the point of view of the structural design, the application of the use of couplers in infrastructure works, yes, of course. I'm not an expert in the metallurgy inside couplers, no.</li> <li>Q. When you say you use couplers in your design, am I right in understanding that by doing so, you relied on the catalogue or the strength data published by a particular coupler manufacturer, and you made use of those data in your design, and then you specified certain type of couplers to be used in the design drawing? That is how</li> </ul>	1 2 3 4 5 6 7 8 9 10 11 12	Page 152 So I'm not saying that those tests are not relevant for a coupler that you want to take off the shelf and use anywhere. Q. So is that what you guess or you know as a matter of fact those are the reasons behind those requirements? A. I wasn't involved in drafting the AC133, I wasn't involved in drafting the Hong Kong Code, so the reasons for these tests I mean, they're all to do with ensuring and guaranteeing the performance of the coupler Q. I see. A for use anywhere.
	1 2 3 4 5 6 7 8 9 10 11	<ul> <li>Page 150</li> <li>the behaviour of couplers?</li> <li>A. I have used couplers in my structural design, so from the point of view of the structural design, the application of the use of couplers in infrastructure works, yes, of course. I'm not an expert in the metallurgy inside couplers, no.</li> <li>Q. When you say you use couplers in your design, am I right in understanding that by doing so, you relied on the catalogue or the strength data published by a particular coupler manufacturer, and you made use of those data in your design, and then you specified certain type of couplers to be used in the design drawing? That is how you so-called make use of couplers?</li> </ul>	1 2 3 4 5 6 7 8 9 10 11 12 13	Page 152 So I'm not saying that those tests are not relevant for a coupler that you want to take off the shelf and use anywhere. Q. So is that what you guess or you know as a matter of fact those are the reasons behind those requirements? A. I wasn't involved in drafting the AC133, I wasn't involved in drafting the Hong Kong Code, so the reasons for these tests I mean, they're all to do with ensuring and guaranteeing the performance of the coupler Q. I see. A for use anywhere. Q. Okay. So you would not suggest to this Commission that
	1 2 3 4 5 6 7 8 9 10 11 12 13	<ul> <li>Page 150</li> <li>the behaviour of couplers?</li> <li>A. I have used couplers in my structural design, so from the point of view of the structural design, the application of the use of couplers in infrastructure works, yes, of course. I'm not an expert in the metallurgy inside couplers, no.</li> <li>Q. When you say you use couplers in your design, am I right in understanding that by doing so, you relied on the catalogue or the strength data published by a particular coupler manufacturer, and you made use of those data in your design, and then you specified certain type of couplers to be used in the design drawing? That is how you so-called make use of couplers?</li> <li>A. Yes, that's how industry works.</li> </ul>	1 2 3 4 5 6 7 8 9 10 11 12	Page 152 So I'm not saying that those tests are not relevant for a coupler that you want to take off the shelf and use anywhere. Q. So is that what you guess or you know as a matter of fact those are the reasons behind those requirements? A. I wasn't involved in drafting the AC133, I wasn't involved in drafting the Hong Kong Code, so the reasons for these tests I mean, they're all to do with ensuring and guaranteeing the performance of the coupler Q. I see. A for use anywhere. Q. Okay. So you would not suggest to this Commission that the elongation test is wholly unnecessary?
	1 2 3 4 5 6 7 8 9 10 11 12 13 14	<ul> <li>Page 150</li> <li>the behaviour of couplers?</li> <li>A. I have used couplers in my structural design, so from the point of view of the structural design, the application of the use of couplers in infrastructure works, yes, of course. I'm not an expert in the metallurgy inside couplers, no.</li> <li>Q. When you say you use couplers in your design, am I right in understanding that by doing so, you relied on the catalogue or the strength data published by a particular coupler manufacturer, and you made use of those data in your design, and then you specified certain type of couplers to be used in the design drawing? That is how you so-called make use of couplers?</li> <li>A. Yes, that's how industry works.</li> <li>Q. So if the contractor fails to comply with, for example,</li> </ul>	1 2 3 4 5 6 7 8 9 10 11 12 13 14	Page 152 So I'm not saying that those tests are not relevant for a coupler that you want to take off the shelf and use anywhere. Q. So is that what you guess or you know as a matter of fact those are the reasons behind those requirements? A. I wasn't involved in drafting the AC133, I wasn't involved in drafting the Hong Kong Code, so the reasons for these tests I mean, they're all to do with ensuring and guaranteeing the performance of the coupler Q. I see. A for use anywhere. Q. Okay. So you would not suggest to this Commission that the elongation test is wholly unnecessary? A. If I wanted to use the coupler, say, at the base of the
	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	<ul> <li>Page 150</li> <li>the behaviour of couplers?</li> <li>A. I have used couplers in my structural design, so from the point of view of the structural design, the application of the use of couplers in infrastructure works, yes, of course. I'm not an expert in the metallurgy inside couplers, no.</li> <li>Q. When you say you use couplers in your design, am I right in understanding that by doing so, you relied on the catalogue or the strength data published by a particular coupler manufacturer, and you made use of those data in your design, and then you specified certain type of couplers to be used in the design drawing? That is how you so-called make use of couplers?</li> <li>A. Yes, that's how industry works.</li> <li>Q. So if the contractor fails to comply with, for example, the way a particular brand of coupler should be</li> </ul>	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	<ul> <li>Page 152</li> <li>So I'm not saying that those tests are not relevant for a coupler that you want to take off the shelf and use anywhere.</li> <li>Q. So is that what you guess or you know as a matter of fact those are the reasons behind those requirements?</li> <li>A. I wasn't involved in drafting the AC133, I wasn't involved in drafting the Hong Kong Code, so the reasons for these tests I mean, they're all to do with ensuring and guaranteeing the performance of the coupler</li> <li>Q. I see.</li> <li>A for use anywhere.</li> <li>Q. Okay. So you would not suggest to this Commission that the elongation test is wholly unnecessary?</li> <li>A. If I wanted to use the coupler, say, at the base of the Nina Tower, that coupler would be subjected to very,</li> </ul>
	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	<ul> <li>Page 150</li> <li>the behaviour of couplers?</li> <li>A. I have used couplers in my structural design, so from the point of view of the structural design, the application of the use of couplers in infrastructure works, yes, of course. I'm not an expert in the metallurgy inside couplers, no.</li> <li>Q. When you say you use couplers in your design, am I right in understanding that by doing so, you relied on the catalogue or the strength data published by a particular coupler manufacturer, and you made use of those data in your design, and then you specified certain type of couplers to be used in the design drawing? That is how you so-called make use of couplers?</li> <li>A. Yes, that's how industry works.</li> <li>Q. So if the contractor fails to comply with, for example, the way a particular brand of coupler should be installed, then you are not you don't claim any</li> </ul>	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	Page 152 So I'm not saying that those tests are not relevant for a coupler that you want to take off the shelf and use anywhere. Q. So is that what you guess or you know as a matter of fact those are the reasons behind those requirements? A. I wasn't involved in drafting the AC133, I wasn't involved in drafting the Hong Kong Code, so the reasons for these tests I mean, they're all to do with ensuring and guaranteeing the performance of the coupler Q. I see. A for use anywhere. Q. Okay. So you would not suggest to this Commission that the elongation test is wholly unnecessary? A. If I wanted to use the coupler, say, at the base of the Nina Tower, that coupler would be subjected to very, very high tension and compression stresses because of
	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	<ul> <li>Page 150</li> <li>the behaviour of couplers?</li> <li>A. I have used couplers in my structural design, so from the point of view of the structural design, the application of the use of couplers in infrastructure works, yes, of course. I'm not an expert in the metallurgy inside couplers, no.</li> <li>Q. When you say you use couplers in your design, am I right in understanding that by doing so, you relied on the catalogue or the strength data published by a particular coupler manufacturer, and you made use of those data in your design, and then you specified certain type of couplers to be used in the design drawing? That is how you so-called make use of couplers?</li> <li>A. Yes, that's how industry works.</li> <li>Q. So if the contractor fails to comply with, for example, the way a particular brand of coupler should be installed, then you are not you don't claim any expertise in trying to extrapolate and to form any</li> </ul>	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	<ul> <li>Page 152</li> <li>So I'm not saying that those tests are not relevant for a coupler that you want to take off the shelf and use anywhere.</li> <li>Q. So is that what you guess or you know as a matter of fact those are the reasons behind those requirements?</li> <li>A. I wasn't involved in drafting the AC133, I wasn't involved in drafting the Hong Kong Code, so the reasons for these tests I mean, they're all to do with ensuring and guaranteeing the performance of the coupler</li> <li>Q. I see.</li> <li>A for use anywhere.</li> <li>Q. Okay. So you would not suggest to this Commission that the elongation test is wholly unnecessary?</li> <li>A. If I wanted to use the coupler, say, at the base of the Nina Tower, that coupler would be subjected to very, very high tension and compression stresses because of wind loading, earthquake loading, you know. So if</li> </ul>
	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	<ul> <li>Page 150</li> <li>the behaviour of couplers?</li> <li>A. I have used couplers in my structural design, so from the point of view of the structural design, the application of the use of couplers in infrastructure works, yes, of course. I'm not an expert in the metallurgy inside couplers, no.</li> <li>Q. When you say you use couplers in your design, am I right in understanding that by doing so, you relied on the catalogue or the strength data published by a particular coupler manufacturer, and you made use of those data in your design, and then you specified certain type of couplers to be used in the design drawing? That is how you so-called make use of couplers?</li> <li>A. Yes, that's how industry works.</li> <li>Q. So if the contractor fails to comply with, for example, the way a particular brand of coupler should be installed, then you are not you don't claim any expertise in trying to extrapolate and to form any opinion as to how, under those circumstances, the</li> </ul>	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	<ul> <li>Page 152</li> <li>So I'm not saying that those tests are not relevant for a coupler that you want to take off the shelf and use anywhere.</li> <li>Q. So is that what you guess or you know as a matter of fact those are the reasons behind those requirements?</li> <li>A. I wasn't involved in drafting the AC133, I wasn't involved in drafting the Hong Kong Code, so the reasons for these tests I mean, they're all to do with ensuring and guaranteeing the performance of the coupler</li> <li>Q. I see.</li> <li>A for use anywhere.</li> <li>Q. Okay. So you would not suggest to this Commission that the elongation test is wholly unnecessary?</li> <li>A. If I wanted to use the coupler, say, at the base of the Nina Tower, that coupler would be subjected to very, very high tension and compression stresses because of wind loading, earthquake loading, you know. So if I wanted to use a coupler there, I want to make sure</li> </ul>
	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	<ul> <li>Page 150</li> <li>the behaviour of couplers?</li> <li>A. I have used couplers in my structural design, so from the point of view of the structural design, the application of the use of couplers in infrastructure works, yes, of course. I'm not an expert in the metallurgy inside couplers, no.</li> <li>Q. When you say you use couplers in your design, am I right in understanding that by doing so, you relied on the catalogue or the strength data published by a particular coupler manufacturer, and you made use of those data in your design, and then you specified certain type of couplers to be used in the design drawing? That is how you so-called make use of couplers?</li> <li>A. Yes, that's how industry works.</li> <li>Q. So if the contractor fails to comply with, for example, the way a particular brand of coupler should be installed, then you are not you don't claim any expertise in trying to extrapolate and to form any opinion as to how, under those circumstances, the couplers would behave?</li> </ul>	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	<ul> <li>Page 152</li> <li>So I'm not saying that those tests are not relevant for a coupler that you want to take off the shelf and use anywhere.</li> <li>Q. So is that what you guess or you know as a matter of fact those are the reasons behind those requirements?</li> <li>A. I wasn't involved in drafting the AC133, I wasn't involved in drafting the Hong Kong Code, so the reasons for these tests I mean, they're all to do with ensuring and guaranteeing the performance of the coupler</li> <li>Q. I see.</li> <li>A for use anywhere.</li> <li>Q. Okay. So you would not suggest to this Commission that the elongation test is wholly unnecessary?</li> <li>A. If I wanted to use the coupler, say, at the base of the Nina Tower, that coupler would be subjected to very, very high tension and compression stresses because of wind loading, earthquake loading, you know. So if I wanted to use a coupler there, I want to make sure that coupler can meet all of the criteria, all of the</li> </ul>
	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	<ul> <li>Page 150</li> <li>the behaviour of couplers?</li> <li>A. I have used couplers in my structural design, so from the point of view of the structural design, the application of the use of couplers in infrastructure works, yes, of course. I'm not an expert in the metallurgy inside couplers, no.</li> <li>Q. When you say you use couplers in your design, am I right in understanding that by doing so, you relied on the catalogue or the strength data published by a particular coupler manufacturer, and you made use of those data in your design, and then you specified certain type of couplers to be used in the design drawing? That is how you so-called make use of couplers?</li> <li>A. Yes, that's how industry works.</li> <li>Q. So if the contractor fails to comply with, for example, the way a particular brand of coupler should be installed, then you are not you don't claim any expertise in trying to extrapolate and to form any opinion as to how, under those circumstances, the</li> </ul>	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	<ul> <li>Page 152</li> <li>So I'm not saying that those tests are not relevant for a coupler that you want to take off the shelf and use anywhere.</li> <li>Q. So is that what you guess or you know as a matter of fact those are the reasons behind those requirements?</li> <li>A. I wasn't involved in drafting the AC133, I wasn't involved in drafting the Hong Kong Code, so the reasons for these tests I mean, they're all to do with ensuring and guaranteeing the performance of the coupler</li> <li>Q. I see.</li> <li>A for use anywhere.</li> <li>Q. Okay. So you would not suggest to this Commission that the elongation test is wholly unnecessary?</li> <li>A. If I wanted to use the coupler, say, at the base of the Nina Tower, that coupler would be subjected to very, very high tension and compression stresses because of wind loading, earthquake loading, you know. So if I wanted to use a coupler there, I want to make sure that coupler can meet all of the criteria, all of the loading, that is put to it.</li> </ul>
	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	<ul> <li>Page 150</li> <li>the behaviour of couplers?</li> <li>A. I have used couplers in my structural design, so from the point of view of the structural design, the application of the use of couplers in infrastructure works, yes, of course. I'm not an expert in the metallurgy inside couplers, no.</li> <li>Q. When you say you use couplers in your design, am I right in understanding that by doing so, you relied on the catalogue or the strength data published by a particular coupler manufacturer, and you made use of those data in your design, and then you specified certain type of couplers to be used in the design drawing? That is how you so-called make use of couplers?</li> <li>A. Yes, that's how industry works.</li> <li>Q. So if the contractor fails to comply with, for example, the way a particular brand of coupler should be installed, then you are not you don't claim any expertise in trying to extrapolate and to form any opinion as to how, under those circumstances, the couplers would behave?</li> <li>A. No. I think that's kind of straying into the whole</li> </ul>	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	<ul> <li>Page 152</li> <li>So I'm not saying that those tests are not relevant for a coupler that you want to take off the shelf and use anywhere.</li> <li>Q. So is that what you guess or you know as a matter of fact those are the reasons behind those requirements?</li> <li>A. I wasn't involved in drafting the AC133, I wasn't involved in drafting the Hong Kong Code, so the reasons for these tests I mean, they're all to do with ensuring and guaranteeing the performance of the coupler</li> <li>Q. I see.</li> <li>A for use anywhere.</li> <li>Q. Okay. So you would not suggest to this Commission that the elongation test is wholly unnecessary?</li> <li>A. If I wanted to use the coupler, say, at the base of the Nina Tower, that coupler would be subjected to very, very high tension and compression stresses because of wind loading, earthquake loading, you know. So if I wanted to use a coupler there, I want to make sure that coupler can meet all of the criteria, all of the</li> </ul>
	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>Page 150</li> <li>the behaviour of couplers?</li> <li>A. I have used couplers in my structural design, so from the point of view of the structural design, the application of the use of couplers in infrastructure works, yes, of course. I'm not an expert in the metallurgy inside couplers, no.</li> <li>Q. When you say you use couplers in your design, am I right in understanding that by doing so, you relied on the catalogue or the strength data published by a particular coupler manufacturer, and you made use of those data in your design, and then you specified certain type of couplers to be used in the design drawing? That is how you so-called make use of couplers?</li> <li>A. Yes, that's how industry works.</li> <li>Q. So if the contractor fails to comply with, for example, the way a particular brand of coupler should be installed, then you are not you don't claim any expertise in trying to extrapolate and to form any opinion as to how, under those circumstances, the couplers would behave?</li> <li>A. No. I think that's kind of straying into the whole specification side and the project administration side.</li> </ul>	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>Page 152</li> <li>So I'm not saying that those tests are not relevant for a coupler that you want to take off the shelf and use anywhere.</li> <li>Q. So is that what you guess or you know as a matter of fact those are the reasons behind those requirements?</li> <li>A. I wasn't involved in drafting the AC133, I wasn't involved in drafting the Hong Kong Code, so the reasons for these tests I mean, they're all to do with ensuring and guaranteeing the performance of the coupler</li> <li>Q. I see.</li> <li>A for use anywhere.</li> <li>Q. Okay. So you would not suggest to this Commission that the elongation test is wholly unnecessary?</li> <li>A. If I wanted to use the coupler, say, at the base of the Nina Tower, that coupler would be subjected to very, very high tension and compression stresses because of wind loading, earthquake loading, you know. So if I wanted to use a coupler there, I want to make sure that coupler can meet all of the criteria, all of the loading, that is put to it. So yes, those tests in that case, certainly I'm sure</li> </ul>

1	Page 153		Page 155
1	Now, the designer, Atkins, specifies the use of those	1	analysis is a good tool because if modelled correctly
2	couplers. There is a requirement for elongation test in	2	and if you can understand the input and the output, you
3	the Concrete Code. Are you suggesting that for the	3	can look at the flow of the stresses through the joint,
4	purpose of our structure that the Commission is	4	and that flow of stress, the lines of principal stress,
5	considering, it is wholly unnecessary to carry out those	5	are very useful in determining how that joint behaves.
6	elongation tests?	6	But I didn't have that time so
7	A. Well, I'm saying you've got to look at it from the	7	Q. I appreciate that.
8	perspective of where are we now. We are in a situation	8	A. And I wasn't
9	that the structure is in the ground, it's been built,	9	COMMISSIONER HANSFORD: Can I just ask, in your experience,
10	it's standing up, it's holding its load. The load has	10	does the how does the output from a finite element
11	been taken up by all of the couplers. The structure is	11	analysis correlate to the output from a simple
12	there. It's working. There's no sign of distress.	12	strut-and-tie analysis?
13	What is the future loading going to be on the coupler?	13	A. Okay. So if you took a bridge pier, you know, a bridge
14	The future loading sorry, the future change in	14	column that had two bridge bearings on top and then the
15	loading, that change in loading is actually going to be	15	load of the bridge above, so you've got two point loads
16	very small because it's only the live load of the trains	16	on the top of this column, and you did a 2D plate
17	on the platform slab, which is almost on top of the	17	analysis, finite element analysis, of that column, you
18	diaphragm wall, so the incremental stress change is very	18	would see the lines of principal compressive test and
19	small, which is a completely different situation to	19	principal tensile stress. You know the graphics that
20	a coupler at the base of the Nina Tower which is going	20	were in COWI's
21	to experience very large stress reversals.	21	COMMISSIONER HANSFORD: Yes.
22	Q. Can I move on to the next slide, please, where you set	22	A. If you've seen those. So you would get similar graphics
23	out various possible methods to determine the internal	23	showing the flow of compression and tension stresses,
24	stress inside the connection.	24	and you could use something like that to verify
25	A. Sorry, which slide?	25	a strut-and-tie analysis, because the point of
	Page 154		Page 156
1	Q. Slide 18, I think.	1	a strut-and-tie analysis is to show where the
1 2	Q. Slide 18, I think. Now, you list out possible methods or acceptable	1 2	a strut-and-tie analysis is to show where the compression struts are and where the tension ties are.
2	Now, you list out possible methods or acceptable	2	compression struts are and where the tension ties are.
2 3	Now, you list out possible methods or acceptable methods, and you also told us that the one you usually	2 3	compression struts are and where the tension ties are. So you do your strut-and-tie and then you could check it
2 3 4	Now, you list out possible methods or acceptable methods, and you also told us that the one you usually use is a finite element analysis using two-dimensional	2 3 4	compression struts are and where the tension ties are. So you do your strut-and-tie and then you could check it by doing a 2D finite element analysis.
2 3 4 5	Now, you list out possible methods or acceptable methods, and you also told us that the one you usually use is a finite element analysis using two-dimensional plate elements or three-dimensional solid brick	2 3 4 5	compression struts are and where the tension ties are. So you do your strut-and-tie and then you could check it by doing a 2D finite element analysis. COMMISSIONER HANSFORD: I understand that, but my question
2 3 4 5 6	Now, you list out possible methods or acceptable methods, and you also told us that the one you usually use is a finite element analysis using two-dimensional plate elements or three-dimensional solid brick elements.	2 3 4 5 6	<ul><li>compression struts are and where the tension ties are.</li><li>So you do your strut-and-tie and then you could check it</li><li>by doing a 2D finite element analysis.</li><li>COMMISSIONER HANSFORD: I understand that, but my question</li><li>is, in your experience, are the results usually similar?</li></ul>
2 3 4 5 6 7	Now, you list out possible methods or acceptable methods, and you also told us that the one you usually use is a finite element analysis using two-dimensional plate elements or three-dimensional solid brick elements. Am I right in thinking that for the joints that we	2 3 4 5 6 7	<ul><li>compression struts are and where the tension ties are.</li><li>So you do your strut-and-tie and then you could check it</li><li>by doing a 2D finite element analysis.</li><li>COMMISSIONER HANSFORD: I understand that, but my question is, in your experience, are the results usually similar?</li><li>A. Finite element analysis will give you a better result.</li></ul>
2 3 4 5 6 7 8	Now, you list out possible methods or acceptable methods, and you also told us that the one you usually use is a finite element analysis using two-dimensional plate elements or three-dimensional solid brick elements. Am I right in thinking that for the joints that we are interested in, you have not carried out any really	2 3 4 5 6 7 8	<ul> <li>compression struts are and where the tension ties are.</li> <li>So you do your strut-and-tie and then you could check it by doing a 2D finite element analysis.</li> <li>COMMISSIONER HANSFORD: I understand that, but my question is, in your experience, are the results usually similar?</li> <li>A. Finite element analysis will give you a better result.</li> <li>COMMISSIONER HANSFORD: What's the order of magnitude of</li> </ul>
2 3 4 5 6 7 8 9	Now, you list out possible methods or acceptable methods, and you also told us that the one you usually use is a finite element analysis using two-dimensional plate elements or three-dimensional solid brick elements. Am I right in thinking that for the joints that we are interested in, you have not carried out any really numerical checking to satisfy yourself that under the most critical load cases, the connection as-built is strong enough to take those loading?	2 3 4 5 6 7 8 9	<ul> <li>compression struts are and where the tension ties are.</li> <li>So you do your strut-and-tie and then you could check it</li> <li>by doing a 2D finite element analysis.</li> <li>COMMISSIONER HANSFORD: I understand that, but my question is, in your experience, are the results usually similar?</li> <li>A. Finite element analysis will give you a better result.</li> <li>COMMISSIONER HANSFORD: What's the order of magnitude of "better"?</li> <li>A. It depends. It depends vastly on the application and the situation. I could say 10 per cent, maybe 20, maybe</li> </ul>
2 3 4 5 6 7 8 9 10 11 12	Now, you list out possible methods or acceptable methods, and you also told us that the one you usually use is a finite element analysis using two-dimensional plate elements or three-dimensional solid brick elements. Am I right in thinking that for the joints that we are interested in, you have not carried out any really numerical checking to satisfy yourself that under the most critical load cases, the connection as-built is strong enough to take those loading? A. Before yesterday, no, I had not done any calculations.	2 3 4 5 6 7 8 9 10 11 12	<ul> <li>compression struts are and where the tension ties are.</li> <li>So you do your strut-and-tie and then you could check it</li> <li>by doing a 2D finite element analysis.</li> <li>COMMISSIONER HANSFORD: I understand that, but my question is, in your experience, are the results usually similar?</li> <li>A. Finite element analysis will give you a better result.</li> <li>COMMISSIONER HANSFORD: What's the order of magnitude of "better"?</li> <li>A. It depends. It depends vastly on the application and the situation. I could say 10 per cent, maybe 20, maybe 30; it really depends on the situation, because</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13	<ul> <li>Now, you list out possible methods or acceptable methods, and you also told us that the one you usually use is a finite element analysis using two-dimensional plate elements or three-dimensional solid brick elements.</li> <li>Am I right in thinking that for the joints that we are interested in, you have not carried out any really numerical checking to satisfy yourself that under the most critical load cases, the connection as-built is strong enough to take those loading?</li> <li>A. Before yesterday, no, I had not done any calculations.</li> <li>Q. And how about today?</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13	<ul> <li>compression struts are and where the tension ties are.</li> <li>So you do your strut-and-tie and then you could check it</li> <li>by doing a 2D finite element analysis.</li> <li>COMMISSIONER HANSFORD: I understand that, but my question is, in your experience, are the results usually similar?</li> <li>A. Finite element analysis will give you a better result.</li> <li>COMMISSIONER HANSFORD: What's the order of magnitude of "better"?</li> <li>A. It depends. It depends vastly on the application and the situation. I could say 10 per cent, maybe 20, maybe 30; it really depends on the situation, because strut-and-tie analysis is just a 2D thing, whereas</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14	<ul> <li>Now, you list out possible methods or acceptable methods, and you also told us that the one you usually use is a finite element analysis using two-dimensional plate elements or three-dimensional solid brick elements.</li> <li>Am I right in thinking that for the joints that we are interested in, you have not carried out any really numerical checking to satisfy yourself that under the most critical load cases, the connection as-built is strong enough to take those loading?</li> <li>A. Before yesterday, no, I had not done any calculations.</li> <li>Q. And how about today?</li> <li>A. Yesterday, after hearing the conversations on Monday</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14	<ul> <li>compression struts are and where the tension ties are.</li> <li>So you do your strut-and-tie and then you could check it</li> <li>by doing a 2D finite element analysis.</li> <li>COMMISSIONER HANSFORD: I understand that, but my question is, in your experience, are the results usually similar?</li> <li>A. Finite element analysis will give you a better result.</li> <li>COMMISSIONER HANSFORD: What's the order of magnitude of "better"?</li> <li>A. It depends. It depends vastly on the application and the situation. I could say 10 per cent, maybe 20, maybe 30; it really depends on the situation, because strut-and-tie analysis is just a 2D thing, whereas finite element analysis can be completely</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15	<ul> <li>Now, you list out possible methods or acceptable methods, and you also told us that the one you usually use is a finite element analysis using two-dimensional plate elements or three-dimensional solid brick elements.</li> <li>Am I right in thinking that for the joints that we are interested in, you have not carried out any really numerical checking to satisfy yourself that under the most critical load cases, the connection as-built is strong enough to take those loading?</li> <li>A. Before yesterday, no, I had not done any calculations.</li> <li>Q. And how about today?</li> <li>A. Yesterday, after hearing the conversations on Monday about how simple the joint calculation was, I thought</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15	<ul> <li>compression struts are and where the tension ties are.</li> <li>So you do your strut-and-tie and then you could check it</li> <li>by doing a 2D finite element analysis.</li> <li>COMMISSIONER HANSFORD: I understand that, but my question is, in your experience, are the results usually similar?</li> <li>A. Finite element analysis will give you a better result.</li> <li>COMMISSIONER HANSFORD: What's the order of magnitude of "better"?</li> <li>A. It depends. It depends vastly on the application and the situation. I could say 10 per cent, maybe 20, maybe 30; it really depends on the situation, because strut-and-tie analysis is just a 2D thing, whereas finite element analysis can be completely three-dimensional. So you are modelling the effect of</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	<ul> <li>Now, you list out possible methods or acceptable methods, and you also told us that the one you usually use is a finite element analysis using two-dimensional plate elements or three-dimensional solid brick elements.</li> <li>Am I right in thinking that for the joints that we are interested in, you have not carried out any really numerical checking to satisfy yourself that under the most critical load cases, the connection as-built is strong enough to take those loading?</li> <li>A. Before yesterday, no, I had not done any calculations.</li> <li>Q. And how about today?</li> <li>A. Yesterday, after hearing the conversations on Monday about how simple the joint calculation was, I thought let me have a look at it, let me see if I can do</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	<ul> <li>compression struts are and where the tension ties are.</li> <li>So you do your strut-and-tie and then you could check it</li> <li>by doing a 2D finite element analysis.</li> <li>COMMISSIONER HANSFORD: I understand that, but my question is, in your experience, are the results usually similar?</li> <li>A. Finite element analysis will give you a better result.</li> <li>COMMISSIONER HANSFORD: What's the order of magnitude of "better"?</li> <li>A. It depends. It depends vastly on the application and the situation. I could say 10 per cent, maybe 20, maybe 30; it really depends on the situation, because strut-and-tie analysis is just a 2D thing, whereas finite element analysis can be completely three-dimensional. So you are modelling the effect of that force going everywhere.</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	<ul> <li>Now, you list out possible methods or acceptable methods, and you also told us that the one you usually use is a finite element analysis using two-dimensional plate elements or three-dimensional solid brick elements.</li> <li>Am I right in thinking that for the joints that we are interested in, you have not carried out any really numerical checking to satisfy yourself that under the most critical load cases, the connection as-built is strong enough to take those loading?</li> <li>A. Before yesterday, no, I had not done any calculations.</li> <li>Q. And how about today?</li> <li>A. Yesterday, after hearing the conversations on Monday about how simple the joint calculation was, I thought let me have a look at it, let me see if I can do a simple calculation. So I asked for the representative</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	<ul> <li>compression struts are and where the tension ties are.</li> <li>So you do your strut-and-tie and then you could check it</li> <li>by doing a 2D finite element analysis.</li> <li>COMMISSIONER HANSFORD: I understand that, but my question is, in your experience, are the results usually similar?</li> <li>A. Finite element analysis will give you a better result.</li> <li>COMMISSIONER HANSFORD: What's the order of magnitude of "better"?</li> <li>A. It depends. It depends vastly on the application and the situation. I could say 10 per cent, maybe 20, maybe 30; it really depends on the situation, because strut-and-tie analysis is just a 2D thing, whereas finite element analysis can be completely three-dimensional. So you are modelling the effect of that force going everywhere.</li> <li>COMMISSIONER HANSFORD: So, if you get sufficient confidence</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	<ul> <li>Now, you list out possible methods or acceptable methods, and you also told us that the one you usually use is a finite element analysis using two-dimensional plate elements or three-dimensional solid brick elements.</li> <li>Am I right in thinking that for the joints that we are interested in, you have not carried out any really numerical checking to satisfy yourself that under the most critical load cases, the connection as-built is strong enough to take those loading?</li> <li>A. Before yesterday, no, I had not done any calculations.</li> <li>Q. And how about today?</li> <li>A. Yesterday, after hearing the conversations on Monday about how simple the joint calculation was, I thought let me have a look at it, let me see if I can do a simple calculation. So I asked for the representative loads, and these were extracted from the calculations,</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	<ul> <li>compression struts are and where the tension ties are.</li> <li>So you do your strut-and-tie and then you could check it</li> <li>by doing a 2D finite element analysis.</li> <li>COMMISSIONER HANSFORD: I understand that, but my question is, in your experience, are the results usually similar?</li> <li>A. Finite element analysis will give you a better result.</li> <li>COMMISSIONER HANSFORD: What's the order of magnitude of "better"?</li> <li>A. It depends. It depends vastly on the application and the situation. I could say 10 per cent, maybe 20, maybe 30; it really depends on the situation, because strut-and-tie analysis is just a 2D thing, whereas finite element analysis can be completely three-dimensional. So you are modelling the effect of that force going everywhere.</li> <li>COMMISSIONER HANSFORD: So, if you get sufficient confidence from a strut-and-tie analysis, would it then be</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	<ul> <li>Now, you list out possible methods or acceptable methods, and you also told us that the one you usually use is a finite element analysis using two-dimensional plate elements or three-dimensional solid brick elements.</li> <li>Am I right in thinking that for the joints that we are interested in, you have not carried out any really numerical checking to satisfy yourself that under the most critical load cases, the connection as-built is strong enough to take those loading?</li> <li>A. Before yesterday, no, I had not done any calculations.</li> <li>Q. And how about today?</li> <li>A. Yesterday, after hearing the conversations on Monday about how simple the joint calculation was, I thought let me have a look at it, let me see if I can do a simple calculation. So I asked for the representative loads, and these were extracted from the calculations, and I did a very simple, very quick, extremely quick,</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	<ul> <li>compression struts are and where the tension ties are.</li> <li>So you do your strut-and-tie and then you could check it</li> <li>by doing a 2D finite element analysis.</li> <li>COMMISSIONER HANSFORD: I understand that, but my question is, in your experience, are the results usually similar?</li> <li>A. Finite element analysis will give you a better result.</li> <li>COMMISSIONER HANSFORD: What's the order of magnitude of "better"?</li> <li>A. It depends. It depends vastly on the application and the situation. I could say 10 per cent, maybe 20, maybe 30; it really depends on the situation, because strut-and-tie analysis is just a 2D thing, whereas finite element analysis can be completely three-dimensional. So you are modelling the effect of that force going everywhere.</li> <li>COMMISSIONER HANSFORD: So, if you get sufficient confidence from a strut-and-tie analysis, would it then be unnecessary to do a finite element analysis?</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	<ul> <li>Now, you list out possible methods or acceptable methods, and you also told us that the one you usually use is a finite element analysis using two-dimensional plate elements or three-dimensional solid brick elements.</li> <li>Am I right in thinking that for the joints that we are interested in, you have not carried out any really numerical checking to satisfy yourself that under the most critical load cases, the connection as-built is strong enough to take those loading?</li> <li>A. Before yesterday, no, I had not done any calculations.</li> <li>Q. And how about today?</li> <li>A. Yesterday, after hearing the conversations on Monday about how simple the joint calculation was, I thought let me have a look at it, let me see if I can do a simple calculation. So I asked for the representative loads, and these were extracted from the calculations, and I did a very simple, very quick, extremely quick, strut-and-tie analysis to see if the joint could work.</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	<ul> <li>compression struts are and where the tension ties are.</li> <li>So you do your strut-and-tie and then you could check it</li> <li>by doing a 2D finite element analysis.</li> <li>COMMISSIONER HANSFORD: I understand that, but my question is, in your experience, are the results usually similar?</li> <li>A. Finite element analysis will give you a better result.</li> <li>COMMISSIONER HANSFORD: What's the order of magnitude of "better"?</li> <li>A. It depends. It depends vastly on the application and the situation. I could say 10 per cent, maybe 20, maybe 30; it really depends on the situation, because strut-and-tie analysis is just a 2D thing, whereas finite element analysis can be completely three-dimensional. So you are modelling the effect of that force going everywhere.</li> <li>COMMISSIONER HANSFORD: So, if you get sufficient confidence from a strut-and-tie analysis, would it then be unnecessary to do a finite element analysis?</li> <li>A. I think a strut-and-tie analysis is more conservative.</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	<ul> <li>Now, you list out possible methods or acceptable methods, and you also told us that the one you usually use is a finite element analysis using two-dimensional plate elements or three-dimensional solid brick elements.</li> <li>Am I right in thinking that for the joints that we are interested in, you have not carried out any really numerical checking to satisfy yourself that under the most critical load cases, the connection as-built is strong enough to take those loading?</li> <li>A. Before yesterday, no, I had not done any calculations.</li> <li>Q. And how about today?</li> <li>A. Yesterday, after hearing the conversations on Monday about how simple the joint calculation was, I thought let me have a look at it, let me see if I can do a simple calculation. So I asked for the representative loads, and these were extracted from the calculations, and I did a very simple, very quick, extremely quick, strut-and-tie analysis to see if the joint could work. So this was very, very quick. Clearly, I said my</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	<ul> <li>compression struts are and where the tension ties are.</li> <li>So you do your strut-and-tie and then you could check it</li> <li>by doing a 2D finite element analysis.</li> <li>COMMISSIONER HANSFORD: I understand that, but my question is, in your experience, are the results usually similar?</li> <li>A. Finite element analysis will give you a better result.</li> <li>COMMISSIONER HANSFORD: What's the order of magnitude of "better"?</li> <li>A. It depends. It depends vastly on the application and the situation. I could say 10 per cent, maybe 20, maybe 30; it really depends on the situation, because strut-and-tie analysis is just a 2D thing, whereas finite element analysis can be completely three-dimensional. So you are modelling the effect of that force going everywhere.</li> <li>COMMISSIONER HANSFORD: So, if you get sufficient confidence from a strut-and-tie analysis, would it then be unnecessary to do a finite element analysis?</li> <li>A. I think a strut-and-tie analysis is more conservative. I mean, I've been in situations where we have produced</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>Now, you list out possible methods or acceptable methods, and you also told us that the one you usually use is a finite element analysis using two-dimensional plate elements or three-dimensional solid brick elements.</li> <li>Am I right in thinking that for the joints that we are interested in, you have not carried out any really numerical checking to satisfy yourself that under the most critical load cases, the connection as-built is strong enough to take those loading?</li> <li>A. Before yesterday, no, I had not done any calculations.</li> <li>Q. And how about today?</li> <li>A. Yesterday, after hearing the conversations on Monday about how simple the joint calculation was, I thought let me have a look at it, let me see if I can do a simple calculation. So I asked for the representative loads, and these were extracted from the calculations, and I did a very simple, very quick, extremely quick, strut-and-tie analysis to see if the joint could work. So this was very, very quick. Clearly, I said my preference, out of my preference in engineering</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>compression struts are and where the tension ties are.</li> <li>So you do your strut-and-tie and then you could check it</li> <li>by doing a 2D finite element analysis.</li> <li>COMMISSIONER HANSFORD: I understand that, but my question is, in your experience, are the results usually similar?</li> <li>A. Finite element analysis will give you a better result.</li> <li>COMMISSIONER HANSFORD: What's the order of magnitude of "better"?</li> <li>A. It depends. It depends vastly on the application and the situation. I could say 10 per cent, maybe 20, maybe 30; it really depends on the situation, because strut-and-tie analysis is just a 2D thing, whereas finite element analysis can be completely three-dimensional. So you are modelling the effect of that force going everywhere.</li> <li>COMMISSIONER HANSFORD: So, if you get sufficient confidence from a strut-and-tie analysis, would it then be unnecessary to do a finite element analysis?</li> <li>A. I think a strut-and-tie analysis is more conservative. I mean, I've been in situations where we have produced a design of bridge piers and we've done nice</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	<ul> <li>Now, you list out possible methods or acceptable methods, and you also told us that the one you usually use is a finite element analysis using two-dimensional plate elements or three-dimensional solid brick elements.</li> <li>Am I right in thinking that for the joints that we are interested in, you have not carried out any really numerical checking to satisfy yourself that under the most critical load cases, the connection as-built is strong enough to take those loading?</li> <li>A. Before yesterday, no, I had not done any calculations.</li> <li>Q. And how about today?</li> <li>A. Yesterday, after hearing the conversations on Monday about how simple the joint calculation was, I thought let me have a look at it, let me see if I can do a simple calculation. So I asked for the representative loads, and these were extracted from the calculations, and I did a very simple, very quick, extremely quick, strut-and-tie analysis to see if the joint could work. So this was very, very quick. Clearly, I said my preference, out of my preference in engineering design is to do a finite element analysis, using 2D or</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	<ul> <li>compression struts are and where the tension ties are.</li> <li>So you do your strut-and-tie and then you could check it</li> <li>by doing a 2D finite element analysis.</li> <li>COMMISSIONER HANSFORD: I understand that, but my question is, in your experience, are the results usually similar?</li> <li>A. Finite element analysis will give you a better result.</li> <li>COMMISSIONER HANSFORD: What's the order of magnitude of "better"?</li> <li>A. It depends. It depends vastly on the application and the situation. I could say 10 per cent, maybe 20, maybe 30; it really depends on the situation, because strut-and-tie analysis is just a 2D thing, whereas finite element analysis can be completely three-dimensional. So you are modelling the effect of that force going everywhere.</li> <li>COMMISSIONER HANSFORD: So, if you get sufficient confidence from a strut-and-tie analysis, would it then be unnecessary to do a finite element analysis?</li> <li>A. I think a strut-and-tie analysis is more conservative. I mean, I've been in situations where we have produced a design of bridge piers and we've done nice three-dimensional finite element analysis, and I've had</li> </ul>
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>Now, you list out possible methods or acceptable methods, and you also told us that the one you usually use is a finite element analysis using two-dimensional plate elements or three-dimensional solid brick elements.</li> <li>Am I right in thinking that for the joints that we are interested in, you have not carried out any really numerical checking to satisfy yourself that under the most critical load cases, the connection as-built is strong enough to take those loading?</li> <li>A. Before yesterday, no, I had not done any calculations.</li> <li>Q. And how about today?</li> <li>A. Yesterday, after hearing the conversations on Monday about how simple the joint calculation was, I thought let me have a look at it, let me see if I can do a simple calculation. So I asked for the representative loads, and these were extracted from the calculations, and I did a very simple, very quick, extremely quick, strut-and-tie analysis to see if the joint could work. So this was very, very quick. Clearly, I said my preference, out of my preference in engineering</li> </ul>	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>compression struts are and where the tension ties are.</li> <li>So you do your strut-and-tie and then you could check it</li> <li>by doing a 2D finite element analysis.</li> <li>COMMISSIONER HANSFORD: I understand that, but my question is, in your experience, are the results usually similar?</li> <li>A. Finite element analysis will give you a better result.</li> <li>COMMISSIONER HANSFORD: What's the order of magnitude of "better"?</li> <li>A. It depends. It depends vastly on the application and the situation. I could say 10 per cent, maybe 20, maybe 30; it really depends on the situation, because strut-and-tie analysis is just a 2D thing, whereas finite element analysis can be completely three-dimensional. So you are modelling the effect of that force going everywhere.</li> <li>COMMISSIONER HANSFORD: So, if you get sufficient confidence from a strut-and-tie analysis, would it then be unnecessary to do a finite element analysis?</li> <li>A. I think a strut-and-tie analysis is more conservative. I mean, I've been in situations where we have produced a design of bridge piers and we've done nice</li> </ul>

1	Page 157		Page 159
	strut-and-tie, to demonstrate that your computer	1	the structure. It will show you the first way that the
2	wizardry is correct." But that strut-and-tie analysis	2	structure wants to behave. And if that structure
3	does sometimes give you a more conservative answer	3	then because it's made of reinforced concrete, that
4	sorry, will give you a more conservative answer.	4	structure might then crack a bit, and it cracks, which
5	COMMISSIONER HANSFORD: So therefore, if a strut-and-tie	5	is perfectly okay reinforced concrete cracks, that's
6	analysis gives you confidence or proves, to your	6	okay the structure cracks and then the load will
7	satisfaction, that the structure is adequate, the finite	7	redistribute inside the section, and it will then go
8	element analysis would give you	8	into its second response, the second way it's taken up
9	A. It would improve the result.	9	its load.
10	COMMISSIONER HANSFORD: It would improve the result?	10	So when you do a strut-and-tie, if your
11	A. Yes.	11	strut-and-tie is the same as the first order of
12	COMMISSIONER HANSFORD: And in improving the result, it	12	response, then it's exactly it models exactly how the
13	would give you even further confidence?	13	structure will behave first. But if it's not, if it's
14	A. Correct.	14	a different strut-and-tie, the structure might have to
15	COMMISSIONER HANSFORD: Thank you.	15	crack a bit and the load redistribute, and then the load
16	CHAIRMAN: So, in other words, the two are on a plane	16	goes into the second response.
17	together? It's not as if you are going to have the	17	COMMISSIONER HANSFORD: Okay.
18	strut-and-tie saying, "No, this is going to fail", and	18	A. Do you follow?
19	you're going to have the other one saying, "Yes, it's	19	COMMISSIONER HANSFORD: I do follow, but in order
20	going to be fine"? It will be the question of the	20	A. So that's why there are many different ways of doing
21	strut-and-tie will give you a result, quite	21	strut-and-ties. So I'm not saying this is "the way".
22	conservative, and the other test, the computer test I'll	22	I'm just saying it is one way that was, as you said,
23	call it, will give you a more refined test, but	23	quick and dirty.
24	essentially on the same a rising plane?	24	COMMISSIONER HANSFORD: That's very helpful. In order no
25	A. That does depend on where you've started. If you've	25	to alarm anyone that might be listening to this
	Page 158		Page 160
1	started from a finite element analysis, and you have	1	conversation, those initial cracks are not cracks of
	designed it some officiently and some tight and some		,
2	designed it very efficiently and very tight and, you	2	concern?
2 3	know, you really have made it meet all the rules	2 3	
			concern?
3	know, you really have made it meet all the rules	3	concern? A. No, absolutely not. No, no, no, of course not.
3 4	know, you really have made it meet all the rules exactly, then if you use a strut-and-tie, you might find the tension force is a little bit larger than the tension stresses in the computer analysis.	3 4	concern? A. No, absolutely not. No, no, no, of course not. COMMISSIONER HANSFORD: Thank you. MR CHOW: Thank you, Prof Hansford. Mr Southward, just now you told us that yesterday
3 4 5	know, you really have made it meet all the rules exactly, then if you use a strut-and-tie, you might find the tension force is a little bit larger than the tension stresses in the computer analysis. CHAIRMAN: Put it this way, a better way than the rather	3 4 5	concern? A. No, absolutely not. No, no, no, of course not. COMMISSIONER HANSFORD: Thank you. MR CHOW: Thank you, Prof Hansford.
3 4 5 6	know, you really have made it meet all the rules exactly, then if you use a strut-and-tie, you might find the tension force is a little bit larger than the tension stresses in the computer analysis. CHAIRMAN: Put it this way, a better way than the rather clumsy way I put it earlier my apologies they	3 4 5 6	concern? A. No, absolutely not. No, no, no, of course not. COMMISSIONER HANSFORD: Thank you. MR CHOW: Thank you, Prof Hansford. Mr Southward, just now you told us that yesterday you have carried out your checking for the first time. Is it the 23rd slide or the 25th slide, is that
3 4 5 6 7	<ul><li>know, you really have made it meet all the rules</li><li>exactly, then if you use a strut-and-tie, you might find</li><li>the tension force is a little bit larger than the</li><li>tension stresses in the computer analysis.</li><li>CHAIRMAN: Put it this way, a better way than the rather</li><li>clumsy way I put it earlier my apologies they</li><li>complement each other, the tests?</li></ul>	3 4 5 6 7 8 9	concern? A. No, absolutely not. No, no, no, of course not. COMMISSIONER HANSFORD: Thank you. MR CHOW: Thank you, Prof Hansford. Mr Southward, just now you told us that yesterday you have carried out your checking for the first time.
3 4 5 6 7 8	know, you really have made it meet all the rules exactly, then if you use a strut-and-tie, you might find the tension force is a little bit larger than the tension stresses in the computer analysis. CHAIRMAN: Put it this way, a better way than the rather clumsy way I put it earlier my apologies they	3 4 5 6 7 8	concern? A. No, absolutely not. No, no, no, of course not. COMMISSIONER HANSFORD: Thank you. MR CHOW: Thank you, Prof Hansford. Mr Southward, just now you told us that yesterday you have carried out your checking for the first time. Is it the 23rd slide or the 25th slide, is that right, where you set out the result? A. Yes.
3 4 5 6 7 8 9 10 11	<ul><li>know, you really have made it meet all the rules</li><li>exactly, then if you use a strut-and-tie, you might find</li><li>the tension force is a little bit larger than the</li><li>tension stresses in the computer analysis.</li><li>CHAIRMAN: Put it this way, a better way than the rather</li><li>clumsy way I put it earlier my apologies they</li><li>complement each other, the tests?</li><li>A. Yes.</li><li>COMMISSIONER HANSFORD: In some areas, in some professions.</li></ul>	3 4 5 6 7 8 9 10 11	<ul> <li>concern?</li> <li>A. No, absolutely not. No, no, no, of course not.</li> <li>COMMISSIONER HANSFORD: Thank you.</li> <li>MR CHOW: Thank you, Prof Hansford.</li> <li>Mr Southward, just now you told us that yesterday you have carried out your checking for the first time. Is it the 23rd slide or the 25th slide, is that right, where you set out the result?</li> <li>A. Yes.</li> <li>Q. Now, I have a few questions on this.</li> </ul>
3 4 5 6 7 8 9 10 11 12	<ul> <li>know, you really have made it meet all the rules</li> <li>exactly, then if you use a strut-and-tie, you might find</li> <li>the tension force is a little bit larger than the</li> <li>tension stresses in the computer analysis.</li> <li>CHAIRMAN: Put it this way, a better way than the rather</li> <li>clumsy way I put it earlier my apologies they</li> <li>complement each other, the tests?</li> <li>A. Yes.</li> <li>COMMISSIONER HANSFORD: In some areas, in some professions.</li> <li>I might suggest, reference is made to a quick and dirty</li> </ul>	3 4 5 6 7 8 9 10 11 12	<ul> <li>concern?</li> <li>A. No, absolutely not. No, no, no, of course not.</li> <li>COMMISSIONER HANSFORD: Thank you.</li> <li>MR CHOW: Thank you, Prof Hansford.</li> <li>Mr Southward, just now you told us that yesterday you have carried out your checking for the first time. Is it the 23rd slide or the 25th slide, is that right, where you set out the result?</li> <li>A. Yes.</li> <li>Q. Now, I have a few questions on this. First of all, the bending moment that you use for</li> </ul>
3 4 5 6 7 8 9 10 11	<ul> <li>know, you really have made it meet all the rules</li> <li>exactly, then if you use a strut-and-tie, you might find</li> <li>the tension force is a little bit larger than the</li> <li>tension stresses in the computer analysis.</li> <li>CHAIRMAN: Put it this way, a better way than the rather</li> <li>clumsy way I put it earlier my apologies they</li> <li>complement each other, the tests?</li> <li>A. Yes.</li> <li>COMMISSIONER HANSFORD: In some areas, in some professions.</li> <li>I might suggest, reference is made to a quick and dirty</li> <li>analysis, if you can excuse that term.</li> </ul>	3 4 5 6 7 8 9 10 11 12 13	<ul> <li>concern?</li> <li>A. No, absolutely not. No, no, no, of course not.</li> <li>COMMISSIONER HANSFORD: Thank you.</li> <li>MR CHOW: Thank you, Prof Hansford.</li> <li>Mr Southward, just now you told us that yesterday you have carried out your checking for the first time. Is it the 23rd slide or the 25th slide, is that right, where you set out the result?</li> <li>A. Yes.</li> <li>Q. Now, I have a few questions on this. First of all, the bending moment that you use for your strut-and-tie analysis, if you look at the bending</li> </ul>
3 4 5 6 7 8 9 10 11 12	<ul> <li>know, you really have made it meet all the rules</li> <li>exactly, then if you use a strut-and-tie, you might find</li> <li>the tension force is a little bit larger than the</li> <li>tension stresses in the computer analysis.</li> <li>CHAIRMAN: Put it this way, a better way than the rather</li> <li>clumsy way I put it earlier my apologies they</li> <li>complement each other, the tests?</li> <li>A. Yes.</li> <li>COMMISSIONER HANSFORD: In some areas, in some professions,</li> <li>I might suggest, reference is made to a quick and dirty</li> <li>analysis, if you can excuse that term.</li> <li>A. That's fine.</li> </ul>	3 4 5 6 7 8 9 10 11 12 13 14	<ul> <li>concern?</li> <li>A. No, absolutely not. No, no, no, of course not.</li> <li>COMMISSIONER HANSFORD: Thank you.</li> <li>MR CHOW: Thank you, Prof Hansford.</li> <li>Mr Southward, just now you told us that yesterday you have carried out your checking for the first time. Is it the 23rd slide or the 25th slide, is that right, where you set out the result?</li> <li>A. Yes.</li> <li>Q. Now, I have a few questions on this.</li> <li>First of all, the bending moment that you use for your strut-and-tie analysis, if you look at the bending moment on the left side, left-hand side, it's</li> </ul>
3 4 5 6 7 8 9 10 11 12 13	<ul> <li>know, you really have made it meet all the rules</li> <li>exactly, then if you use a strut-and-tie, you might find</li> <li>the tension force is a little bit larger than the</li> <li>tension stresses in the computer analysis.</li> <li>CHAIRMAN: Put it this way, a better way than the rather</li> <li>clumsy way I put it earlier my apologies they</li> <li>complement each other, the tests?</li> <li>A. Yes.</li> <li>COMMISSIONER HANSFORD: In some areas, in some professions.</li> <li>I might suggest, reference is made to a quick and dirty</li> <li>analysis, if you can excuse that term.</li> <li>A. That's fine.</li> <li>COMMISSIONER HANSFORD: Therefore, would an overnight</li> </ul>	3 4 5 6 7 8 9 10 11 12 13 14 15	<ul> <li>concern?</li> <li>A. No, absolutely not. No, no, no, of course not.</li> <li>COMMISSIONER HANSFORD: Thank you.</li> <li>MR CHOW: Thank you, Prof Hansford.</li> <li>Mr Southward, just now you told us that yesterday you have carried out your checking for the first time. Is it the 23rd slide or the 25th slide, is that right, where you set out the result?</li> <li>A. Yes.</li> <li>Q. Now, I have a few questions on this.</li> <li>First of all, the bending moment that you use for your strut-and-tie analysis, if you look at the bending moment on the left side, left-hand side, it's 10,406 kilonewtons/metre width; right?</li> </ul>
3 4 5 6 7 8 9 10 11 12 13 14 15 16	<ul> <li>know, you really have made it meet all the rules</li> <li>exactly, then if you use a strut-and-tie, you might find</li> <li>the tension force is a little bit larger than the</li> <li>tension stresses in the computer analysis.</li> <li>CHAIRMAN: Put it this way, a better way than the rather</li> <li>clumsy way I put it earlier my apologies they</li> <li>complement each other, the tests?</li> <li>A. Yes.</li> <li>COMMISSIONER HANSFORD: In some areas, in some professions.</li> <li>I might suggest, reference is made to a quick and dirty</li> <li>analysis, if you can excuse that term.</li> <li>A. That's fine.</li> <li>COMMISSIONER HANSFORD: Therefore, would an overnight</li> <li>strut-and-tie analysis constitute a quick and dirty?</li> </ul>	3 4 5 6 7 8 9 10 11 12 13 14 15 16	<ul> <li>concern?</li> <li>A. No, absolutely not. No, no, no, of course not.</li> <li>COMMISSIONER HANSFORD: Thank you.</li> <li>MR CHOW: Thank you, Prof Hansford.</li> <li>Mr Southward, just now you told us that yesterday you have carried out your checking for the first time. Is it the 23rd slide or the 25th slide, is that right, where you set out the result?</li> <li>A. Yes.</li> <li>Q. Now, I have a few questions on this. First of all, the bending moment that you use for your strut-and-tie analysis, if you look at the bending moment on the left side, left-hand side, it's 10,406 kilonewtons/metre width; right?</li> <li>A. Yes.</li> </ul>
3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	<ul> <li>know, you really have made it meet all the rules</li> <li>exactly, then if you use a strut-and-tie, you might find</li> <li>the tension force is a little bit larger than the</li> <li>tension stresses in the computer analysis.</li> <li>CHAIRMAN: Put it this way, a better way than the rather</li> <li>clumsy way I put it earlier my apologies they</li> <li>complement each other, the tests?</li> <li>A. Yes.</li> <li>COMMISSIONER HANSFORD: In some areas, in some professions,</li> <li>I might suggest, reference is made to a quick and dirty</li> <li>analysis, if you can excuse that term.</li> <li>A. That's fine.</li> <li>COMMISSIONER HANSFORD: Therefore, would an overnight</li> <li>strut-and-tie analysis constitute a quick and dirty?</li> <li>A. It would be, yes.</li> </ul>	3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	<ul> <li>concern?</li> <li>A. No, absolutely not. No, no, no, of course not.</li> <li>COMMISSIONER HANSFORD: Thank you.</li> <li>MR CHOW: Thank you, Prof Hansford.</li> <li>Mr Southward, just now you told us that yesterday you have carried out your checking for the first time. Is it the 23rd slide or the 25th slide, is that right, where you set out the result?</li> <li>A. Yes.</li> <li>Q. Now, I have a few questions on this. First of all, the bending moment that you use for your strut-and-tie analysis, if you look at the bending moment on the left side, left-hand side, it's 10,406 kilonewtons/metre width; right?</li> <li>A. Yes.</li> <li>Q. If you look at Atkins, the section the Atkins</li> </ul>
3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	<ul> <li>know, you really have made it meet all the rules</li> <li>exactly, then if you use a strut-and-tie, you might find</li> <li>the tension force is a little bit larger than the</li> <li>tension stresses in the computer analysis.</li> <li>CHAIRMAN: Put it this way, a better way than the rather</li> <li>clumsy way I put it earlier my apologies they</li> <li>complement each other, the tests?</li> <li>A. Yes.</li> <li>COMMISSIONER HANSFORD: In some areas, in some professions.</li> <li>I might suggest, reference is made to a quick and dirty</li> <li>analysis, if you can excuse that term.</li> <li>A. That's fine.</li> <li>COMMISSIONER HANSFORD: Therefore, would an overnight</li> <li>strut-and-tie analysis constitute a quick and dirty?</li> <li>A. It would be, yes.</li> <li>COMMISSIONER HANSFORD: Thank you.</li> </ul>	3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	<ul> <li>concern?</li> <li>A. No, absolutely not. No, no, no, of course not.</li> <li>COMMISSIONER HANSFORD: Thank you.</li> <li>MR CHOW: Thank you, Prof Hansford.</li> <li>Mr Southward, just now you told us that yesterday you have carried out your checking for the first time. Is it the 23rd slide or the 25th slide, is that right, where you set out the result?</li> <li>A. Yes.</li> <li>Q. Now, I have a few questions on this.</li> <li>First of all, the bending moment that you use for your strut-and-tie analysis, if you look at the bending moment on the left side, left-hand side, it's 10,406 kilonewtons/metre width; right?</li> <li>A. Yes.</li> <li>Q. If you look at Atkins, the section the Atkins calculation, on the manuscript page, page 19, the</li> </ul>
3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	<ul> <li>know, you really have made it meet all the rules</li> <li>exactly, then if you use a strut-and-tie, you might find</li> <li>the tension force is a little bit larger than the</li> <li>tension stresses in the computer analysis.</li> <li>CHAIRMAN: Put it this way, a better way than the rather</li> <li>clumsy way I put it earlier my apologies they</li> <li>complement each other, the tests?</li> <li>A. Yes.</li> <li>COMMISSIONER HANSFORD: In some areas, in some professions.</li> <li>I might suggest, reference is made to a quick and dirty</li> <li>analysis, if you can excuse that term.</li> <li>A. That's fine.</li> <li>COMMISSIONER HANSFORD: Therefore, would an overnight</li> <li>strut-and-tie analysis constitute a quick and dirty?</li> <li>A. It would be, yes.</li> <li>COMMISSIONER HANSFORD: Thank you.</li> <li>A. And I have to stress that there are lots of different</li> </ul>	3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	<ul> <li>concern?</li> <li>A. No, absolutely not. No, no, no, of course not.</li> <li>COMMISSIONER HANSFORD: Thank you.</li> <li>MR CHOW: Thank you, Prof Hansford.</li> <li>Mr Southward, just now you told us that yesterday you have carried out your checking for the first time. Is it the 23rd slide or the 25th slide, is that right, where you set out the result?</li> <li>A. Yes.</li> <li>Q. Now, I have a few questions on this.</li> <li>First of all, the bending moment that you use for your strut-and-tie analysis, if you look at the bending moment on the left side, left-hand side, it's 10,406 kilonewtons/metre width; right?</li> <li>A. Yes.</li> <li>Q. If you look at Atkins, the section the Atkins calculation, on the manuscript page, page 19, the bending moment used by Atkins is 14,000.</li> </ul>
3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	<ul> <li>know, you really have made it meet all the rules</li> <li>exactly, then if you use a strut-and-tie, you might find</li> <li>the tension force is a little bit larger than the</li> <li>tension stresses in the computer analysis.</li> <li>CHAIRMAN: Put it this way, a better way than the rather</li> <li>clumsy way I put it earlier my apologies they</li> <li>complement each other, the tests?</li> <li>A. Yes.</li> <li>COMMISSIONER HANSFORD: In some areas, in some professions,</li> <li>I might suggest, reference is made to a quick and dirty</li> <li>analysis, if you can excuse that term.</li> <li>A. That's fine.</li> <li>COMMISSIONER HANSFORD: Therefore, would an overnight</li> <li>strut-and-tie analysis constitute a quick and dirty?</li> <li>A. It would be, yes.</li> <li>COMMISSIONER HANSFORD: Thank you.</li> <li>A. And I have to stress that there are lots of different</li> <li>ways you can draw out a strut-and-tie. You know, what</li> </ul>	3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	<ul> <li>concern?</li> <li>A. No, absolutely not. No, no, no, of course not.</li> <li>COMMISSIONER HANSFORD: Thank you.</li> <li>MR CHOW: Thank you, Prof Hansford.</li> <li>Mr Southward, just now you told us that yesterday you have carried out your checking for the first time. Is it the 23rd slide or the 25th slide, is that right, where you set out the result?</li> <li>A. Yes.</li> <li>Q. Now, I have a few questions on this. First of all, the bending moment that you use for your strut-and-tie analysis, if you look at the bending moment on the left side, left-hand side, it's 10,406 kilonewtons/metre width; right?</li> <li>A. Yes.</li> <li>Q. If you look at Atkins, the section the Atkins calculation, on the manuscript page, page 19, the bending moment used by Atkins is 14,000.</li> <li>A. Yes.</li> </ul>
3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	<ul> <li>know, you really have made it meet all the rules</li> <li>exactly, then if you use a strut-and-tie, you might find</li> <li>the tension force is a little bit larger than the</li> <li>tension stresses in the computer analysis.</li> <li>CHAIRMAN: Put it this way, a better way than the rather</li> <li>clumsy way I put it earlier my apologies they</li> <li>complement each other, the tests?</li> <li>A. Yes.</li> <li>COMMISSIONER HANSFORD: In some areas, in some professions.</li> <li>I might suggest, reference is made to a quick and dirty</li> <li>analysis, if you can excuse that term.</li> <li>A. That's fine.</li> <li>COMMISSIONER HANSFORD: Therefore, would an overnight</li> <li>strut-and-tie analysis constitute a quick and dirty?</li> <li>A. It would be, yes.</li> <li>COMMISSIONER HANSFORD: Thank you.</li> <li>A. And I have to stress that there are lots of different</li> <li>ways you can draw out a strut-and-tie. You know, what</li> <li>I drew, I don't say that's the absolute the way it</li> </ul>	3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	<ul> <li>concern?</li> <li>A. No, absolutely not. No, no, no, of course not.</li> <li>COMMISSIONER HANSFORD: Thank you.</li> <li>MR CHOW: Thank you, Prof Hansford.</li> <li>Mr Southward, just now you told us that yesterday you have carried out your checking for the first time. Is it the 23rd slide or the 25th slide, is that right, where you set out the result?</li> <li>A. Yes.</li> <li>Q. Now, I have a few questions on this.</li> <li>First of all, the bending moment that you use for your strut-and-tie analysis, if you look at the bending moment on the left side, left-hand side, it's 10,406 kilonewtons/metre width; right?</li> <li>A. Yes.</li> <li>Q. If you look at Atkins, the section the Atkins calculation, on the manuscript page, page 19, the bending moment used by Atkins is 14,000.</li> <li>A. Yes.</li> <li>Q. Then why don't you use Atkins' bending moment for your</li> </ul>
3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>know, you really have made it meet all the rules</li> <li>exactly, then if you use a strut-and-tie, you might find</li> <li>the tension force is a little bit larger than the</li> <li>tension stresses in the computer analysis.</li> <li>CHAIRMAN: Put it this way, a better way than the rather</li> <li>clumsy way I put it earlier my apologies they</li> <li>complement each other, the tests?</li> <li>A. Yes.</li> <li>COMMISSIONER HANSFORD: In some areas, in some professions.</li> <li>I might suggest, reference is made to a quick and dirty</li> <li>analysis, if you can excuse that term.</li> <li>A. That's fine.</li> <li>COMMISSIONER HANSFORD: Therefore, would an overnight</li> <li>strut-and-tie analysis constitute a quick and dirty?</li> <li>A. It would be, yes.</li> <li>COMMISSIONER HANSFORD: Thank you.</li> <li>A. And I have to stress that there are lots of different</li> <li>ways you can draw out a strut-and-tie. You know, what</li> <li>I drew, I don't say that's the absolute the way it</li> <li>works. It's just a representation. And the point is</li> </ul>	3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>concern?</li> <li>A. No, absolutely not. No, no, no, of course not.</li> <li>COMMISSIONER HANSFORD: Thank you.</li> <li>MR CHOW: Thank you, Prof Hansford.</li> <li>Mr Southward, just now you told us that yesterday you have carried out your checking for the first time. Is it the 23rd slide or the 25th slide, is that right, where you set out the result?</li> <li>A. Yes.</li> <li>Q. Now, I have a few questions on this.</li> <li>First of all, the bending moment that you use for your strut-and-tie analysis, if you look at the bending moment on the left side, left-hand side, it's 10,406 kilonewtons/metre width; right?</li> <li>A. Yes.</li> <li>Q. If you look at Atkins, the section the Atkins calculation, on the manuscript page, page 19, the bending moment used by Atkins is 14,000.</li> <li>A. Yes.</li> <li>Q. Then why don't you use Atkins' bending moment for your strut-and-tie analysis?</li> </ul>
3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	<ul> <li>know, you really have made it meet all the rules</li> <li>exactly, then if you use a strut-and-tie, you might find</li> <li>the tension force is a little bit larger than the</li> <li>tension stresses in the computer analysis.</li> <li>CHAIRMAN: Put it this way, a better way than the rather</li> <li>clumsy way I put it earlier my apologies they</li> <li>complement each other, the tests?</li> <li>A. Yes.</li> <li>COMMISSIONER HANSFORD: In some areas, in some professions.</li> <li>I might suggest, reference is made to a quick and dirty</li> <li>analysis, if you can excuse that term.</li> <li>A. That's fine.</li> <li>COMMISSIONER HANSFORD: Therefore, would an overnight</li> <li>strut-and-tie analysis constitute a quick and dirty?</li> <li>A. It would be, yes.</li> <li>COMMISSIONER HANSFORD: Thank you.</li> <li>A. And I have to stress that there are lots of different</li> <li>ways you can draw out a strut-and-tie. You know, what</li> <li>I drew, I don't say that's the absolute the way it</li> <li>works. It's just a representation. And the point is</li> <li>that in a finite element analysis, it's elastic</li> </ul>	3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	<ul> <li>concern?</li> <li>A. No, absolutely not. No, no, no, of course not.</li> <li>COMMISSIONER HANSFORD: Thank you.</li> <li>MR CHOW: Thank you, Prof Hansford.</li> <li>Mr Southward, just now you told us that yesterday you have carried out your checking for the first time. Is it the 23rd slide or the 25th slide, is that right, where you set out the result?</li> <li>A. Yes.</li> <li>Q. Now, I have a few questions on this.</li> <li>First of all, the bending moment that you use for your strut-and-tie analysis, if you look at the bending moment on the left side, left-hand side, it's 10,406 kilonewtons/metre width; right?</li> <li>A. Yes.</li> <li>Q. If you look at Atkins, the section the Atkins calculation, on the manuscript page, page 19, the bending moment used by Atkins is 14,000.</li> <li>A. Yes.</li> <li>Q. Then why don't you use Atkins' bending moment for your strut-and-tie analysis?</li> <li>A. Because I guess those are for two different panels.</li> </ul>
3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>know, you really have made it meet all the rules</li> <li>exactly, then if you use a strut-and-tie, you might find</li> <li>the tension force is a little bit larger than the</li> <li>tension stresses in the computer analysis.</li> <li>CHAIRMAN: Put it this way, a better way than the rather</li> <li>clumsy way I put it earlier my apologies they</li> <li>complement each other, the tests?</li> <li>A. Yes.</li> <li>COMMISSIONER HANSFORD: In some areas, in some professions.</li> <li>I might suggest, reference is made to a quick and dirty</li> <li>analysis, if you can excuse that term.</li> <li>A. That's fine.</li> <li>COMMISSIONER HANSFORD: Therefore, would an overnight</li> <li>strut-and-tie analysis constitute a quick and dirty?</li> <li>A. It would be, yes.</li> <li>COMMISSIONER HANSFORD: Thank you.</li> <li>A. And I have to stress that there are lots of different</li> <li>ways you can draw out a strut-and-tie. You know, what</li> <li>I drew, I don't say that's the absolute the way it</li> <li>works. It's just a representation. And the point is</li> </ul>	3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	<ul> <li>concern?</li> <li>A. No, absolutely not. No, no, no, of course not.</li> <li>COMMISSIONER HANSFORD: Thank you.</li> <li>MR CHOW: Thank you, Prof Hansford.</li> <li>Mr Southward, just now you told us that yesterday you have carried out your checking for the first time. Is it the 23rd slide or the 25th slide, is that right, where you set out the result?</li> <li>A. Yes.</li> <li>Q. Now, I have a few questions on this.</li> <li>First of all, the bending moment that you use for your strut-and-tie analysis, if you look at the bending moment on the left side, left-hand side, it's 10,406 kilonewtons/metre width; right?</li> <li>A. Yes.</li> <li>Q. If you look at Atkins, the section the Atkins calculation, on the manuscript page, page 19, the bending moment used by Atkins is 14,000.</li> <li>A. Yes.</li> <li>Q. Then why don't you use Atkins' bending moment for your strut-and-tie analysis?</li> </ul>

	Page 161		Page 163
1	I asked for the typical bending moment and it came to	1	CHAIRMAN: That's excellent. Thank you very much. Then we
2		2	will adjourn for the day, a quarter of an hour earlier,
3		3	for the reasons I gave earlier.
4	So that is the bending moments for panel EH113, so	4	Tomorrow morning, 10 o'clock. Thank you.
5	I have checked panel EH113.	5	You are reminded again, Mr Southward thank you
6	Q. Okay. So you are only well, on the assumption that	6	very much about keeping your own counsel now until
7	your calculation is correct, all that you can say is the	7	the completion of your evidence.
8	panel that you have checked is safe?	8	WITNESS: Yes.
9	A. Well, that's correct, yes.	9	MR SHIEH: Can I just clarify that Mr Southward is supposed
10	Q. I see. Okay.	10	to do the calculation and produce it on a piece of paper
11	A. Prof Au did say that there were lots of different	11	tomorrow, because I don't want people to get confused as
12	panels.	12	to when he's going to produce the calculation?
13	Q. Yes.	13	COMMISSIONER HANSFORD: If that's something he could readily
14	A. So there are. I don't dispute that.	14	do, it might be useful.
15	Q. The force diagram that you show, have you checked	15	MR SHIEH: I just want to clarify, in order not to waste
16	whether the resistance inside the connection is able to	16	time tomorrow, not to have any misunderstanding as to
17	take up those forces? For example, the inclined force,	17	what Mr Chow is asking for.
18	the tension force which runs diagonal between from	18	CHAIRMAN: I'm not sure exactly what was being asked for.
19	the top, on the left-hand side, down to the right of the	19	COMMISSIONER HANSFORD: I'm not sure we need it, actually.
20	lower part, the blue line with arrows, that represents	20	I'm not sure we need it. You asked Mr Southward whether
21	the tension; is that right?	21	he had done that calculation.
22	A. It does, yes.	22	MR CHOW: That's right, yes.
23	Q. I can't find any reinforcement to resist that tension?	23	COMMISSIONER HANSFORD: He has said he has.
24	A. There are horizontal shear links. There are horizontal	24	CHAIRMAN: Good. Thank you very much.
25	shear links in the diaphragm wall that are referred to	25	(4.48 pm)
	Page 162		Page 164
1	in the Atkins calculation of December. In the back of	1	(The hearing adjourned until 10.00 am the following day)
2	that, there are diagrams showing the diaphragm wall	2	
3	panels and there are shear links.	3	
4	Q. Have you checked the dimension or the cross-sectional	4	
5	area of the shear links to satisfy yourself that	5	
6	A. I believe the shear links are T16.	6	
7	Q. Have you checked? This is my question.	7	
8	A. Yes, I looked at the drawing and I saw that the shear	8	
9	links were T16.	9	
10	Q. Have you checked numerically, determined the	10	
11	cross-section of the shear link and then compared it	11	
12	with the tension force that you have found, to satisfy	12	
13	yourself that there are sufficient shear links to resist	13	
14	the tension force?	14	
15	A. Yes.	15	
16		16	
17	A. Well, to be honest, I have done yes, of course I can,	17	
18	2	18	
19	5	\$ 19	
20		20	
21	into structural calculations, but that's just	21	
21 22	into structural calculations, but that's just an observation.	21 22	
21 22 23	into structural calculations, but that's just an observation. MR CHOW: Thank you, Prof Hansford.	21 22 23	
21 22	<ul><li>into structural calculations, but that's just</li><li>an observation.</li><li>MR CHOW: Thank you, Prof Hansford.</li><li>Mr Chairman, I note the time. According to my</li></ul>	21 22	

Page 165	
1 INDEX 2 PAGE 3 PROF YEUNG TAK CHUNG, ALBERT (on former1 affirmation)	
<ul> <li>Further cross-examination by MR SHIEH2</li> <li>Further cross-examination by MR BOULDING17</li> <li>Questioning by THE COMMISSIONERS31</li> <li>Cross-examination by MR CHOW38</li> <li>Re-examination by MR SO</li></ul>	
<ul> <li>Re-examination by MR SO</li></ul>	
Closs-coanination by Mix CHOW	
25	